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**Line Positions and Intensities in the  $2\nu_2/\nu_4$  Vibrational  
System of  $^{14}\text{NH}_3$  near 5-7  $\mu\text{m}$**

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## Abstract

Line positions and intensities belonging to the vibrational system  $2\nu_2/\nu_4$  of ammonia  $^{14}\text{NH}_3$  are measured and analyzed between 1200 and 2200  $\text{cm}^{-1}$  in order to improve the molecular database. For this, laboratory spectra are obtained at 0.006 and 0.011  $\text{cm}^{-1}$  unapodized resolution and with 4% precisions for the intensities using Fourier transform spectrometers located at the Kitt Peak National Observatory and the Jet Propulsion Laboratory. The observed data contain transitions of the  $\nu_4$  fundamental band near 1626.276(1) and 1627.375(2)  $\text{cm}^{-1}$  (for s and a inversion upper states respectively) and the  $2\nu_2$  overtone band near 1597.470(3) and 1882.179(5)  $\text{cm}^{-1}$  (for s and a inversion states respectively). A total of 2345 lines with  $J' \leq 15$  is assigned from which 2114 lines positions with  $J' \leq 15$  are fitted using an effective rotation-inversion-rotation Hamiltonian to achieve a rms of 0.003  $\text{cm}^{-1}$  with 57 molecular parameters. Over 1200 intensity measurements are modeled to  $\pm 4.7\%$  using 16 terms of the dipole moment expansion. A dyad model is used in order to model all the interactions expected within the  $2\nu_2/\nu_4$  system. The bandstrengths of  $2\nu_2$  (s $\leftarrow$ a),  $2\nu_2$  (a $\leftarrow$ s) and  $\nu_4$  (s $\leftarrow$ s and a $\leftarrow$ a) are estimated to be 6.68(24), 0.201(5) and 116(3)  $\text{cm}^{-2} \text{ atm}^{-1}$  respectively at 296 K. The prediction generated by this study is available for planetary studies.

## I. INTRODUCTION

Ammonia is the fourth most abundant constituent in the atmosphere of Jupiter, after hydrogen, helium and methane (1). The 5-7  $\mu\text{m}$  window is of particular interest for studies of the giant planets because the detected radiation originates from deep in the atmosphere where pressures are a few bars (1). In particular, in May 1997, the SWS (Short Wavelength Spectrometer) instrument on board of the ISO satellite recorded spectra of the Jovian atmosphere from 2.4 to 45  $\mu\text{m}$  at an average resolving power of 1500. The 5 and 10  $\mu\text{m}$  spectral range of this SWS-ISO spectrum was interpreted with a line-by-line radiative transfer code by Fouchet et al. (2), using the  $\text{NH}_3$  spectroscopic data available at that time (3), but the analysis quickly revealed that a more complete and detailed database of spectroscopic parameters of  $^{14}\text{NH}_3$  in the 1200-2200  $\text{cm}^{-1}$  region was needed for the analysis of planetary data.

The goal of the present paper is thus to provide a complete prediction of line positions and intensities for the  $2\nu_2/\nu_4$  system of  $^{14}\text{NH}_3$  at 5-7  $\mu\text{m}$  similar to the

studies performed at 4  $\mu\text{m}$  and 3  $\mu\text{m}$  (4-5).

The main absorption of ammonia at 5-7  $\mu\text{m}$  is due to the  $\nu_4$  fundamental and the  $2\nu_2$  overtone band. With the large inversion splitting of the  $\nu_2$  vibrational mode, the  $2\nu_2/\nu_4$  system covers an extended range from 1200 to 2200  $\text{cm}^{-1}$ . The two overtone components,  $2\nu_2$  (s $\leftarrow$ a),  $2\nu_2$  (a $\leftarrow$ s) centered at 1597.470(3)  $\text{cm}^{-1}$  and 1882.179(5)  $\text{cm}^{-1}$ , respectively, are indeed no less than 285  $\text{cm}^{-1}$  apart. The two fundamental components  $\nu_4$  (s $\leftarrow$ s) and  $\nu_4$  (a $\leftarrow$ a) are centered at 1626.276(1)  $\text{cm}^{-1}$  and 1627.375(2)  $\text{cm}^{-1}$  respectively.

In the past, this spectral range was the object of many investigations of both line positions (6-14) and intensities (3, 15-22). Those studies assigned over 1600 line positions of  $^{14}\text{NH}_3$ , and the analyses revealed a strong Coriolis type coupling between the  $\nu_4$  (a $\leftarrow$ a) and the  $2\nu_2$  (s $\leftarrow$ a) components and also large l-type resonances in  $\nu_4$ . Urban et al. (6) studied the  $\nu_2 = 1$ ,  $\nu_2 = 2$ ,  $\nu_2 = 3$ ,  $\nu_4 = 1$  and  $\nu_2 = \nu_4 = 1$  interacting energy system by combining microwave and infrared data. They determined Coriolis couplings and l-type doubling constants using combined data from a vacuum grating infrared spectrometer, a diode laser spectrometer and a submillimeter wave spectrometer. About 420 lines of  $\nu_4$  band ( $J \leq 11$ ) and 180 lines of  $2\nu_2$  band ( $J \leq 12$ ) were assigned from 1450 to 2086  $\text{cm}^{-1}$ . Using a theoretical treatment developed by Spirko et al. (23), the molecular constants for the  $\nu_2 = 2$  and  $\nu_4 = 1$  states were determined by least-squares with a standard deviation of 0.041  $\text{cm}^{-1}$ . Later on, Cohen et al. (7) and Urban et al. (8) assigned about 860 perturbation-allowed transitions (in  $\Delta K = \pm 3$  and  $\Delta K = \pm 2$ ) in  $\nu_4$ . More recently, Sasada et al. (9, 10) gathered a number of published measurements and added about 630 new IR measurements ( $J \leq 13$ ) and 153 MW transitions in  $\nu_2 = 2$  (s) and  $\nu_4 = 1$  (s and a). Those authors achieved a root mean square deviation of 0.00038  $\text{cm}^{-1}$  for the IR transitions, but when the MW data were weighted according to the experimental accuracy, large IR data deviations were generated. The number of adjusted parameters used was quite important; no less than 91 parameters were needed to model upper state levels of the three components up to  $J = 13$ , and for 11 pairs of those parameters, there was a strong correlation factor larger than 0.99.

The highest upper state component  $\nu_2 = 2$  (a) was studied up to  $J = 11$ ,  $K = 10$  by Lellouch et al. (3) who assigned about 90 transitions in the  $2\nu_2$  (a $\leftarrow$ s) band between 1800-2100  $\text{cm}^{-1}$ . Upper state energy parameters of this  $2\nu_2$  (a $\leftarrow$ s) component were also obtained by hot band studies of  $\nu_2=2$  (a)  $\leftarrow$   $\nu_2=1$  (s) (24-26).

The line intensities with reported precisions of 5% to 15% were measured at high resolution in five prior studies. In the 1480-1596  $\text{cm}^{-1}$  spectral range, some 40 experimental intensities from a tunable diode laser spectrometer were reported by Urban et al. (15, 16) for both components of  $\nu_4$  (including 18  $\Delta K=\pm 2$  perturbation-allowed transitions) and the lower component of  $2\nu_2$  ( $s\leftarrow a$ ). Using Fourier transform spectrometers, Lellouch et al. (3) obtained over 750 line intensities in  $\nu_4$  and  $2\nu_2$  ( $a\leftarrow s$ ) in the 1800-2100  $\text{cm}^{-1}$  range while Aroui et al. (17) measured about 57 P branch line intensities in  $\nu_4$  near 1550  $\text{cm}^{-1}$ . Most recently, Kralik et al. (18) obtained intensities of 16 R branch lines of  $\nu_4$  between 1793 and 1810  $\text{cm}^{-1}$ .

None of the previous studies covers the total spectral range of the four components of the  $2\nu_2/\nu_4$  system nor do they simultaneously model both line positions and intensities. Therefore, in the present effort, a comprehensive new data set is obtained for the whole region between 1200 and 2200  $\text{cm}^{-1}$ . Assignments are extended and completed as much as possible to  $J = 15$ . The  $2\nu_2/\nu_4$  system is treated as a dyad so that all Coriolis and "essential" resonance interactions ("l-type" and "K-type") between the four components  $2\nu_2$  ( $a\leftarrow s$ ),  $2\nu_2$  ( $s\leftarrow a$ ),  $\nu_4$  ( $a\leftarrow a$ ) and  $\nu_4$  ( $s\leftarrow s$ ) can be included explicitly. From the modeling of both line positions and intensities, a reliable prediction of the ammonia spectrum is achieved.

In this paper, Section II presents the experimental details. In Section III, we briefly describe the theoretical approach used. Section IV concerns the line positions and intensities analyses and the determination of energy and intensity parameters. Finally, results of Section IV are used in Section V to generate a line-by-line frequency and intensity prediction suitable for the analysis of the Jovian spectrum.

## II. EXPERIMENTAL DETAILS

Seventeen laboratory spectra of ammonia were recorded using the National Solar Observatory McMath FTS located at Kitt Peak National Observatory in Arizona, and five spectra were obtained using a Bruker HR120 FTS located at the Jet Propulsion Laboratory. The gas conditions of these data are listed in Table 1. The ammonia gas samples were generally in normal abundance.

The Kitt Peak data were collected during five different observing sessions between 1984 and 1995. The first nine spectra in Table 1 were recorded in the 900 to 2600  $\text{cm}^{-1}$  region using two matched As-doped Si detectors and a KCl beamsplitter. The next four runs at higher optical density were taken using the same detectors with a  $\text{CaF}_2$  beamsplitter. Finally, four other spectra from 1800 to 5200  $\text{cm}^{-1}$ , originally obtained for other studies (4, 5), were also measured to provide intensities of the very weak features throughout the important 5  $\mu\text{m}$  window region. These latter spectra were scanned using matched InSb detectors and a  $\text{CaF}_2$  beamsplitter. For all sets, global sources were used, and scans were integrated for 60 - 70 minutes to achieve signal-to-noise ratios of 300:1 or better.

In order to confirm the absolute accuracies of the intensity data, five additional spectra were recorded at JPL using a HR120 Bruker FTS. For this, a KCl beamsplitter and a Helium-cooled Boron-doped Silicon detector was used with a global source. Each Bruker spectrum was at 0.006  $\text{cm}^{-1}$  resolution. The signal from a global source was integrated for 3 to 4 hours to record the 6-to-5  $\mu\text{m}$  region.

Seven different absorption cells were utilized in all. Two of these (10. and 4. cm) were made of glass, and the rest were constructed of stainless steel. The path lengths greater than 1.5 m were achieved using multipass cells with base lengths of one meter and six meters. Pressures in the range of 2 to 20 Torr were selected in order to maximize the stability of the ammonia sample in the absorption cells. Pressures and temperatures were monitored continuously during the scanning using, respectively, capacitance manometers and thermistors (or for the 1-m-base white cell, platinum resistance thermocouples. For a few spectra, a second absorption chamber containing low pressure CO was included so that the 1 - 0 band (27) could be employed as the wavenumber calibration standard. For other spectra, the calibration was based on residual water features (28) or by calibrated  $\text{NH}_3$  transitions.

The spectra were measured by spectral curve fitting (29) of the unapodized spectrum in the manner described in other ammonia studies (4, 5, 30, 31). In the higher pressure scans, it was necessary to retrieve the self-broadened line widths and to fit features in larger intervals (of 1 to 2 wavenumbers) simultaneously in order to determine the location of the continuum correctly. A sample retrieval is

shown in Fig. 1 using the 10.9 Torr spectrum in the region of the  $2\nu_2$  ( $a \leftarrow s$ ) R branch. In the figure, the observed and computed spectra are overlaid, with the differences between the spectral digits plotted above.

A sample of the resulting individual measurements and the corresponding averaged values are shown in Table 2. The averages are marked by \*\* with the rms of the differences between the "ith" observed value from the average following the measurement; for intensities, the differences are shown in percent. It can be seen in Table 2 that the measurements cover nearly five orders of magnitude of intensity. Furthermore, there are no large systematic differences in the intensities from run to run.

The question of the absolute accuracies for intensities is addressed by comparing measurements from other instruments. In Table 2, it is seen that the results from the JPL Bruker are within a few percent of those from the Kitt Peak FTS. Furthermore, line-by-line comparisons with most other studies (3, 15-17, 18) also show good agreement with present results. The comparisons are summarized in Table 3, which gives the type of instrument, spectral range, type of transitions, and number of transitions reported by the other studies. Line intensities that were remeasured in the present study were selected, and the mean ratio of the intensities (other/present), the rms in percent and the range of the ratio values were computed. Three of the studies (3, 15 and 17) were found to be within 3% of the present values, even though these other measurements were done in somewhat different spectral regions with different spectrometers. One study (16), which had also used the FTS at Kitt Peak, reported intensities that were lower by a factor of 17. The source of their systematic error is likely a combination of uncertainty in the optical density and the method chosen to retrieve intensities from a limited number of ammonia spectra. Another study (18) differed by  $18\% \pm 14.5\%$ . Nevertheless, these comparisons suggest that the overall absolute accuracy of the  $^{14}\text{NH}_3$  intensities in the 5 to 7  $\mu\text{m}$  region is close to 3%, although the precisions of individual transitions vary greatly, as demonstrated by the rms values.

The new spectra in this study were intended primarily for the analysis of the line intensities, rather than for the positions, and thus higher ammonia pressures up to 20 Torr were selected to provide stability in the gas samples. Therefore, accuracies of the line positions taken from these data are affected by self-broadened pressure-induced shifts which are largely unknown. As discussed in the 3  $\mu\text{m}$  study (5),

pressure shifts might be as high as  $0.00025 \text{ cm}^{-1}$  per Torr. Therefore, many of the positions for  $2\nu_2$  (s  $\leftarrow$  a) and  $\nu_4$  were taken from the prior study of Sasada et al. (10); these had been retrieved with a reported accuracy of  $\pm 0.0002 \text{ cm}^{-1}$  from a spectrum of 1 Torr (also recorded at Kitt Peak). Toward the end of the present analysis, some 400 line centers were retrieved from a new low pressure spectrum of 0.1 Torr of ammonia (not listed in Table 1); when calibrated with carbon monoxide (27) and water (28) transitions, these new positions were found to agree with the old values with a mean difference of  $0.000004 \text{ cm}^{-1}$  and an rms of  $0.00020 \text{ cm}^{-1}$ . However, for the very weakest lines, particularly  $2\nu_2$  (a  $\leftarrow$  s), the positions were taken from scans with pressures of 6 to 20 Torr so that the accuracies may be  $\pm 0.003 \text{ cm}^{-1}$  even for isolated lines (like the R branch lines shown in Fig. 1).

### III. THEORETICAL MODEL

As in the  $4 \mu\text{m}$  and  $3 \mu\text{m}$  band system (4, 5), the present analysis of the infrared  $^{14}\text{NH}_3$  spectrum in the  $5\text{-}7 \mu\text{m}$  region uses the theoretical approach based on a vibration-inversion-rotation energy levels parameterization developed by Spirko et al. (23) and Urban et al. (32), and on an intensity parameterization introduced by Pracna et al. (33).

The two bands  $2\nu_2$  and  $\nu_4$  presently investigated are treated as a dyad system in order to account for the Coriolis type coupling between  $2\nu_2$  and  $\nu_4$  and also for all essential resonances (l-type and k-type) within  $2\nu_2$  or  $\nu_4$ . All the interactions between the  $2\nu_2/\nu_4$  system and other vibrational bands like  $\nu_2$ ,  $3\nu_2$  or  $\nu_2+\nu_4$  are assumed to be weak enough to be taken into account properly by a perturbation treatment via the contact transformation method. We will see later that this assumption is reasonably valid, as was the case for  $3\nu_2/\nu_2+\nu_4$  (4).

The same computer programs set up for the  $3 \mu\text{m}$  region (5) are used in the present investigation. The energy matrix needed in the present work to calculate the upper state energies of the  $2\nu_2/\nu_4$  system is very similar (in its rotational dependance) to the upper state energy matrix required for the  $3\nu_2/\nu_2+\nu_4$  system. The exact expressions of the energy matrix elements for the diagonal terms and for the essential resonances used in our present study are given in the Table 4. In Fig. 2, we represent the upper state energy matrix with the energy parameters used in the present study to describe the interactions between inversion-vibration-rotation



levels. Hereafter we will refer to the different interactions as “Coriolis 1”, “Coriolis 2”, “2, -1” l-type, “2, 2” l-type, “2, -4” l-type and “k-type” as defined in Fig. 2.

The transition dipole matrix elements corresponding to the transitions investigated in the  $2\nu_2$  and  $\nu_4$  bands are also similar in their rotational forms to those used in the  $3\nu_2$  and  $\nu_2+\nu_4$  bands. They can be found in Table IV of Ref. (4). The  $d_0^i$ ,  $d_{0n}^i$  ... and  $d_1^i$ ,  $d_{1n}^i$  ... parameters (where  $i$  represents the inversion quantum number for the lower state) represent the transition dipole moment and Herman-Wallis corrections for  $2\nu_2$  and  $\nu_4$  components respectively.

The basis wavefunctions used in Tables III and IV of Ref. (4) and in Table 4 of this paper are the eigenfunctions of the zero order Hamiltonian labeled  $|i, \nu_2, \nu_4, l_4; J, K\rangle$  where  $i = s$  or  $a$  represents the inversion symmetric and antisymmetric components respectively. Like in Refs. (4-5), the energy and transition dipole moment matrices are expressed (before diagonalization) in terms of symmetrized basis functions so that both matrices can be factored according to the symmetry classification of the vibration-inversion-rotation levels within the  $D_{3h}$  group.

#### IV. RESULTS

Energy and intensity parameters are determined by fitting the experimental data. In all our fits of the two upper state levels of  $^{14}\text{NH}_3$  between 5 and 7  $\mu\text{m}$ , the ground state parameters are fixed to the values reported by Urban et al. (8). Their ground state combination differences are better than  $10^{-4} \text{ cm}^{-1}$ , and therefore satisfactory for the present study. We thus decided to keep those ground state parameters to be consistent with our previous works (4, 5).

##### a) Line assignments and upper state energy fit :

Our study covers the spectral range of  $1200\text{--}2200 \text{ cm}^{-1}$ . Starting from the line positions and prior published assignments (3, 8, 10), we extended them up to  $J=15$ .

Using the ground state combination difference method, we increased the number of identified lines from about 1600 to 2345 transitions. In particular, for the relatively weak  $2\nu_2$  ( $a \leftarrow s$ ) band, some 40 line assignments were added to the 90 previously reported (3).

For the fit of the upper state energies, we discarded all lines corresponding to either multiple or uncertain assignments or corresponding to very weak lines until 2114 transitions remained. They include 1307 allowed transitions and 807 perturbation-allowed transitions. Our best fit in energy has allowed us to reproduce infrared experimental data with an overall rms of  $0.0034 \text{ cm}^{-1}$  using only 57 parameters for the 2114 fitted lines which all show (observed - calculated) values smaller than  $0.020 \text{ cm}^{-1}$ . All the transitions are included in the fit with the same weight equal to 1.0. The root-mean-square deviations (rms) in  $\text{cm}^{-1}$  are given in Table 5 and show the quality of the fit for each vibrational band and each inversion component. The 2114 fitted lines correspond to 114, 108, 245 and 225 different upper state energy levels for  $2\nu_2$  ( $s \leftarrow a$ ),  $2\nu_2$  ( $a \leftarrow s$ ),  $\nu_4$  ( $s \leftarrow s$ ) and  $\nu_4$  ( $a \leftarrow a$ ), respectively.

Although those rms values do not reach the experimental accuracy, they do represent an improvement over the prior analyses. For the first time, the four symmetric and asymmetric components of  $2\nu_2$  and  $\nu_4$  are included simultaneously in the model, increasing considerably the total spectral range analyzed in energy and intensity.

Our fit in fact takes into account all assigned lines up to  $J \leq 15$ . As illustrated in Fig. 3. a for the two components of  $2\nu_2$ , the observed-calculated values as a function of the upper state energy quantum numbers  $J'$  and  $K'$  stay around  $\pm 0.003 \text{ cm}^{-1}$  up to  $J = 13$ , and even when we add almost one hundred lines at higher  $J$ , the quality of the fit is similar. In particular, the  $2\nu_2$  ( $a \leftarrow s$ ) component, which is analyzed for the first time together with the other components, is rather well reproduced. There are 21 parameters fitted for  $\nu_2 = 2$ , 27 for  $\nu_4 = 1$  and 9 parameters fitted to describe the  $2\nu_2/\nu_4$  Coriolis coupling. No strong correlation between the parameters is observed, except between the diagonal  $\eta_J^s$  and  $\eta_K^s$  parameters (correlation of 0.99). We tried to eliminate this correlation by fitting only one of those parameters and fixing the other one to zero, but the rms deviation of the fit increased considerably in this case.

In the present least square fit, the choice of the higher order terms was sometimes difficult. In order to choose the best and the most predictable set of parameters, we

had to iterate between the position fit to the intensity fit. The decision to introduce a parameter in the energy fit was taken after considering its uncertainty, its correlation with other parameters and its influence on the intensity fit.

The tables that follow show our results with those from other investigations. However, comparisons with previous studies are difficult even with the most complete analysis done by Sasada et al. (10) who did not include in their fit the  $\nu_2 = 2$  (a) component and needed 91 parameters to fit 785 lines.

Tables 6.a and 6.b compare the parameters used in the fundamental state (8) and those obtained by our fits in different vibrational systems (4, 5). Table 6.a presents the parameters corresponding to the  $\nu_2$  overtones ( $\nu_2$ ,  $2\nu_2$  and  $3\nu_2$ ), while Table 6.b gives the parameters corresponding to the  $\nu_4$  overtones ( $\nu_4$  and  $2\nu_4$ ) and to the combination band  $\nu_2 + \nu_4$ . Table 6.c shows the values of the Coriolis interaction parameters for the  $2\nu_2/\nu_4$  system and the  $3\nu_2/\nu_2 + \nu_4$  system. Throughout Tables 6, the columns (s) give the values of the parameters for the symmetric component and the columns (a-s) give the differences of the parameters between the asymmetric and symmetric components.

In Table 6.a, we note that the values of the rotational parameters  $B_v$  and  $C_v$ , as well as the centrifugal distortion parameters  $D_v$  and  $H_v$ , show large differences with the values in the ground vibrational state when the inversion mode  $\nu_2$  is involved. For  $\nu_4$ , the second order centrifugal distortion parameters  $D_J$ ,  $D_{JK}$  and  $D_K$  are not significantly different from the fundamental values (8) or from those obtained by Sasada et al. (10), but for the  $3\nu_2$  overtone, they change sign. The same effect is also seen for the higher order terms  $H_J$ ,  $H_{JK}$ ,  $H_{KJ}$  and  $H_K$ , except that the change of sign already occurs for  $2\nu_2$ . For the  $2\nu_2^a$  component, the values of the fourth order centrifugal distortion parameters are in agreement with those obtained by D'Cunha (25) in their  $2\nu_2^a \leftarrow \nu_2^s$  hot band studies. The values of the eighth order centrifugal distortion terms are kept fixed to their ground state values from Ref. (8), as was done in the  $3\nu_2/\nu_2 + \nu_4$  and  $\nu_1/\nu_3/2\nu_4$  studies (4, 5).

In Table 6.b, among all the "essential" resonance parameters, only the l-type interaction parameters  $q_2$  and  $f_4$  (and their J and K dependance) have a sign determined by the giant l-type splitting occurring in  $\nu_4$ . The values obtained for  $q_2$  and  $f_4$  are positive, as presented in Tables 6. On the other hand, the relative signs of the  $q_{3v}$ ,  $q_1$ ,  $c_2$  and  $c_1$  parameters (and their rotational dependances) are not

determined by the fit, and changing all the signs of this series of parameters does not modify the fit. In the same way, changing the relative signs of  $c_1$  and  $c_2$  (and their rotational dependences) does not change the fit.

In Table 6.c, we show the values of the Coriolis parameters for the  $2\nu_2/\nu_4$  and  $3\nu_2/\nu_2+\nu_4$  systems. Contrary to the  $3\nu_2/\nu_2+\nu_4$  system, the leading Coriolis type interaction  $c_1^s$  term between the two vibrational states  $2\nu_2$  and  $\nu_4$  is very well determined due to the proximity of the  $\nu_2 = 2$  (s) and  $\nu_4 = 1$  (a) components, and no less than nine parameters are needed to describe properly the interaction between the two bands. Contrary to the symmetric component, the difference between the symmetric and asymmetric component of this Coriolis parameter ( $c_1^s - c_1^a$ ) between the  $2\nu_2^s$  and  $\nu_4^s$  components cannot be determined in our fit due to the fact that the  $2\nu_2^s$  component is far away from the  $\nu_4^s$  component, even though the first order correction in K of this difference ( $c_{1K}^s - c_{1K}^a$ ) appears to be significant. Our best fit (both in energy and intensity) is obtained by fixing the first order interaction term ( $c_1^s$ ) between  $2\nu_2^s$  and  $\nu_4^s$  to the same value as the  $c_1^s$  parameter.

All those interaction parameters are determined by fitting a large number of allowed and perturbation-allowed transitions for both the  $2\nu_2$  and  $\nu_4$  bands. In Table 7, we present the standard deviation (in  $\text{cm}^{-1}$ ) and the number of perturbation-allowed transitions fitted. With such a good modeling of the positions, most of the intensities of perturbation-allowed transitions can be well reproduced also (see next section). Finally, some 48 vibrationally mixed transitions involving a strong mixing between the  $2\nu_2$  and  $\nu_4$  upper states (50 - 50 mixing) are also included in the fit which show a rms deviation of  $0.0032 \text{ cm}^{-1}$ .

Due to the strong Coriolis interaction between the  $\nu_2 = 2$  (s) and  $\nu_4 = 1$  (a) upper state energy levels, avoided crossings are observed for high J values between 9 and 11 and K values ranging from 1 to 8 (except for  $K = 2$ ) of the  $2\nu_2^s$  component. An avoided crossing between the  $\nu_2 = 2$  (s) and  $\nu_4 = 1$  (a) upper state energy levels due to the fourth order Coriolis interaction is also observed for  $J = 12$  and  $K = 6$  of the  $2\nu_2^s$  component. Consequently, the first order ( $c_1^s$ ,  $c_{1J}^s$  and  $c_{1K}^s$ ) Coriolis interaction parameters are well determined in our fit (as well as their relative sign) and induce a strong mixing between the energy levels. For most upper state energy levels, the mixing of the basis wavefunctions  $|i, \nu_2, \nu_4, l_4; J K\rangle$  in the eigenfunction correspond to 10/90 % to 30/70 % and this rotational-vibrational mixing has a significant influence on the intensity, as shown in the next section.

## b) Intensity Fit

In the present work, some 1203 intensity measurements between 1253 and 2134  $\text{cm}^{-1}$  were modeled with a rms of 4.7 %. As seen in Table 5, some 142, 112, 501 and 426 transitions from  $2\nu_2$  ( $s \leftarrow a$ ),  $2\nu_2$  ( $a \leftarrow s$ ),  $\nu_4$  ( $s \leftarrow s$ ) and  $\nu_4$  ( $a \leftarrow a$ ) band, respectively, as well as 22 vibrationally mixed transitions were included in the fit. The standard deviations in Table 5, calculated as  $[I_{\text{obs}} - I_{\text{calc}} / I_{\text{obs}}] \times 100$  for each vibrational component, are 5.0 % for  $2\nu_2$  ( $s \leftarrow a, s$ ), 3.0 % for  $2\nu_2$  ( $a \leftarrow s, a$ ), 5.0 % for  $\nu_4$  ( $s \leftarrow s, a$ ), 4.8 % for  $\nu_4$  ( $a \leftarrow a, s$ ) and 5.5 % for 22 vibrationally mixed lines, similar to the 5 % experimental accuracy. Fig. 3.b. shows the observed-calculated intensities (%) as a function of the lower state quantum numbers  $J''$  and  $K''$  for the allowed transitions  ${}^1Q$ ,  ${}^1P$  and  ${}^1R$  of the two components of  $2\nu_2$ . As in the energy fit, we were able to include in the intensity fit as many high  $J$  values as possible, in particular for the newly modeled  $2\nu_2$  ( $a \leftarrow s$ ) component. Thus we believe that this demonstrates the reliability of the model to reproduce the measurements and to predict the spectrum through the full range of the observed values of  $J$ .

The Appendix presents all the fitted line intensities; it lists the line assignment (column I-III), the observed line position (IV), the difference between observed and calculated positions (in  $10^{-3} \text{ cm}^{-1}$ ) (V), the measured intensity ( $S_o$ ) (VI) and corresponding estimated measurement uncertainty in percent (VII), the difference between measured and calculated intensities in percent ( $(S_o - S_c) / S_o$ ) (VIII) and the number of optical densities used for the intensity measurement (IX).

The sixteen fitted transition moment parameters are given in Table 8 which lists the parameters as defined in Table IV of Ref. (4), the retrieved values and uncertainties by vibrational component and the rotational quantum number dependence associated with each term. Only parameters showing a test value greater than twice the overall test value were retained as significant parameters.

Prior to selecting which transition moments to use, it was necessary to evaluate the effect of the implicit interactions on the calculated intensities. It was found that the intensity of  $2\nu_2$  ( $a \leftarrow s$ ) component is particularly sensitive to the Coriolis interaction modeling between  $2\nu_2^a$  and  $\nu_4^s$  components. If, in the energy fit, all the Coriolis

interaction parameters (including all the J and K dependance of those parameters) between  $2\nu_2^a$  and  $\nu_4^s$  components are set equal or opposite to those between  $2\nu_2^s$  and  $\nu_4^a$  components, the  $2\nu_2^a$  intensities are greatly overestimated (up to 90%), particularly in the R branch. On the other hand, when we consider the  $c_1^a$  value different from the asymmetric component  $c_1^s$  (i.e. when we try to fit both the  $c_1^s$  parameter and the difference ( $c_1^a - c_1^s$ ) in the energy fit), we note that the  $2\nu_2^a$  intensities are not well modeled either; the standard deviation goes up to about 12% for this component, and there is no significant decrease in the standard deviation for the other bands. Finally, we conclude that the best intensity calculation is obtained when, as already mentioned in the previous section, we fit only the  $c_1^s$  parameter, constrain the difference  $c_1^a - c_1^s$  to zero, and fit both the  $c_{1K}^s$  and the difference ( $c_{1K}^a - c_{1K}^s$ ).

For the  $\nu_4$  band, we need seven intensity parameters (the leading term  $d_1$  and six Herman-Wallis terms  $d_{11}$ ,  $d_{12}$ ,  $d_{15}$ ,  $d_{16}$ ,  $d_{17}$  and  $d_{18}$ ) to model 927 lines with a rms deviation of 4.9 %. The differences  $d^a - d^s$  for those  $\nu_4$  band parameters are not found to be significant and are set to zero. For the  $2\nu_2$  band, nine intensity parameters (the leading terms for the s and a components  $d_0^s$  and ( $d_0^a - d_0^s$ ) and four Herman-Wallis terms  $d_{01}^s$ ,  $d_{02}^s$ ,  $d_{03}^s$  and  $d_{04}^s$  and three of their ( $d^a - d^s$ ) corresponding values) were required to fit 254 lines to a rms deviation of 4.1%. The group of  $d_{11}$ ,  $d_{12}$ ,  $d_{15}$ ,  $d_{16}$  and  $d_{01}$ ,  $d_{02}$ ,  $d_{03}$  and  $d_{04}$  intensity parameters ( as defined in Table IV in Ref. (4)) represents the J and K dependance Herman - Wallis correction of the leading term  $d_1$  for  $\nu_4$  and  $d_0$  for  $2\nu_2$  respectively. The role of those Herman-Wallis corrections is very important: if we fit only the leading terms, the standard deviation goes up to 68 % for the  $\nu_4$  band and to 28 and 60 % for the  $2\nu_2$  (s) and  $2\nu_2$  (a) components. The  $d_{17}$  and  $d_{18}$  (the J (J+1) dependance of  $d_{17}$ ) intensity parameters become determined only when we take into account in the fit the perturbation-allowed transitions in  $\Delta J = 0, \pm 1$  and  $\Delta K = \pm 2$  of  $\nu_4$  (noted "O" and "S" in the Appendix).

As it can be seen in Table 7, these perturbation-allowed transitions of the  $\nu_4$  band in  $\Delta K = \pm 2$  are reproduced with a 6.5 % rms standard deviation, slightly larger than the experimental accuracy. It is to note that for the first time we were able to model a large number of perturbation-allowed transitions, not only in energy but also in intensity.

For a given inversion state, we consider the vibrational dipole moments defined as following :

$$\langle \mu_v \rangle 2\nu_2 (a \leftarrow s) = |d_0^s| / \sqrt{2} = 0.003256(35) \text{ D} \quad (1)$$

$$\langle \mu_v \rangle 2\nu_2 (s \leftarrow a) = |d_0^a| / \sqrt{2} = 0.02036(25) \text{ D} \quad (2)$$

$$\langle \mu_v \rangle \nu_4 (s \leftarrow s) = |d_1^s| = \langle \mu_v \rangle \nu_4 (a \leftarrow a) = |d_1^a| = 0.08408(34) \text{ D} \quad (3)$$

In Table 9, we show the total integrated band intensity  $S_v(\text{int})$  (sixth column), defined by the summation of all the transitions associated with a band :

$$S_v(\text{int}) = \sum_{\Delta J, \Delta K} S_A^B \quad (4)$$

where  $S_A^B$  is the line intensity of a  $\Delta J, \Delta K$  transition from state A to state B predicted by our model. This prediction is calculated up to  $J = 15$ , using the energy and intensity parameters from Tables 6.a, 6.b and 8 respectively, and taking the total partition function equal to 577.16 at 296 K as calculated by Urban et al. (15). The number of transitions (second column) and the minimum and maximum positions (third and fourth column) used for calculating this sum are also shown in Table 9. We can also define the vibrational bandstrength  $S_v^0$  such as:

$$S_v(\text{int}) = \sum_{\Delta J, \Delta K} S_A^B = S_v^0 \left[ \sum_{\Delta J, \Delta K} R_A^B(\Delta J, \Delta K) \cdot F(m) \right] \quad (5)$$

where  $R_A^B(\Delta J, \Delta K)$  contains the rotational part of the intensity as defined in Ref. (34).  $F(m)$  is the Herman-Wallis factor and describes the  $m$  dependance ( $m = -J_A$  in P branch,  $m = J_A + 1$  in R branch) and  $K$  dependance of the effective vibrational transition moment :

$$S_v(\text{int}) = S_v^0 \sum_{\Delta J, \Delta K} R_A^B(\Delta J, \Delta K) \cdot \left( 1 + \frac{d_{np}}{d_n} + \frac{d_{np'}}{d_n} m + 2 \frac{d_{np''}}{d_n} K + \dots \right) \quad (6)$$

Where  $d_n, d_{np}, \dots$  are the Herman-Wallis coefficients defined in Table 8 for each component.

If we assume that  $\sum_{\Delta J, \Delta K} R_A^B(\Delta J, \Delta K) \cdot F(m) \approx 1$ , the total integrated band intensity is approximated by the  $S_v^0$  vibrational bandstrength expressed by ( in  $\text{cm}^{-2}\text{atm}^{-1}$ ):

$$S_v(\text{int}) \approx S_v^0 = \frac{8\pi^3}{3hc} \cdot \frac{v_0 \cdot \mathcal{L} T_0}{Q_v(T) \cdot T} \cdot \langle \mu_v \rangle^2 \quad (7)$$

with  $\mathcal{L} = 2.68675 \times 10^{19} \text{ molecules} \cdot \text{cm}^{-3} \cdot \text{atm}^{-1}$  at  $T_0 = 273.15 \text{ K}$ . The band centers  $v_0$  are taken from Table 6 and  $\langle \mu_v \rangle^2$  is the vibrational dipole moment for each component from Eq. (1)-(3). In Eq. (7),  $Q_v$  is the vibrational partition function and is equal to 1.022(10) in the harmonic approximation (35) with the band centers from Refs. (4, 5). The uncertainty on the vibrational partition function is estimated to be 2%.

The assumption that leads to Eq. (7) is valid as long as the vibrational band under study is relatively isolated and as long as the mixing of the wavefunctions describing the upper state energy levels is small. For the  $2\nu_2/\nu_4$  system, this mixing is not so small due to the Coriolis-type and l-type interactions and so the value of the total vibrational bandstrengths  $S_v^0$  ( $123(3) \text{ cm}^{-2} \text{atm}^{-1}$  at 296 K) shown in the last column of Table 9 differs by 5 % from the total integrated band intensity, equal to  $117(6) \text{ cm}^{-2} \text{atm}^{-1}$  but is still within the error bar.

In our previous study of the  $3\nu_2/\nu_2+\nu_4$  system (4), the Herman-Wallis correction was introduced in the calculation of the vibrational bandstrength. As we noticed that the  $d_{12}$  Herman-Wallis correction for  $\nu_2+\nu_4$  was especially large, a so-called "effective" vibrational transition moment was therefore introduced (see Eq. (7) in Ref. (4)):

$$\langle \mu_{v=\nu_2+\nu_4} \rangle^2 = d_1^2 \left( 1 + \frac{d_{12}}{d_1} \right)^2 \quad (12)$$

For the  $\nu_4$  band presently studied, we could in principle consider the same development for the vibrational transition moment as the  $d_{11}$  (m dependance) Herman-Wallis correction is especially large and even larger than the  $d_{12}$  (K dependance) Herman-Wallis correction. But the introduction of the  $d_{11}$  Herman-Wallis correction in the  $S_v^0$  vibrational bandstrength is not straightforward as its effect is different for each  $\Delta J$  branch. So none of those effects were thus considered



here.

Table 10 shows a comparison between the values we obtained for the transition dipole moment matrix elements,  $\langle 0^{s(a)}, 0^0 | \mu_z | 2^{a(s)}, 0^0 \rangle$  and  $\langle 0^{s(a)}, 0^0 | \mu_x | 0^0, 1_{\pm}^{1s(a)} \rangle = \langle 0^{s(a)}, 0^0 | \mu_y | 0^0, 1_{\pm}^{1s(a)} \rangle$  for the  $2\nu_2$  and  $\nu_4$  bands respectively, and those obtained by different authors. For  $\nu_4$  (last column of Table 10), we note that our transition dipole moment value is not too different (within about 1-6 %) from previous studies. Aroui et al. (17) gave two different values for the symmetric  $\nu_4$  (s) and antisymmetric  $\nu_4$  (a) transition dipole moments. The theoretical approach those authors used involves only the  $\nu_4$  band, and no Coriolis coupling with the  $2\nu_2$  band was taken into account explicitly, which makes the comparison with our dyad model difficult. In our case, only the intensity parameters corresponding to the transition dipole moment of the  $\nu_4$  (s,a $\leftarrow$ s) band were required. The differences between the (s) and (a) intensity parameters are not found to be significant, as indicated above.

For the  $2\nu_2$  (s $\leftarrow$ a) component (second column of Table 10), the only other experimental values available for comparison are from Urban et al. (15) who used only 10 transition measurements for this component to fit the dipole moment transition. Their value is about 11 % larger than ours. For the transition dipole moment matrix element of the  $2\nu_2$  (a $\leftarrow$ s) component (first column of Table 10), our value is the first one obtained from direct (experimental intensities) measurements. The value of the transition dipole moment listed in Ref. (15) involves a mixing coefficient analysis in energy and some consideration about the ratio of the  $\nu_2$  and  $2\nu_2$  transition dipole moment. Urban et al. (15) obtained a value about 10 times higher than ours and an opposite sign (relative to the other components). Finally, the ab initio values from Pracna et al. (33) are in fairly good agreement with ours.

Table 11 summarizes the comparison between the values we obtained for the bandstrengths and values from earlier literature. We are in good agreement with the bandstrength of the  $\nu_4$  band obtained from experimental measurements by Aroui et al. (17) and in reasonable agreement with the average of the values obtained in the low resolution studies (19-22). Also, we can calculate from Eq. (7) the bandstrength obtained by Urban et al. (15) using his values of the vibrational transition moment matrix element. Although they used 10 relatively unperturbed transitions for evaluating the  $\nu_4$  transition dipole moment, their values are not far from ours.

The energy and intensity parameters are also used to generate a line-by-line frequency and intensity prediction of  $^{14}\text{NH}_3$  of the  $2\nu_2/\nu_4$  system for all the transitions with  $J = 15$ , with an intensity cut-off of  $1.0 \times 10^{-5} \text{ cm}^{-2}\text{atm}^{-1}$  at 296 K, which is sufficient for planetary purposes. A comparison of observed and calculated spectra is shown in Fig. 4. In the top panel, the calculated spectrum is based on the line parameters in the HITRAN database (37) while the bottom panel shows the same interval calculated with the present results. This complete data file is available from the authors.

### V. First application to planetary spectra analysis

As a preliminary illustration, the present prediction was used for a calculation of a synthetic spectrum of Jupiter at 4.8-5.5  $\mu\text{m}$ . The 5  $\mu\text{m}$  region of Jupiter's spectrum includes absorptions by  $\text{CH}_4$ ,  $\text{H}_2\text{O}$ ,  $\text{NH}_3$ ,  $\text{PH}_3$ ,  $\text{GeH}_4$ ,  $\text{CH}_3\text{D}$ , as well as a continuum  $\text{H}_2$ -He and cloud opacity. Further details of the modeling can be found in Ref. (2).

In Fig. 5 (solid line), two synthetic spectra are compared, calculated respectively with the  $^{14}\text{NH}_3$  spectroscopic line list of Lellouch et al. (3), and the one resulting from the present study, all other parameters being fixed. Using the data of this study results in less absorption in several  $\text{NH}_3$  lines, especially at 5.13  $\mu\text{m}$  ( $1950 \text{ cm}^{-1}$ ), 5.16  $\mu\text{m}$  ( $1940 \text{ cm}^{-1}$ ), 5.21  $\mu\text{m}$  ( $1920 \text{ cm}^{-1}$ ), and in the Q-branch of the  $2\nu_2$  ( $a \leftarrow s$ ) band centered at 5.31  $\mu\text{m}$  ( $1882 \text{ cm}^{-1}$ ). In contrast, the continuum longward of 5.4  $\mu\text{m}$  is lowered, since the new line list includes more weak lines than those of (3).

These differences warrant a reinterpretation of the planetary spectra, and in particular of the high quality ISO-SWS observations acquired in 1997. Such a task will be presented elsewhere, but preliminary simulations indicate that, compared to the results presented in Ref. (2), the  $\text{NH}_3$  mixing ratio in Jupiter's atmosphere should be increased by a factor of 1.6 at 2 bar, smoothly reducing to 1.1 at 4 bar and higher pressures (Fig. 5, dashed line). This already illustrates the importance of an accurate  $\text{NH}_3$  line list.

## VI. CONCLUSION

Our theoretical approach to treat the  $2\nu_2/\nu_4$  system as a dyad in interaction isolated from the  $\nu_2$ ,  $3\nu_2$  and  $\nu_2+\nu_4$  bands has allowed us to reproduce the line positions and intensities reasonably well up to  $J = 15$ . This approximation is validated by the present work which required a relatively small number of parameters in energy and intensity to achieve a reasonable agreement with the high resolution infrared spectra. However, as is usually the case, we do not expect predictions arising from this effort to extrapolate to much higher values of the quantum numbers; at some point accidental degeneracies with the higher levels of  $3\nu_2$  (s) will require an expanded polyad analysis to be performed.

We have now investigated the inversion-vibration bands of ammonia in three separate vibrational systems between 1200 and 3600  $\text{cm}^{-1}$  using measurements from the same FTS: 5-7  $\mu\text{m}$  (present study), 4  $\mu\text{m}$  (4) and 3  $\mu\text{m}$  (5). Using a polyad system to describe the interactions in each region, we have been able to determine a set of energy and intensity parameters in order to predict the spectral positions and intensities with the accuracy needed for planetary applications that involve the cold atmospheres of the outer planets. To achieve these results, it has been important to perform a simultaneous analysis of both energies and intensities using a comprehensive set of good quality measurements. We have also found some limitations in our approach. In our different studies, we have noticed that the parameters in the  $\nu_2$ ,  $2\nu_2$  and  $3\nu_2$  overtones did not show any convergence. This effect does not seem to appear for  $\nu_4$  and  $2\nu_4$ , and is probably related to the large inversion splitting of the  $\nu_2$  mode. Therefore, the intensity analysis we performed based on the energy parameters helped us to confirm our choice. This approach allows one to study each region independently from others.

Another problem encountered in the infrared studies of  $\text{NH}_3$  is the large number of inversion-vibration bands in interaction. In the 3  $\mu\text{m}$  region for example, we did not include the  $4\nu_2$  and  $2\nu_2+\nu_4$  bands. For  $4\nu_2$  (s), the assignments were too uncertain, and for the  $2\nu_2+\nu_4$ , the band was too weak. To complete the assignments in this region, we are studying the  $\nu_1 \leftarrow \nu_2$ ,  $\nu_3 \leftarrow \nu_2$ ,  $2\nu_4 \leftarrow \nu_2$ ,  $4\nu_2 \leftarrow \nu_2$  and  $2\nu_2+\nu_4 \leftarrow \nu_2$  hot bands in frequency and intensity.

As indicated by the missing lines in Fig. 4, the 5-7  $\mu\text{m}$  region of ammonia will not

be completely characterized without the inclusion of hot bands. Therefore, in addition to the present 5  $\mu\text{m}$  study and to the 4  $\mu\text{m}$   $3\nu_2/\nu_4+\nu_2$  system (4), we are also assigning and modeling the intensities for the  $3\nu_2 \leftarrow \nu_2$  and  $\nu_4+\nu_2 \leftarrow \nu_2$  hot bands. The modelling of exoplanet atmospheres (38) and brown dwarf stars with relatively high temperatures ( $\sim 1000$  K) will probably require consideration of more hot bands of ammonia. For the present, our study of the 5 to 7  $\mu\text{m}$  region can facilitate the initial detection of ammonia in these objects.

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## Figures Captions.

Fig. 1 : Retrieval of positions, intensities and widths using least squares curve fitting in the region of the R (7,0) and R (7,1)  $2\nu_2$  ( $a \leftarrow s$ ) R branch. The lower panel shows the observed and synthetic spectrum overlaid. The upper panel shows the differences between the two spectra digits in percent. The spectrum is recorded at  $0.011 \text{ cm}^{-1}$  resolution using the FTS at Kitt Peak. The path is 433 m cell and the pressure of the  $^{14}\text{NH}_3$  sample is 6.5 Torr at 297.4 K.

Fig. 2 : Interaction blocks in the upper state energy matrix for the  $2\nu_2/\nu_4$  system of  $^{14}\text{NH}_3$ .

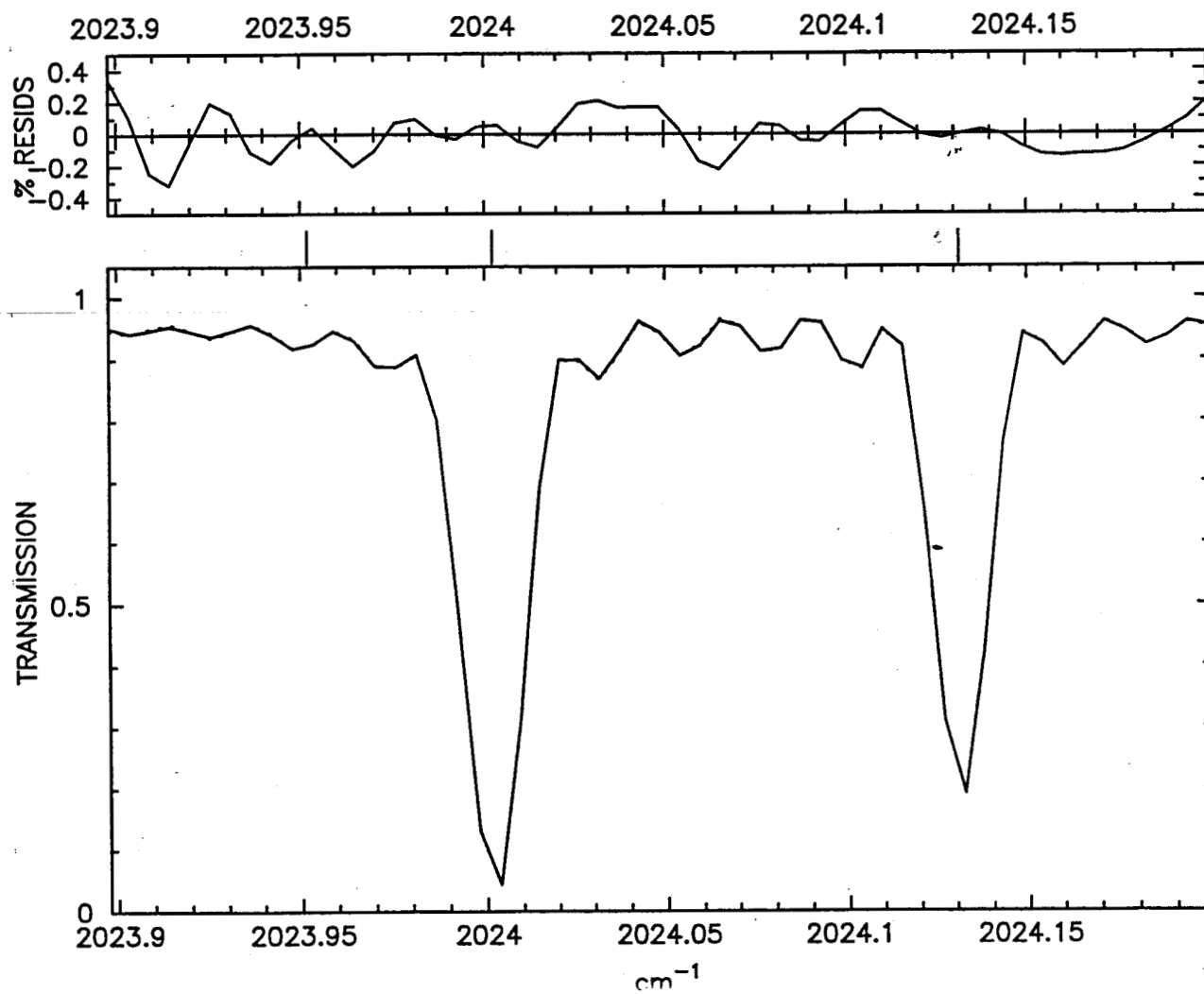
Fig. 3 : Panel A. : Observed-calculated values for the energy levels (in  $10^{-4} \text{ cm}^{-1}$ ) as a function of upper state quantum numbers  $J'$  and  $K'$  for the two components of  $2\nu_2$ .

Panel B. : Observed-calculated values  $[I_{\text{obs}} - I_{\text{calc}} / I_{\text{obs}}] \times 100$  from the intensity fit (in %) as a function of lower state quantum numbers  $J''$  and  $K''$  for the  $^{\text{q}}\text{R}$ ,  $^{\text{q}}\text{Q}$  and  $^{\text{q}}\text{P}$  branches of  $2\nu_2$  ( $s \leftarrow a$ ) component (left panel) and of  $2\nu_2$  ( $a \leftarrow s$ ) component (right panel).

Fig.4 : Comparison of observed and predicted spectra of ammonia. Using an observed Kitt Peak FTS spectrum recorded at  $0.0056 \text{ cm}^{-1}$  resolution with a path of 0.25 m and a pressure of 5.5 Torr at room temperature, the improvement of the prediction is shown. The upper panel shows the observed and synthetic spectra based on the 1996 HITRAN database and the lower panel shows the present results. The features missing in the prediction are generally hot band transitions.

Fig.5 : Comparison between two synthetic spectra of Jupiter calculated with the  $\text{NH}_3$  spectroscopic data of Lellouch et al. (3) (solid line) and of this study (dotted line).

run: j105.4

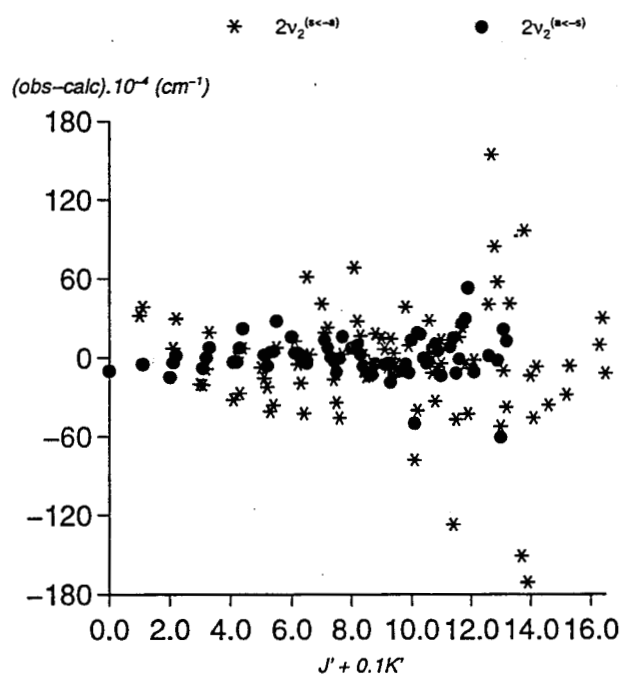




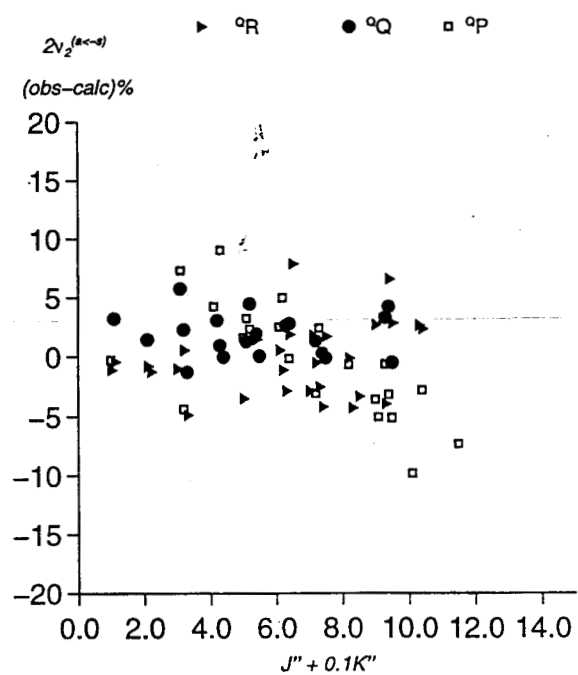
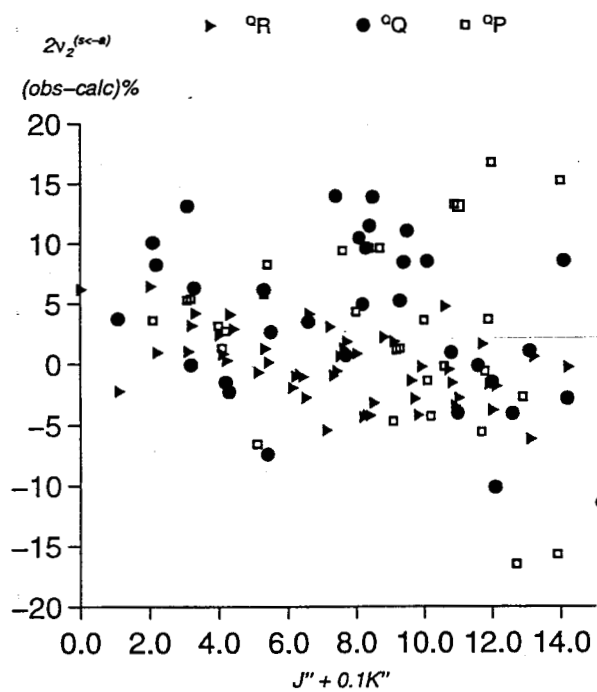
$v_2 = 2; a$  $v_2 = 2; s$  $v_4 = 1; a$  $v_4 = 1; s$ 

$v_2 = 2; a$	Diagonal terms.	"essential" resonances : "k-type" $\Delta K = \pm 3 : q_{3v}$	Coriolis $\Delta v_2 = -2 \Delta v_4 = +1 :$ "Coriolis 2" $\Delta K = \pm 2 \Delta l_4 = \mp 1 : C_2^a$ "Coriolis 4" $\Delta K = \pm 4 \Delta l_4 = \pm 1 : C_4^a$	Coriolis $\Delta v_2 = -2 \Delta v_4 = +1 :$ "Coriolis 1" $\Delta K = \pm 1 \Delta l_4 = \pm 1 :$ $C_1^a, C_{1K}^a, C_{1K1}^a, C_{1J}^a$
$v_2 = 2; s$	Diagonal terms.	Diagonal terms.	Coriolis $\Delta v_2 = -2 \Delta v_4 = +1 :$ "Coriolis 1" $\Delta K = \pm 1 \Delta l_4 = \pm 1 : C_1^s$	Coriolis $\Delta v_2 = -2 \Delta v_4 = +1 :$ "Coriolis 2" $\Delta K = \pm 2 \Delta l_4 = \mp 1 : C_2^s$ "Coriolis 4" $\Delta K = \pm 4 \Delta l_4 = \pm 1 : C_4^s$
$v_4 = 1; a$			Diagonal terms. "essential" resonances : "2, 2" l-type $\Delta K = \pm 2 \Delta l_4 = \pm 2 : q_2^a$ "2, -4" l-type $\Delta K = \pm 4 \Delta l_4 = \mp 2 : f_4^a$	"essential" resonances : "k-type" $\Delta K = \pm 3 : q_{3v}$ "2, -1" l-type $\Delta K = \pm 1 \Delta l_4 = \mp 2 : q_1$
$v_4 = 1; s$				diagonal terms. "essential" resonances : "2, 2" l-type $\Delta K = \pm 2 \Delta l_4 = \pm 2 : q_2^s$ "2, -4" l-type $\Delta K = \pm 4 \Delta l_4 = \mp 2 : f_4^s$

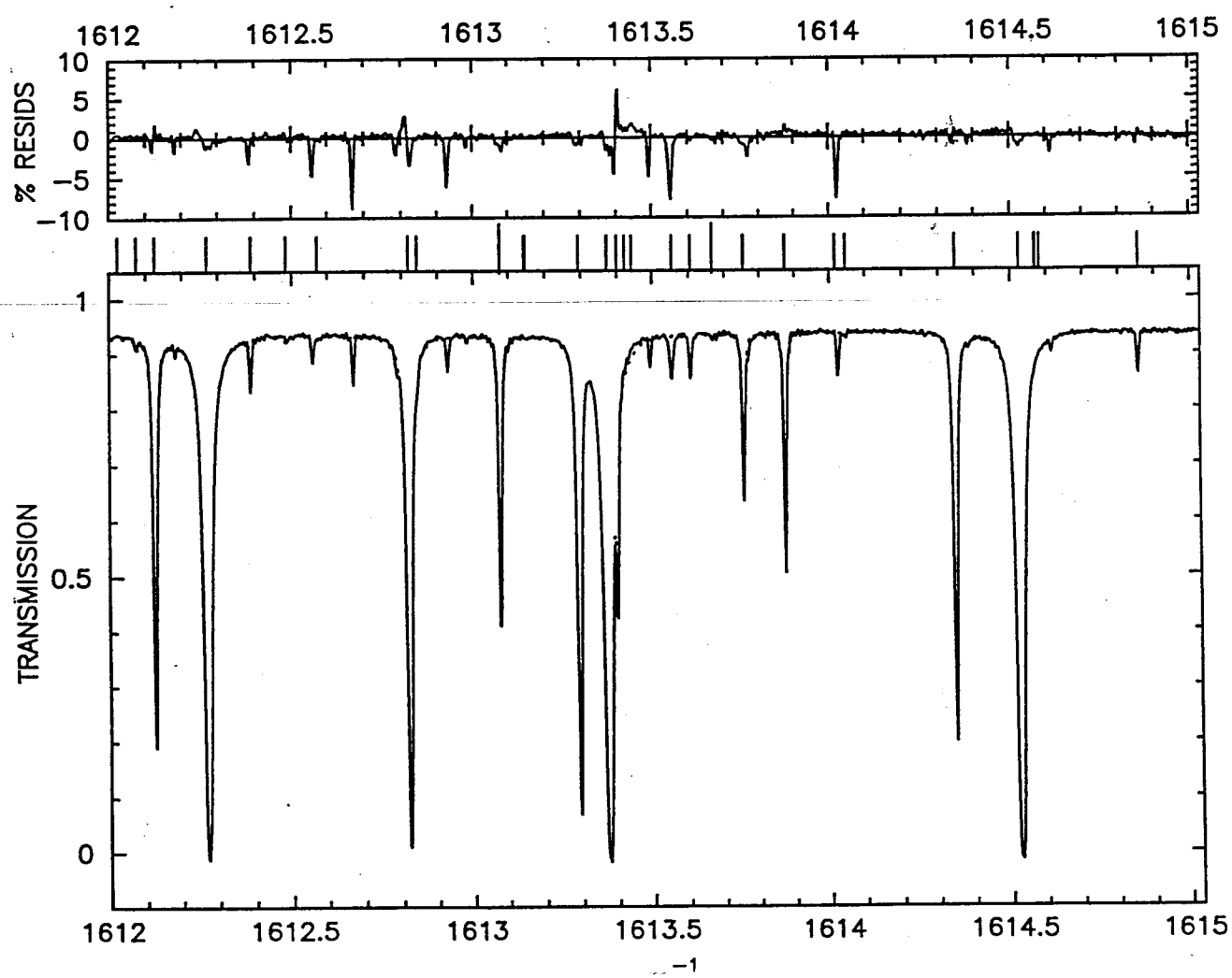
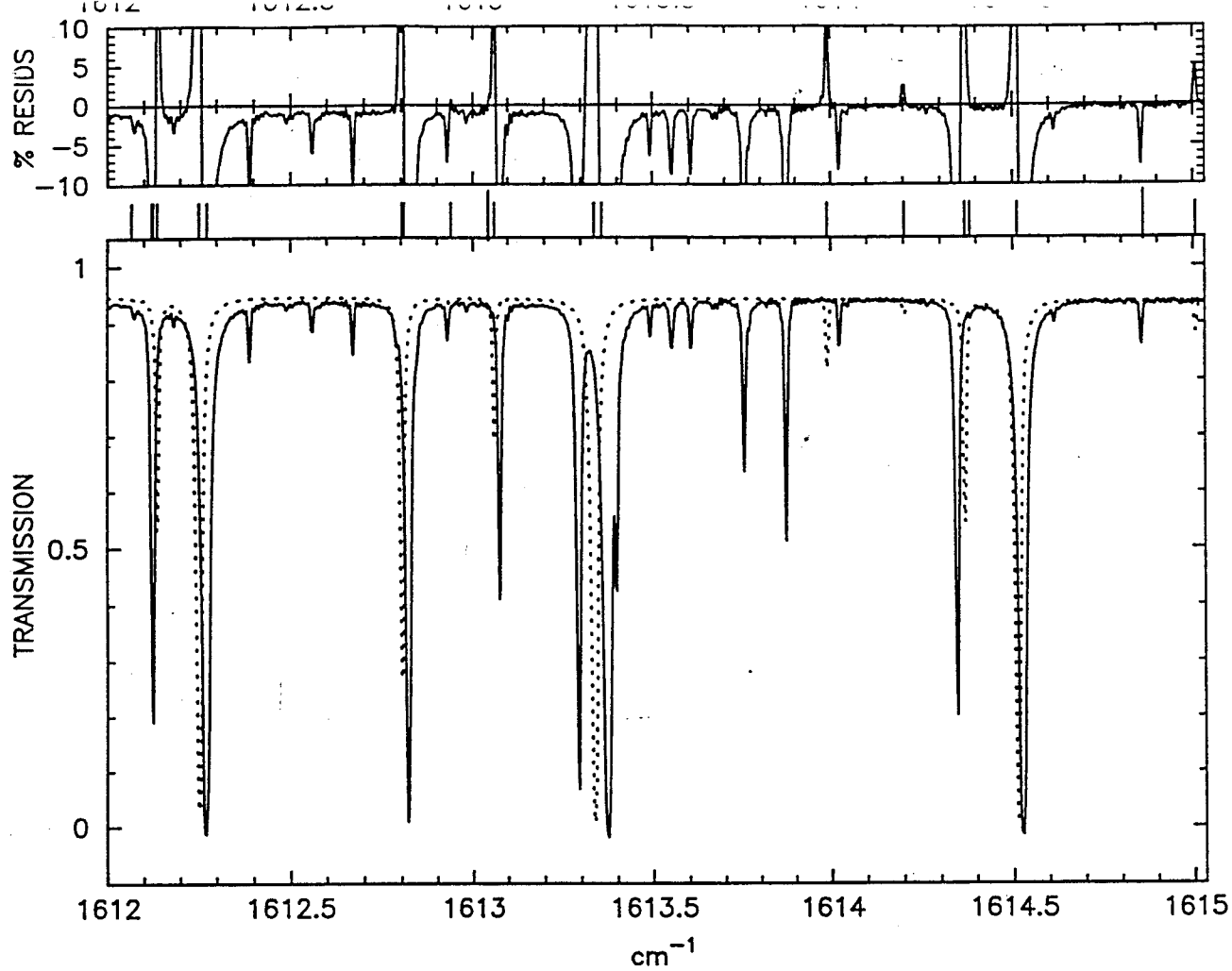
Note : for the non-diagonal elements, only the quantum numbers which are varying are indicated.  
 Only the lowest order parameters of Table III of Ref. (4) and Table 4 of this paper are indicated.

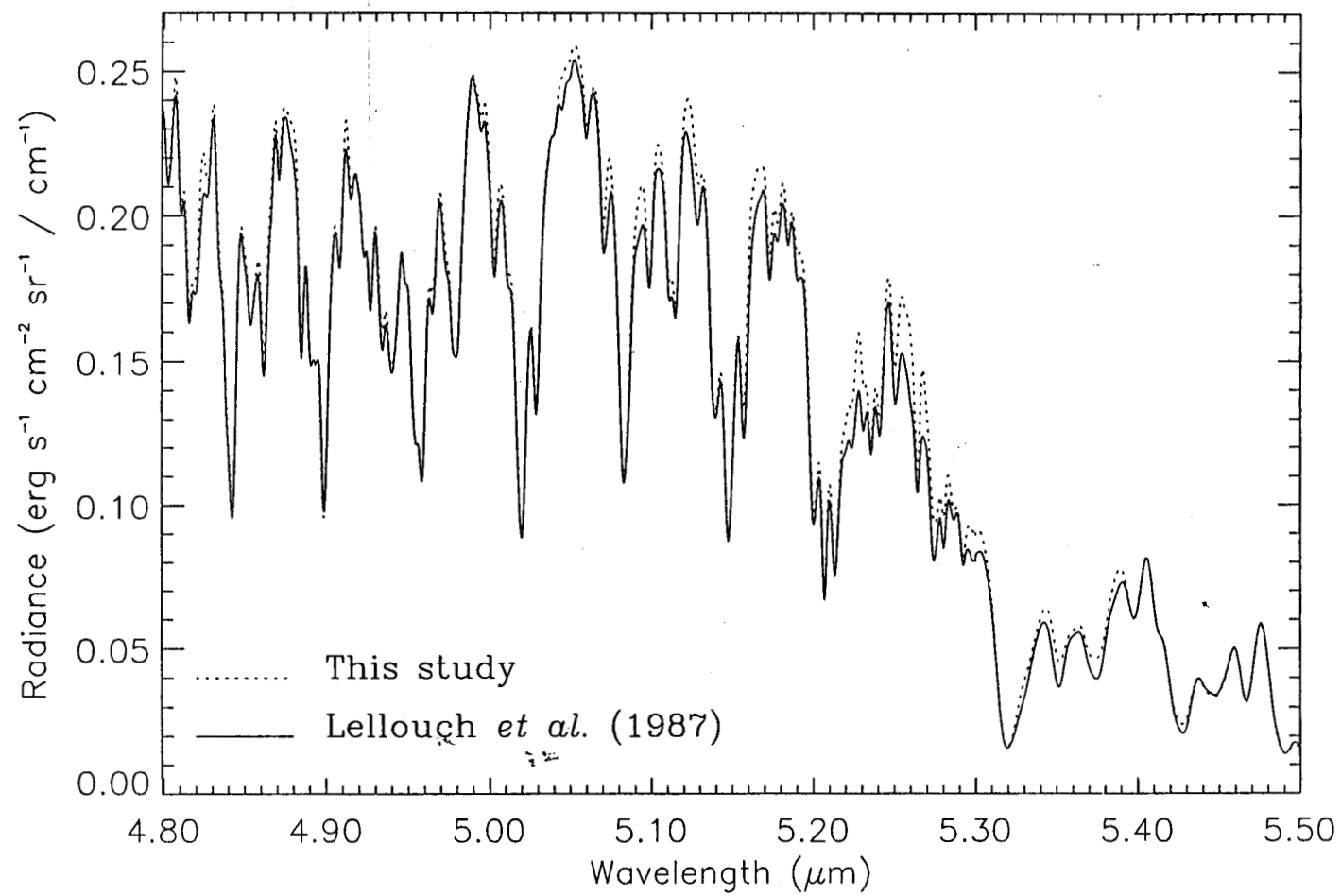


A



B





## Tables Captions.

Table 1. Experimental Conditions of the Ammonia Spectra.

Table 2. Sample of Intensity Measurements for  $\text{NH}_3$  at 6  $\mu\text{m}$ .

Table 3. Comparison of present  $\text{NH}_3$  experimental line intensities to other studies.

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Table 6.c. Coriolis Energy Parameters<sup>a</sup> ( $\text{cm}^{-1}$ ) for the  $2\nu_2/\nu_4$  and  $3\nu_2/\nu_2+\nu_4^b$  systems of  $^{14}\text{NH}_3$ .

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Table 9. Bandstrengths ( $\text{cm}^{-2}\text{atm}^{-1}$ ) for the  $2\nu_2/\nu_4$  bands of  $^{14}\text{NH}_3$  at 296 K.

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Appendix . Experimental Line Intensities in  $2\nu_2$  and  $\nu_4$ .

**Table 1**  
Experimental Conditions of the Ammonia Spectra.

Press. Torr	Path m	Temp. K	Res. cm <sup>-1</sup>
a) Kitt Peak FTS			
9 - 4 $\mu$ m bandpass			
2.21	0.04	296.9	0.0053
4.91	0.04	296.7	0.0053
10.02	0.04	296.3	0.0053
6.27	0.25	299.3	0.0053
2.50	0.25	296.9	0.0053
5.49	0.25	296.9	0.0053
8.40	0.25	299.3	0.0053
10.90	0.25	296.4	0.0053
19.85	0.25	296.2	0.0053
11.73	8.35	295.0	0.0106
4.53	8.35	295.0	0.0106
9.96	24.40	295.0	0.0106
19.78	24.40	295.0	0.0106
6 - 2 $\mu$ m bandpass:			
2.60	1.50	294.6	0.0114
1.05	25.00	295.0	0.0114
6.20	25.00	297.7	0.0114
6.50	433.00	297.4	0.0114
b) JPL BRUKER FTS			
6 - 5 $\mu$ m bandpass:			
9.61	0.10	296.3	0.006
1.80	0.80	295.8	0.006
2.60	0.80	296.2	0.006
5.30	0.80	295.7	0.006
15.2	0.80	296.0	0.006

**Table 2**  
Sample of intensity measurements for NH<sub>3</sub> at 6 μm.

Position. cm <sup>-1</sup>	obs-av 10 <sup>-3</sup> .cm <sup>-1</sup>	Intensity cm <sup>-2</sup> /atm	% ob-av	Path m	Press. Torr	Temp. K
1532.450173	-0.37	1.262	1.2	0.040	2.22	296.9
1532.450347	-0.20	1.232	-1.2	0.040	4.91	296.7
1532.451109	0.57	1.248	0.1	0.040	10.02	296.3
**1532.450543	0.41 **	1.248	1.0 **			
1494.242028	-0.08	1.086E-01	2.5	0.040	10.02	296.3
1494.242046	-0.06	1.070E-01	0.9	0.040	4.91	296.7
1494.242104	0.00	1.081E-01	2.0	0.250	2.50	296.9
1494.242110	0.00	1.103E-01	4.1	0.040	2.22	296.9
1494.242114	0.01	1.011E-01	-4.7	0.250	6.27	299.3
1494.242120	0.01	1.072E-01	1.2	0.250	5.49	296.9
1494.242139	0.03	9.759E-02	-7.9	0.250	8.40	299.3
1494.242147	0.04	1.070E-01	1.0	0.250	19.85	296.2
1494.242151	0.04	1.070E-01	0.9	0.250	10.90	296.4
**1494.242107	0.04 **	1.060E-01	3.6 **			
1596.895958	-0.24	5.592E-02	-4.3	0.102	9.60	296.0
1596.896059	-0.14	6.067E-02	3.8	0.040	2.22	296.9
1596.896157	-0.04	5.770E-02	-1.3	0.040	4.91	296.7
1596.896162	-0.04	5.898E-02	0.9	0.250	2.50	296.9
1596.896224	0.02	5.917E-02	1.2	0.250	5.49	296.9
1596.896325	0.13	5.798E-02	-0.8	0.250	10.90	296.4
1596.896325	0.13	5.803E-02	-0.7	0.250	19.85	296.2
1596.896385	0.19	5.919E-02	1.3	0.040	10.02	296.3
**1596.896199	0.14 **	5.845E-02	2.2 **			
1631.765631	-0.20	4.144E-03	0.6	0.80	1.80	296.0
1631.765641	-0.19	4.278E-03	3.9	0.80	2.60	296.0
1631.765731	-0.10	3.838E-03	-6.8	8.35	4.53	295.0
1631.765767	-0.06	4.008E-03	-2.7	0.80	15.22	296.0
1631.765771	-0.06	4.168E-03	1.2	0.80	5.30	296.0
1631.766018	0.19	4.014E-03	-2.5	0.250	19.85	296.2
1631.766037	0.21	4.158E-03	0.9	0.250	5.49	296.9
1631.766054	0.22	4.346E-03	5.5	0.250	10.90	296.4
**1631.765831	0.17 **	4.119E-03	3.7 **			
1871.342279	-0.34	8.238E-04	0.1	25.0	1.050	295.0
1871.342500	-0.12	8.035E-04	-2.3	8.35	4.530	295.0
1871.342646	0.02	8.323E-04	1.1	24.4	9.960	295.0
1871.342652	0.03	8.111E-04	-1.4	8.35	11.735	295.0
1871.343029	0.41	8.437E-04	2.5	24.4	19.780	295.0
**1871.342621	0.24 **	8.229E-04	1.7 **			
2029.664025	-0.32	1.767E-04	4.3	433.0	6.50	297.4
2029.664062	-0.28	1.667E-04	-1.6	25.0	6.20	297.7
2029.664087	-0.26	1.702E-04	0.5	24.4	9.96	295.0
2029.664662	0.32	1.635E-04	-3.5	8.35	11.74	295.0
2029.664891	0.55	1.700E-04	0.3	24.4	19.78	295.0
**2029.664345	0.36 **	1.694E-04	2.6 **			
2062.217767	-0.26	7.230E-05	2.7	24.4	9.96	295.0
2062.217980	-0.05	7.351E-05	4.4	433.0	6.50	297.4
2062.218025	-0.01	6.762E-05	-4.0	25.0	6.20	297.7
2062.218356	0.32	6.825E-05	-3.1	24.4	19.78	295.0
**2062.218032	0.21 **	7.042E-05	3.6 **			

\*\* indicates the averaged values.  
Individual and averaged intensities are in normal abundance at 296 K.

Table 3

Comparison of present NH<sub>3</sub> experimental line intensities to other studies.

	Urban et al. (15)	Lellouch et al. <sup>+</sup> (3)	Urban et al. <sup>++</sup> (16)	Aroui et al. (17)	Kralik et al. (18)
Instrument	TDL (NASA Langley)	FTS (Orsay)	FTS (Kitt Peak)	FTS (Bruker)	TDL
Spectral range (cm <sup>-1</sup> )	1581-1595	1800-2100	1485-1530	1474-1595	1793-1810
Type of transitions	<sup>Q</sup> Q of 2ν <sub>2</sub> (s←a) allowed of ν <sub>4</sub>	allowed of 2ν <sub>2</sub> and ν <sub>4</sub>	<sup>O</sup> P and <sup>S</sup> P of ν <sub>4</sub>	<sup>P</sup> P of ν <sub>4</sub>	R of ν <sub>4</sub>
Number of line : intensities reported	20	750	23	60	16
# lines in common with present study	16	294	12	51	16
mean intensity ratio (other/present)	1.007	0.969	0.134	0.970	0.822
rms of ratio (other/present)	6.8 %	10.2 %	127. %	9.1 %	14.5
range of ratio (other/present)	0.91 to 1.14	0.25 to 1.25	0.054 to 0.187	0.76 to 1.122	0.636 to 1.022

<sup>+</sup> Some 20 measurements of Lellouch et al. (3) differed by more than 25% from present values and were therefore omitted from consideration.

<sup>++</sup> If two measurements are excluded from the comparison, the mean ratio becomes 0.060 +/- 6.8% for Urban et al. (16) thus indicating some systematic problems with their reported values.



**Table 4**

Upper state energy matrix<sup>a</sup> for the  $2\nu_2/\nu_4$  system of  $^{14}\text{NH}_3$ .

Diagonal<sup>b, c</sup>

$$\begin{aligned} \langle i, v, l_4; J, K | i, v, l_4; J, K \rangle = & v_v^i + B_v^i J(J+1) + (C_v^i - B_v^i) K^2 - D_v^{J,i} J^2(J+1)^2 - D_v^{JK,i} J(J+1) K^2 \\ & - D_v^{K,i} K^4 + H_v^{J,i} J^3(J+1)^3 + H_v^{JK,i} J^2(J+1)^2 K^2 + H_v^{K,i} J(J+1) K^4 + H_v^{K,i} K^6 - 2(C\xi_4)_v^i K l_4 \\ & + \eta_v^{J,i} J(J+1) K l_4 + \eta_v^{K,i} K^3 l_4 + \chi^{J,i} J^2(J+1)^2 K l_4 + \chi^{JK,i} J(J+1) K^3 l_4 + \chi^{K,i} K^5 l_4 \end{aligned}$$

essential resonances<sup>b, c</sup>

$$\langle \begin{smallmatrix} s \\ a \end{smallmatrix}, v, l_4; J, K | \begin{smallmatrix} a \\ s \end{smallmatrix}, v, l_4; J, K \pm 3 \rangle = F_3^\pm(J, K) q_{3v} (2K \pm 3)$$

$$\langle \begin{smallmatrix} s \\ a \end{smallmatrix}, 1, \pm 1; J, K | \begin{smallmatrix} a \\ s \end{smallmatrix}, 1, \mp 1; J, K \pm 1 \rangle = (2K \pm 1) F_1^\pm(J, K) [q_1 + q_{1J} J(J+1) + q_{1K} (2K \pm 1)^2]$$

$$\langle i, 1, \mp 1; J, K | i, 1, \pm 1; J, K \pm 2 \rangle = F_2^\pm(J, K) [q_2^i + q_{2J}^i J(J+1) + q_{2K}^i (2K \pm 2)^2]$$

$$\langle i, 1, \pm 1; J, K | i, 1, \mp 1; J, K \pm 4 \rangle = F_4^\pm(J, K) f_4^i$$

Coriolis-type coupling<sup>b, c</sup>

$$\langle s, 2, 0, 0; J, K | a, 1, \pm 1; J, K \pm 1 \rangle = F_1^\pm(J, K) [c_1^s + c_{1J}^s J(J+1) \mp c_{1K1}^s (2K \pm 1) + c_{1K2}^s (2K \pm 1)^2 + c_{1KJ}^s (2K \pm 1) J(J+1)]$$

$$\langle a, 2, 0, 0; J, K | s, 1, \pm 1; J, K \pm 1 \rangle = F_1^\pm(J, K) [c_1^a + c_{1J}^a J(J+1) \mp c_{1K1}^a (2K \pm 1) + c_{1K2}^a (2K \pm 1)^2 + c_{1KJ}^a (2K \pm 1) J(J+1)]$$

$$\langle i, 2, 0, 0; J, K | i, 1, \mp 1; J, K \pm 2 \rangle = \pm F_2^\pm(J, K) [c_2^i + c_{2J}^i J(J+1) \pm c_{2K}^i (2K \pm 2)]$$

---


$$F_1^\pm(J, K) = [J(J+1) - K(K \pm 1)]^{1/2}; F_2^\pm(J, K) = F_1^\pm(J, K) F_1^\pm(J, K \pm 1); \dots$$


---

<sup>a</sup> The elements are given according to the phase conventions of Ref. (36) and obey  $\langle i', v'; J, K' | i, v; J, K \rangle = \langle i, v; J, K | i', v'; J, K' \rangle$ . The quantum number M is omitted throughout the Table.

<sup>b</sup> The set  $(2\nu_2, \nu_4)$  equal to  $(2, 0)$  and  $(0, 1)$  for the upper states of  $2\nu_2$  and  $\nu_4$  respectively.

<sup>c</sup> In all elements  $\langle i, \dots | i, \dots \rangle = \dots$ , the index i represents s or a.

**Table 5**  
Statistics for Fitted Line Positions and Intensities<sup>a</sup>.

	A) Fit of line positions <sup>a</sup>		B) Fit of the line intensities <sup>a</sup>	
	Number of lines	rms (cm <sup>-1</sup> )	Number of lines	rms (%)
2v <sub>2</sub>	403	0.0031	254	4.1
s←a,s	262	0.0037	142	5.0
a←s,a	141	0.0014	112	3.0
v <sub>4</sub>	1663	0.0034	927	4.9
s←s,a	886	0.0030	501	5.0
a←a,s	777	0.0038	426	4.8
vibrationally mixed	48	0.0032	22	5.5
Global Fit	2114	0.0034	1203	4.7
Number of parameters	57		16	

<sup>a</sup>The results include for each band, all the transitions going up successively to "s" or "a" upper state components. The two inversion parities of the lower state indicate symmetry allowed (listed first) and "perturbation-allowed" (listed second) transitions respectively.

**Table 6.a**  
Energy Parameters<sup>a</sup> (cm<sup>-1</sup>) for the Ground State<sup>b</sup> and the  $\nu_2^b$ ,  $2\nu_2$  and  $3\nu_2^c$  Overtones of  $^{14}\text{NH}_3$ .

	GS (s) <sup>b</sup>	GS (a-s) <sup>b</sup>	$\nu_2$ (s) <sup>b</sup>	$\nu_2$ (a-s) <sup>b</sup>	$2\nu_2$ (s)	$2\nu_2$ (a-s)	$3\nu_2$ (s) <sup>c</sup>	$3\nu_2$ (a-s) <sup>c</sup>
1) diagonal								
$\nu$	0.	0.79340312(95)	932.4338787(98)	35.6881062(32)	1597.470(27)	284.709(45)	2384.1477(57)	511.3652(69)
$B_\nu$	9.94664268(75)	-0.00503222(68)	10.07017463(94)	-0.18015883(52)	10.31255(30)	-0.63624(44)	9.49981(29)	-0.30293(25)
$C_\nu$	6.2275052(24)	0.00200029(17)	6.0883088(27)	0.0715169(14)	5.93597(16)	0.23464(34)	6.19169(39)	0.10411(28)
$D_\nu^J \times 10^3$	0.849460(41)	-0.0167810(20)	1.130565(26)	-0.434232(21)	0.4800(27)	-0.2029(57)	-0.2639(42)	0.0086(19)
$D_\nu^{JK} \times 10^3$	-1.578093(98)	0.0463532(50)	-2.422446(82)	1.189134(68)	-0.5722(64)	0.451(14)	1.282(10)	-0.0846(36)
$D_\nu^K \times 10^3$	0.91383(11)	-0.0317569(41)	1.52044(11)	-0.806754(57)	0.1828(46)	-0.2137(89)	-0.9440(78)	0.1198(36)
$H_\nu^J \times 10^6$	0.25914(51)	-0.038549(24)	0.55533(40)	-0.61772(38)	-0.644(12)	0.345(30)	-0.500(18)	fixed <sup>d</sup>
$H_\nu^{JK} \times 10^5$	-0.09056(19)	0.0158387(73)	-0.22281(16)	0.24660(14)	0.2894(50)	-0.192(11)	0.1744(60)	fixed <sup>d</sup>
$H_\nu^{KJ} \times 10^5$	0.10796(26)	-0.0214917(82)	0.29346(29)	-0.32402(21)	-0.4215(72)	0.288(14)	-0.2035(72)	fixed <sup>d</sup>
$H_\nu^K \times 10^5$	-0.04151(20)	0.0096701(49)	-0.12455(21)	0.140103(92)	0.2035(33)	-0.1378(63)	0.0780(36)	fixed <sup>d</sup>
2) essential								
$q_{3\nu} \times 10^3$	0.105(43)	0.	0.13266(11)	0.	-0.1496(26)	0.	-0.278(26)	0.

<sup>a</sup>The quoted errors represent three standard deviation. For each band, the column "s" and "a-s" give the value of  $\nu^s$ ,  $B_\nu^s$ , ... and  $\nu^a - \nu^s$ ,  $B_\nu^a - B_\nu^s$ , ... respectively.

<sup>b</sup>Values determined in Ref. (8).

<sup>c</sup>Values determined in Ref. (4).

<sup>d</sup>Fixed to the ground state values determined in Ref. (8).

Table 6.0

Energy Parameters<sup>a</sup> (cm<sup>-1</sup>) for the  $\nu_4$ ,  $\nu_2+\nu_4$ <sup>b</sup> and  $2\nu_4$ <sup>c</sup> of <sup>14</sup>NH<sub>3</sub>.

	$\nu_4$ (s)	$\nu_4$ (a-s)	$\nu_2+\nu_4$ (s) <sup>b</sup>	$\nu_2+\nu_4$ (a-s) <sup>b</sup>	$2\nu_4$ (s) <sup>c</sup>	$2\nu_4$ (a-s) <sup>c</sup>
1) diagonal						
$\nu$	1626.2758(13)	1.0986(17)	2540.5287(33)	45.6030(48)	3228.42(18)	1.45(3)
$B_\nu$	10.184388(60)	-0.01774(18)	10.31504(12)	-0.21041(18)	10.413(1)	-0.0575(9)
$C_\nu$	6.169283(64)	0.00297(5)	6.01800(15)	0.090039(22)	6.099(2)	fixed <sup>d</sup>
$D_\nu^J \times 10^3$	1.02494(75)	-0.02200(28)	1.3122(11)	-0.4593(14)	1.28(2)	fixed <sup>d</sup>
$D_\nu^{JK} \times 10^3$	-1.9680(18)	0.0844(12)	-2.7747(69)	1.2625(87)	-2.54(6)	fixed <sup>d</sup>
$D_\nu^K \times 10^3$	1.1270(12)	-0.06430(95)	1.6843(75)	-0.8674(78)	1.45(3)	fixed <sup>d</sup>
$H_\nu^J \times 10^6$	0.3547(19)	fixed <sup>d</sup>	Fixed <sup>d</sup>	fixed <sup>d</sup>	fixed <sup>d</sup>	fixed <sup>d</sup>
$H_\nu^{JK} \times 10^5$	-0.1205(11)	fixed <sup>d</sup>	Fixed <sup>d</sup>	fixed <sup>d</sup>	fixed <sup>d</sup>	fixed <sup>d</sup>
$H_\nu^{KJ} \times 10^5$	0.1406(15)	fixed <sup>d</sup>	Fixed <sup>d</sup>	fixed <sup>d</sup>	fixed <sup>d</sup>	fixed <sup>d</sup>
$H_\nu^K \times 10^5$	-0.05407(76)	fixed <sup>d</sup>	Fixed <sup>d</sup>	fixed <sup>d</sup>	fixed <sup>d</sup>	fixed <sup>d</sup>
$(C\zeta_4)_\nu$	-1.51999(10)	0.	-1.30276(51)	-0.18416(48)	-1.373(2)	-0.033(3)
$\eta_\nu^J \times 10^2$	-0.25682(94)	0.	-0.2111(30)	-0.1527(19)	0.	0.28(2)
$\eta_\nu^K \times 10^2$	0.20326(94)	0.	0.1184(33)	0.1964(26)	0.	-0.37(2)
2) essential						
$q_{3\nu} \times 10^3$	0.1465(36)	-	-0.2258(33)	-	fixed <sup>d</sup>	0.
$q_1 \times 10^1$	-1.2282(15)	-	1.1074(26)	-	0.137(6)	
$q_{1J} \times 10^4$	0.8753(58)	-	-1.316(26)	-	0.	0.
$q_{1K} \times 10^5$	-1.957(20)	-	6.36(44)	-	0.	0.
$q_2 \times 10^1$	1.54214(36)	-0.1028(16)	1.24686(90)	0.17438(78)	0.827(6)	0.156(3)
$q_{2J} \times 10^4$	-0.7988(30)	0.	-0.8220(84)	0.	-0.93(6)	
$q_{2K} \times 10^4$	0.	0.	-0.632(34)	0.		-0.21(6)
$f_4 \times 10^5$	1.729(26)	0.	1.718(66)	0.44(10)		

<sup>a</sup>The quoted errors represent three standard deviation. For each band, the column "s" and "a-s" give the value of  $\nu^s$ ,  $B_\nu^s$ , ... and  $\nu^a - \nu^s$ ,  $B_\nu^a - B_\nu^s$ , ... respectively.

<sup>b</sup>Values determined in Ref. (4).

<sup>c</sup>Values determined in Ref. (5).

<sup>d</sup>Fixed to the ground state values determined in Ref. (8).

**Table 6.c**  
Coriolis Energy Parameters<sup>a</sup> (cm<sup>-1</sup>) for the 2ν<sub>2</sub>/ν<sub>4</sub> and 3ν<sub>2</sub>/ν<sub>2</sub>+ν<sub>4</sub><sup>b</sup> Systems of <sup>14</sup>NH<sub>3</sub>.

		2ν <sub>2</sub> /ν <sub>4</sub> (s)	2ν <sub>2</sub> /ν <sub>4</sub> (a-s)	3ν <sub>2</sub> /ν <sub>4</sub> <sup>b</sup> (s)	3ν <sub>2</sub> /ν <sub>4</sub> <sup>b</sup> (a-s)
3) Coriolis					
C <sub>1</sub>		-1.352(19)	0.	-	-
C <sub>1K1</sub>	× 10 <sup>2</sup>	-0.723(15)	1.389(22)	-	-
C <sub>1K2</sub>	× 10 <sup>3</sup>	-0.6181(38)	0.	-	-
C <sub>1J</sub>	× 10 <sup>3</sup>	1.3683(50)	0.	-	-
C <sub>1JK</sub>	× 10 <sup>5</sup>	-0.618(29)	0.	-	-
C <sub>2</sub>	× 10 <sup>2</sup>	2.006(17)	-1.270(42)	1.158(66)	0.
C <sub>2J</sub>	× 10 <sup>5</sup>	-0.95(13)	0.	-	-

<sup>a</sup>The quoted errors represent three standard deviation. For each band, the column "s" and "a-s" give the value of ν<sup>s</sup>, B<sub>v</sub><sup>s</sup>, ... and ν<sup>a</sup>-ν<sup>s</sup>, B<sub>v</sub><sup>a</sup>-B<sub>v</sub><sup>s</sup>, ... respectively.

<sup>b</sup>values determined in Ref. (4).

Table 7

Statistics for Fitted perturbation-allowed transitions for the  $2\nu_2$  and  $\nu_4$  System.

Bands	Perturbation-allowed Transitions	Notation <sup>a</sup>	Number of Line Positions (Intensities) Fitted	RMS	
				Position (cm <sup>-1</sup> )	Intensity (%)
$\nu_4$	$\Delta K = \pm 2$ a $\leftarrow$ s, s $\leftarrow$ a	"O", "S"	667 (239)	0.0023	6.5
$2\nu_2$	$\Delta K = \pm 3$ a $\leftarrow$ a, s $\leftarrow$ s	"N", "T"	65 (11)	0.0025	7.0
$\nu_4$	$\Delta K = 0$ a $\leftarrow$ s, s $\leftarrow$ a	"Q"	59 (19)	0.0025	6.5
$2\nu_2$	$\Delta K = \pm 1$ a $\leftarrow$ a, s $\leftarrow$ s	"R", "P"	16 (3)	0.0029	7.2

<sup>a</sup> the notation O, S, N, T, Q, P and R is related to the variation of the K quantum number : O stands for  $\Delta K = -2$ , S for  $\Delta K = +2$ , N for  $\Delta K = -3$ , T for  $\Delta K = +3$ , Q for  $\Delta K = 0$ , P for  $\Delta K = -1$  and R for  $\Delta K = +1$ .

**Table 8**  
Intensity Parameters<sup>1</sup> (D) for the  $2\nu_2/\nu_4$  System of  $^{14}\text{NH}_3$ .

		$2\nu_2$		$\nu_4$
		$d^s$	$d^a - d^s$	$d^s = d^{a^2}$
$d_0$		0.004605(50)	0.02419(30)	
$d_{01}$	$\times 10^3$	-0.300(14)	-0.662(38)	
$d_{02}$	$\times 10^4$	-0.167(17)	0. <sup>2</sup>	
$d_{03}$	$\times 10^4$	-0.175(14)	-0.280(54)	
$d_{04}$	$\times 10^4$	0.255(19)	0.516(96)	
$d_1$				0.08408(34)
$d_{11}$	$\times 10^2$			-0.5782(37)
$d_{12}$	$\times 10^2$			0.2609(23)
$d_{15}$	$\times 10^4$			0.143(18)
$d_{16}$	$\times 10^4$			-0.331(26)
$d_{17}$	$\times 10^2$			-0.1100(13)
$d_{18}$	$\times 10^4$			-0.148(19)

<sup>1</sup> $d_0^s, d_{01}^s, d_1^s, \dots$  are related to transitions from ground state  $s$  levels ;  $d_0^a, d_{01}^a, d_1^a, \dots$  are related to transitions from ground state  $a$  levels. The signs of intensity parameters are correlated to those of the energy parameters given in Table IV in Ref. (4). The quoted errors represent three standard deviation.

<sup>2</sup>The differences  $d^a - d^s$  were not found to be significant and were set to zero.

**Table 9**  
Bandstrengths in ( $\text{cm}^{-2} \text{ atm}^{-1}$ ) for the  $2\nu_2/\nu_4$  Bands of  $^{14}\text{NH}_3$  at 296 K.

	Number of transitions <sup>1</sup>	$F_{\min}^1$	$F_{\max}^1$	Band Centers ( $\text{cm}^{-1}$ )	Bandstrengths $S_v(\text{int})^2$	(present work) $S_v^0$
$S_v^s (2\nu_2 a \leftarrow s)$	284	1402.924	2134.438	1882.179(5)	0.145(7)	0.201(5)
$S_v^a (2\nu_2 s \leftarrow a)$	598	1272.381	1949.798	1597.470(3)	7.2(4)	6.68(24)
$S_v (\nu_4 s \leftarrow s)$	1345	1253.847	2035.501	1626.276(1)	57.(3)	116.(3) <sup>3</sup>
$S_v (\nu_4 a \leftarrow a)$	1216	1256.098	2019.033	1627.375(2)	52.(3)	
vibrational mixed	249	1335.398	1977.357		0.55(3)	
<hr/>						
Total	3692	1253.847	2134.438		117(6)	123 (3)
<hr/>						

<sup>1</sup>Number of transitions and frequency limits used to calculate the integrated vibrational bandstrength  $S_v(\text{int})$ .

<sup>2</sup> $S_v(\text{int})$  : integrated vibrational bandstrength  $\sum_i S_i$  with 5 % of precision.

<sup>3</sup> $S_v = (S_v^s + S_v^a)$ .



**Table 10**

Comparison of Transition dipole moment matrix elements (Debye) from the present work and from the literature for the  $2\nu_2^s$ ,  $2\nu_2^a$  and  $\nu_4$  bands of  $^{14}\text{NH}_3$ .

$$\langle 0^s, 0^0 | \mu_z | 2^a, 0^0 \rangle \quad \langle 0^a, 0^0 | \mu_z | 2^s, 0^0 \rangle \quad \langle 0^i, 0^0 | \mu_x | 0^0, 1_{\pm}^1 \rangle$$

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High Resolution Measurements:

Present work (1203 lines)	0.003256(35)	0.02036(25)	0.04203(17)
Urban et al. (15) <sup>1</sup> (40 lines)		0.02261(21)	0.04247(84)
Aroui et al. (17) (57 lines)		-	0.0420(15) $\nu_4^s$ 0.0394(21) $\nu_4^a$

Calculations:

Pracna et al. (33) <sup>2</sup>	0.007	0.027	0.044(1) <sup>3</sup>
Urban et al. (15) <sup>4</sup>	-0.031(16)		

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<sup>1</sup> Observed values correspond to fit I (best fit) in Table IV of Ref. (15).

<sup>2</sup> ab initio values from Tables III or VIII of Ref. (33).

<sup>3</sup> from Tables II of Ref. (33).

<sup>4</sup> Calculated value inferred from fit I in Table IV of Ref. (15).

**Table 11**

Comparison of Bandstrengths ( $S_v^\circ$ ) from the present work and from literature  
(in  $\text{cm}^{-2}\text{atm}^{-1}$ ) for the  $2\nu_2^s$ ,  $2\nu_2^a$  and  $\nu_4$  bands of  $^{14}\text{NH}_3$  at 296 K.

		$2\nu_2 (a \leftarrow s)$	$2\nu_2 (s \leftarrow a)$	$\nu_4$
Present work <sup>1</sup>	1203 lines	0.201(5)	6.68(24)	116 (3)
Urban et al (15,16) <sup>2</sup>	40 lines	-	8.24(31)	118 (7)
Aroui et al. (17)	57 lines	-	-	110.3 (8.5)
low resolution studies <sup>3</sup>		-	-	116 (15)
Average				115.1 (3)

<sup>1</sup> Calculated from Eq. (7) of this paper.

<sup>2</sup> Calculated from the transition dipole moments of Table IV of Ref. (15) ; referred as fits I.

<sup>3</sup> Average value of Ref. Kim (19), Koops et al. (20), France and William (21) and Mc Kean and Schatz (22).

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
(R)P (13,A, 9,a)	12 A Azo	2 a10 1 nu4	1333.00637	-4.1	1.18E-04	0.2	-8.3	3
(R)P (14,E, 8,s)	13 E Eo	9 s 9 1 nu4	1335.21296	-0.5	4.54E-05	2.7	-9.2	2
(Q)P (12,E, 10,a)	12 E Eo	4 s10 0 2nu2	1337.27034	-5.9	1.14E-04	1.8	15.5	3
(Q)P (12,E, 10,a)	11 E Eo	2 s10 0 2nu2	1346.65727	-1.4	2.21E-04	3.4	1.5	4
(R)P (13,E, 8,s)	12 E Eo	7 s 9 1 nu4	1348.49562	0.2	1.47E-04	2.3	-2.0	3
(Q)P (13,A, 9,a)	12 A Azo	3 s 9 0 2nu2	1350.30041	5.9	1.21E-04	2.1	-15.2	3
(R)P (12,A, 9,s)	11 A Azo	2 s10 1 nu4	1351.33503	0.7	6.11E-04	2.3	2.3	4
(R)P (13,E, 7,a)	12 E Eo	8 a 8 1 nu4	1352.52761	-3.5	1.08E-04	1.6	4.5	3
(Q)P (11,E, 10,a)	10 E Eo	1 s10 0 2nu2	1353.60322	1.1	2.37E-04	2.0	17.5	4
(S)P (8,E, 5,a)	7 E Eo	2 s 7-1 nu4	1356.30491	3.9	6.36E-05	0.0	-6.9	2
(R)P (13,E, 7,s)	12 E Eo	10 s 8 1 nu4	1357.29514	0.5	1.34E-04	3.1	-1.6	3
(Q)P (12,A, 9,s)	11 A Azo	3 s 9 0 2nu2	1360.46526	-4.5	4.60E-04	2.0	-2.4	4
(R)P (11,A, 9,s)	10 A Azo	1 s10 1 nu4	1364.50681	-3.3	7.95E-04	1.8	8.1	4
(R)P (13,A, 6,s)	12 A Azo	6 s 7 1 nu4	1364.89273	0.1	2.05E-04	2.4	-12.0	2
(R)P (13,E, 5,a)	12 E Eo	13 a 6 1 nu4	1367.89247	4.1	1.08E-04	2.3	5.8	3
(S)P (10,A, 3,a)	9 A Azo	4 s 5-1 nu4	1370.33408	-2.1	4.63E-04	1.7	15.7	4
(Q)P (11,A, 9,a)	10 A Azo	2 s 9 0 2nu2	1370.81226	-0.9	1.00E-03	1.6	3.9	4
(R)P (12,E, 7,s)	11 E Eo	7 s 8 1 nu4	1371.25546	0.6	3.82E-04	2.2	-0.4	4
(P)P (16,E, 16,s)	15 E Eo	1 s15-1 nu4	1371.66895	-4.1	1.31E-03	1.0	-4.3	3
(P)P (16,E, 16,s)	15 E Eo	1 s15-1 nu4	1371.79708	4.3	1.32E-03	1.3	-2.6	3
(P)P (16,A, 15,s)	15 A Azo	1 s14-1 nu4	1374.62869	-0.1	1.52E-03	0.9	-3.7	4
(P)P (16,A, 15,s)	15 A Azo	2 s14-1 nu4	1375.23178	-1.1	1.44E-03	1.9	-11.0	2
(R)P (11,E, 8,s)	10 E Eo	3 s 9 1 nu4	1375.60412	0.6	7.17E-04	3.6	4.0	3
(P)P (16,E, 14,s)	15 E Eo	5 s13-1 nu4	1377.32292	4.0	4.62E-04	2.3	-3.5	4
(Q)P (10,A, 9,a)	9 A Azo	1 s 9 0 2nu2	1378.24035	1.0	8.76E-04	1.7	13.9	4
(P)P (16,E, 14,s)	15 E Eo	5 s13-1 nu4	1378.48328	-3.9	5.67E-04	3.9	13.0	3
(R)P (11,E, 7,a)	10 E Eo	4 a 8 1 nu4	1378.99796	-1.8	3.09E-04	2.1	5.7	4
(R)P (12,A, 6,s)	11 A Azo	5 s 7 1 nu4	1379.36016	0.5	6.48E-04	2.5	-9.9	4
(R)P (12,E, 6,s)	11 E Eo	11 a 6 1 nu4	1381.39772	-1.1	2.64E-04	3.0	-2.4	4
(Q)P (12,E, 7,s)	11 E Eo	7 s 7 0 2nu2	1382.15339	1.8	9.25E-05	4.0	-15.9	3
(S)P (11,E, 2,s)	10 E Eo	12 a 4-1 nu4	1382.83094	-1.4	1.22E-04	2.5	14.7	3
(Q)P (11,E, 8,s)	10 E Eo	5 s 8 0 2nu2	1383.38753	-3.4	5.56E-04	0.2	-0.5	4
(P)P (16,A, 12,s)	15 A Azo	5 s11-1 nu4	1384.60593	-9.5	3.90E-04	1.6	-11.3	4
(S)P (9,A, 3,a)	8 A Azo	3 s 5-1 nu4	1384.67670	-1.7	7.34E-04	1.5	15.4	4
(R)P (11,E, 7,s)	10 E Eo	6 s 8 1 nu4	1385.39980	1.0	8.85E-04	1.9	1.0	4
(R)P (12,E, 5,s)	11 E Eo	11 s 6 1 nu4	1386.30367	1.1	2.83E-04	1.5	-6.1	4
(R)P (11,A, 6,s)	10 A Azo	3 a 7 1 nu4	1387.39271	-2.3	7.59E-04	2.7	-13.2	2
(P)P (15,A, 15,s)	14 A Azo	1 s14-1 nu4	1387.91773	0.5	7.19E-03	0.0	5.4	2
(P)P (15,A, 15,s)	14 A Azo	1 s14-1 nu4	1388.05461	0.0	7.47E-03	4.7	9.5	2
(R)P (10,E, 8,s)	9 E Eo	2 s 9 1 nu4	1389.55690	-2.3	8.49E-04	0.9	8.7	4
(P)P (15,E, 14,s)	14 E Eo	3 s13-1 nu4	1390.43695	-1.1	2.00E-03	1.3	-1.4	4
(R)P (12,E, 4,s)	11 E Eo	13 s 5 1 nu4	1392.10369	2.1	2.04E-04	1.9	-10.8	4
(P)P (15,E, 13,s)	14 E Eo	4 s12-1 nu4	1392.69715	0.0	1.25E-03	1.2	-2.6	3
(Q)P (10,E, 7,a)	9 E Eo	3 s 7 0 2nu2	1393.26236	-0.7	2.24E-04	2.3	4.0	4
(R)P (12,A, 3,a)	11 A Azo	7 a 4 1 nu4	1393.34869	1.2	4.36E-04	2.0	-14.2	4
(P)P (15,E, 13,s)	14 E Eo	4 s12-1 nu4	1393.83423	-1.9	1.25E-03	1.8	-5.0	4
(Q)P (11,A, 7,a)	10 A Azo	5 s 7 0 2nu2	1393.90101	-2.0	4.50E-04	2.8	-5.4	3
(P)P (11,A, 6,s)	10 A Azo	6 a 7 1 nu4	1393.98230	0.8	1.78E-03	2.4	-4.7	5
(P)P (15,E, 12,s)	14 A Azo	3 s11-1 nu4	1394.71980	2.1	1.63E-03	1.1	-3.2	2
(S)P (11,E, 1,s)	10 E Eo	13 s 3-1 nu4	1398.32330	1.4	1.39E-04	1.6	8.1	2
(S)P (8,A, 3,a)	7 A Azo	2 s 5-1 nu4	1399.75307	-1.4	9.03E-04	1.7	12.7	4
(R)P (10,E, 7,s)	9 E Eo	4 a 8 1 nu4	1399.78732	1.0	1.58E-03	1.9	4.2	4
(R)P (12,E, 2,s)	11 E Eo	16 s 3 1 nu4	1400.14568	2.3	5.77E-05	0.0	-4.2	2
(P)P (15,E, 8,s)	14 E Eo	13 s 7-1 nu4	1400.71228	0.6	2.19E-04	3.1	-11.3	4
(Q)P (10,A, 6,a)	9 A Azo	2 s 6 0 2nu2	1401.37752	-1.8	9.70E-04	1.7	-1.5	4
(R)P (11,E, 5,s)	10 E Eo	9 s 6 1 nu4	1401.40754	0.8	8.47E-04	4.0	-7.7	4
(R)P (11,E, 4,s)	10 E Eo	8 a 1 nu4	1401.45160	-1.7	8.83E-04	1.6	-2.7	4
(P)P (15,E, 10,s)	14 E Eo	10 a 9-1 nu4	1401.55515	-2.3	4.06E-04	2.4	-10.7	4
(P)P (15,E, 7,s)	14 E Eo	16 s 6-1 nu4	1401.69611	-5.2	1.70E-04	3.1	-15.2	3
(P)P (14,E, 14,s)	13 E Eo	2 s13-1 nu4	1404.14629	2.4	9.10E-03	0.9	12.5	3
(S)P (11,E, 1,s)	10 E Eo	14 a 3-1 nu4	1404.50112	-3.3	9.97E-05	4.2	-6.8	2
(S)P (9,E, 2,a)	8 E Eo	8 a 4-1 nu4	1405.47071	-1.0	4.98E-04	3.2	14.1	3
(R)P (10,E, 7,a)	9 E Eo	4 a 8 1 nu4	1406.11989	-1.8	1.27E-03	3.2	-1.3	5
(P)P (14,E, 13,s)	13 E Eo	2 s12-1 nu4	1406.22035	-1.1	5.02E-03	3.7	2.0	5
(R)P (11,A, 3,a)	10 A Azo	6 a 4 1 nu4	1406.81404	-1.4	5.21E-03	3.5	-11.0	3
(S)P (12,A, 0,s)	11 A Azo	10 s 2-1 nu4	1407.02227	-3.8	1.33E-03	3.5	-11.0	3
(R)P (11,E, 4,s)	10 E Eo	11 s 5 1 nu4	1407.46115	-4.5	6.34E-04	3.0	-1.2	4
(P)P (14,A, 12,s)	13 A Azo	2 s11-1 nu4	1407.69356	1.5	6.93E-04	1.0	-4.6	3
(R)P (10,A, 6,s)	9 A Azo	3 s 7 1 nu4	1408.03473	-2.2	6.20E-03	3.2	-3.1	4
(R)P (14,E, 11,s)	13 E Eo	6 s10-1 nu4	1408.80464	1.1	3.92E-03	1.9	-0.6	6
(P)P (14,E, 10,s)	13 E Eo	8 s 9-1 nu4	1409.60723	-1.6	2.03E-03	3.9	-7.2	5
(P)P (14,E, 10,s)	13 E Eo	8 s 9-1 nu4	1410.95182	-0.2	1.51E-03	3.1	-2.3	4
(P)P (14,E, 11,s)	13 E Eo	7 a10-1 nu4	1411.34411	-0.1	2.22E-03	3.0	-2.5	4
(S)P (10,E, 1,a)	9 E Eo	11 s 3-1 nu4	1411.65447	0.7	3.25E-04	2.2	13.7	2
(R)P (11,A, 3,s)	10 A Azo	7 s 4 1 nu4	1412.79824	0.5	9.51E-04	1.2	-8.5	3
(P)P (14,E, 8,s)	13 E Eo	11 s 7-1 nu4	1412.99584	1.1	8.15E-04	2.0	-8.7	3
(P)P (14,E, 10,s)	13 E Eo	8 a 9-1 nu4	1413.43148	-0.6	1.94E-03	2.2	-9.9	3
(P)P (14,E, 7,s)	13 E Eo	14 s 6-1 nu4	1413.70529	0.2	6.38E-04	1.5	-11.3	3
(P)P (14,E, 6,s)	13 A Azo	8 s 5-1 nu4	1414.18487	-2.5	1.03E-03	1.9	-13.3	5
(R)P (14,E, 5,s)	13 E Eo	18 s 4-1 nu4	1414.31930	-12.7	4.25E-04	3.3	-14.6	4
(R)P (9,E, 7,s)	8 E Eo	2 s 8 1 nu4	1414.48681	-1.1	1.70E-03	2.1	8.0	5
(R)P (10,A, 6,a)	9 A Azo	3 a 7 1 nu4	1415.47434	-1.4	2.06E-03	2.4	-16.5	3
(S)P (7,A, 3,a)	6 A Azo	1 s 5-1 nu4	1415.55921	-0.1	8.37E-04	3.2	13.3	4
(P)P (14,E, 2,s)	13 E Eo	24 s 1-1 nu4	1416.39877	34.7	3.70E-04	3.4	-14.2	4
(R)P (11,E, 2,s)	10 E Eo	14 s 3 1 nu4	1416.61704	2.4	2.18E-04	1.9	-12.2	2

	(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
	(R)P (10,E, 5,s)	9 E Ee	7 s 6 1	nu4	1416.67691	0.9	2.05E-03	4.1	-4.1
**	(U)P (9,A, 0,s)	8 A+ A2o	5 a 4 1	nu4	1416.94570	1.5	3.67E-04	0.8	-1.9
	(R)P (9,E, 7,a)	8 E Eo	2 a 8 1	nu4	1418.53966	1.4	2.08E-03	2.4	1.6
	(P)P (13,E, 13,s)	12 E Eo	1 s12-1	nu4	1420.34915	3.2	1.79E-02	3.1	2.6
	(Q)P (10,A, 3,a)	9 A- A2o	5 s 3 0	2nu2	1420.45939	0.5	2.47E-03	3.8	5.4
	(P)P (13,E, 13,a)	12 E Eo	1 a12-1	nu4	1420.50949	-2.5	1.76E-02	3.4	1.1
	(P)P (13,A, 12,s)	12 A+ A2o	1 s11-1	nu4	1421.97053	-1.0	2.34E-02	3.8	4.6
	(P)P (13,A, 12,s)	12 A+ A2o	2 a11-1	nu4	1422.56124	-0.7	2.34E-02	3.0	3.2
**	(*)P (10,E, 5,a)	9 E Eo	8 s ** *	**	1423.03959	0.0	7.90E-04	4.0	-15.3
	(P)P (13,E, 11,s)	12 E Ee	5 s10-1	nu4	1423.32803	-2.6	7.95E-03	3.4	5.8
	(R)P (10,E, 4,s)	9 E Eo	9 s 5 1	nu4	1423.43096	0.8	2.15E-03	3.3	7.3
	(R)P (9,A, 6,s)	8 A+ A2o	2 s 7 1	nu4	1423.88726	0.9	6.48E-03	2.0	3.1
	(Q)P (10,E, 2,a)	9 E Ee	11 s 2 0	2nu2	1424.61529	-0.3	1.07E-03	0.7	-5.2
	(P)P (13,A, 9,s)	12 A- A2e	4 s 8-1	nu4	1425.30220	-1.7	7.76E-03	3.4	0.9
	(P)P (13,E, 8,s)	12 E Eo	10 s 7-1	nu4	1425.93935	-1.1	3.00E-03	3.7	2.0
	(Q)P (8,E, 7,s)	7 E Ee	1 s 7 0	2nu2	1426.06499	0.1	1.36E-03	2.2	10.1
	(P)P (13,E, 10,s)	12 E Ee	6 a 9-1	nu4	1426.13821	1.3	5.27E-03	3.8	-4.3
	(P)P (13,E, 7,s)	12 E Ee	12 s 6-1	nu4	1426.35586	0.2	2.20E-03	3.2	-6.3
	(P)P (13,E, 5,s)	12 E Ee	16 s 4-1	nu4	1426.49518	-1.4	1.43E-03	1.5	-14.2
	(P)P (13,A, 6,s)	12 A+ A2o	7 s 5-1	nu4	1426.55231	0.2	3.43E-03	1.8	-12.4
	(P)P (13,E, 2,s)	12 E Eo	22 s 1-1	nu4	1427.12621	17.0	1.16E-03	0.7	-17.6
	(Q)P (10,E, 1,a)	9 E Eo	13 s 1 0	2nu2	1427.41814	0.6	1.17E-03	3.7	-2.4
	(P)P (13,A, 9,a)	12 A+ A2o	5 a 8-1	nu4	1427.73729	1.3	8.25E-03	3.0	0.9
	(Q)P (10,A, 0,a)	9 A+ A2o	7 s 0 0	2nu2	1428.27832	0.6	1.94E-03	1.2	2.7
	(R)P (9,A, 6,a)	8 A+ A2o	3 a 7 1	nu4	1428.78458	-0.3	5.55E-03	3.9	-2.2
	(P)P (13,A, 3,s)	12 A- A2e	11 s 2-1	nu4	1428.85088	2.4	2.47E-03	2.0	-14.4
	(R)P (10,A, 3,s)	9 A+ A2e	6 s 4 1	nu4	1429.03841	1.1	2.94E-03	2.3	-6.2
	(R)P (10,E, 2,s)	9 E Eo	12 s 3 1	nu4	1433.31677	-0.4	7.86E-04	1.2	-10.0
	(P)P (13,E, 5,a)	12 E Eo	16 a 4-1	nu4	1433.55328	1.8	1.53E-03	2.7	-11.7
**	(S)P (6,A, 3,s)	5 A+ A2e	1 a 5-1	nu4	1433.77473	-4.2	4.33E-04	3.7	8.1
	(Q)P (9,A, 3,s)	8 A+ A2o	4 s 3 0	2nu2	1434.33212	1.8	2.67E-03	3.9	0.1
	(P)P (12,A, 12,s)	11 A- A2o	1 s11-1	nu4	1436.52041	4.2	7.38E-02	1.2	2.7
	(P)P (12,A, 12,s)	11 A- A2o	1 a11-1	nu4	1436.69081	-3.4	7.00E-02	1.1	-2.0
	(P)P (12,E, 11,s)	11 E Ee	3 s10-1	nu4	1437.67996	-0.5	2.41E-02	3.9	1.7
	(Q)P (9,E, 2,a)	8 E Ee	9 s 2 0	2nu2	1438.15472	2.9	1.48E-03	1.8	0.1
	(P)P (12,E, 11,a)	11 E Eo	3 a10-1	nu4	1438.26655	-1.1	2.43E-02	3.6	1.2
	(P)P (12,E, 2,s)	11 E Eo	20 s 1-1	nu4	1438.47729	4.9	3.83E-03	3.4	-4.3
	(P)P (12,A, 9,s)	11 A+ A2e	3 s 8-1	nu4	1439.19211	-2.9	2.49E-02	2.7	4.8
	(P)P (12,E, 5,s)	11 E Ee	14 s 4-1	nu4	1439.24392	0.8	4.72E-03	3.7	-3.4
	(P)P (12,A, 3,s)	11 A+ A2e	10 s 2-1	nu4	1439.28398	-4.1	6.06E-03	3.5	10.3
	(R)P (8,A, 6,s)	7 A- A2o	7 s 7 0	nu4	1439.49972	1.1	6.73E-03	3.5	-10.4
	(R)P (9,E, 4,s)	8 E Ee	7 s 5 1	nu4	1439.53696	0.2	4.46E-03	1.8	-2.9
	(P)P (12,E, 11,s)	11 A- A2o	6 s 5-1	nu4	1439.58253	0.1	1.17E-02	3.5	1.4
	(P)P (12,E, 10,a)	11 E Ee	4 a 9-1	nu4	1439.64711	1.1	1.69E-02	3.7	-0.1
	(P)P (12,E, 7,s)	11 E Ee	10 s 6-1	nu4	1439.68987	-1.0	7.10E-03	3.3	1.1
**	(S)Q (11,A, 9,s)	11 A- A2o	1 s11-1	nu4	1440.01494	3.6	3.96E-04	3.3	3.5
**	(S)P (8,E, 1,a)	7 E Eo	8 s 3-1	nu4	1440.64407	0.2	9.59E-04	1.3	11.5
	(Q)P (9,E, 1,a)	8 E Eo	11 s 1 0	2nu2	1440.66291	6.7	1.54E-03	1.4	-5.8
	(P)P (12,A, 9,a)	11 A- A2o	4 a 8-1	nu4	1440.86381	2.0	2.57E-02	2.8	3.6
	(P)P (12,E, 8,s)	11 E Ee	9 a 7-1	nu4	1441.95554	2.3	7.41E-03	3.6	1.7
	(R)P (8,A, 6,a)	7 A- A2o	2 a 7 1	nu4	1442.33238	2.4	7.87E-03	2.4	1.9
	(P)P (12,E, 7,s)	11 E Eo	9 s 6-1	nu4	1442.93647	-3.8	7.62E-03	3.8	1.1
	(R)P (9,E, 4,a)	8 E Ee	7 a 5 1	nu4	1443.73617	-0.3	2.23E-03	1.0	-9.0
	(P)P (12,A, 6,s)	11 A+ A2e	6 a 5-1	nu4	1443.90681	-1.4	1.17E-02	3.9	-6.4
	(Q)P (8,E, 4,a)	7 E Ee	4 s 4 0	2nu2	1444.13770	-2.2	6.57E-04	0.4	7.9
	(P)P (12,E, 5,a)	11 E Eo	14 a 4-1	nu4	1444.81296	-1.6	4.85E-03	6.8	-8.1
	(R)P (9,A, 3,s)	8 A- A2e	5 s 4 1	nu4	1445.40907	-0.8	8.84E-03	3.6	0.3
	(P)P (12,A, 3,s)	11 A- A2o	10 a 2-1	nu4	1447.85790	15.6	8.79E-02	4.5	4.6
	(Q)P (9,A, 3,s)	8 A+ A2o	5 a 1 0	2nu2	1448.19874	6.6	2.87E-03	2.5	-14.4
	(Q)P (7,A, 6,a)	6 A+ A2o	5 s 6 0	2nu2	1449.21619	0.0	4.62E-03	2.3	9.8
	(R)P (11,A, 9,s)	10 A+ A2o	9 s 1 1	nu4	1449.49442	-1.1	2.00E-02	3.6	-2.6
	(P)P (11,E, 1,s)	10 E Ee	18 s 0 1	nu4	1449.79242	-8.1	1.04E-02	3.5	-0.1
	(R)P (9,E, 2,s)	8 E Eo	10 s 3 1	nu4	1450.17683	-3.5	2.27E-03	3.2	-9.5
	(P)P (11,E, 2,s)	10 E Eo	18 s 1-1	nu4	1450.51249	-0.7	1.06E-02	2.7	0.3
**	(S)P (9,A, 0,s)	8 A+ A2o	6 a 2-1	nu4	1450.84597	-1.8	2.20E-03	2.6	10.7
	(R)P (8,E, 5,a)	7 E Eo	5 a 6 1	nu4	1451.52067	0.8	5.76E-03	3.5	-1.3
	(P)P (11,E, 4,s)	10 E Eo	13 s 3-1	nu4	1451.76261	1.9	1.12E-02	2.6	11.9
**	(P)P (9,E, 2,s)	8 E Eo	11 s 1 0	2nu2	1451.88211	6.6	5.62E-03	1.6	-2.7
	(P)P (11,E, 11,s)	10 E Ee	1 a10-1	nu4	1452.85544	6.2	6.98E-02	3.3	1.7
	(P)P (11,A, 6,s)	10 A+ A2o	5 s 5-1	nu4	1452.83213	-4.0	7.04E-02	3.8	2.6
	(P)P (11,E, 10,s)	10 E Eo	2 s 9-1	nu4	1453.31967	-0.9	3.03E-02	3.5	-2.9
	(R)P (9,E, 1,s)	8 E Ee	12 s 2 1	nu4	1453.34052	0.3	4.95E-02	3.8	5.3
	(P)P (11,E, 7,s)	10 E Ee	8 s 6-1	nu4	1453.72514	-1.8	1.88E-02	3.1	-2.6
	(P)P (11,A, 9,s)	10 A- A2e	2 s 8-1	nu4	1453.74421	-2.2	6.93E-02	3.9	3.7
	(P)P (11,E, 8,s)	10 E Eo	6 s 7-1	nu4	1453.87029	-2.4	2.58E-02	3.3	3.8
	(P)P (11,E, 10,a)	10 E Ee	3 a 9-1	nu4	1453.92316	-1.0	4.83E-02	3.0	1.7
**	(O)P (12,E, 4,s)	11 E Eo	17 a 2 1	nu4	1454.24818	-12.0	4.13E-02	3.8	-2.7
**	(P)P (11,A, 3,s)	10 A- A2e	3 a 8-1	nu4	1454.76276	-0.9	1.33E-02	3.2	-2.2
	(P)P (11,A, 8,s)	10 A+ A2o	9 s 1 0	2nu2	1454.80579	1.3	6.97E-02	3.6	1.2
	(Q)P (8,A, 0,a)	7 A+ A2e	5 s 0 0	2nu2	1454.83069	3.8	3.03E-03	2.5	3.0
	(R)P (8,E, 4,s)	7 E Eo	6 s 5 1	nu4	1455.45636	0.2	8.78E-03	3.6	3.0
	(P)P (11,E, 8,s)	10 E Ee	7 a 7-1	nu4	1455.50925	2.0	2.51E-02	3.9	-3.8
	(P)P (11,E, 7,a)	10 E Eo	7 a 6-1	nu4	1456.06933	1.3	2.04E-02	3.3	-0.6
	(P)P (11,A, 6,s)	10 A- A2e	5 a 5-1	nu4	1456.52962	-0.1	3.24E-02	2.2	-4.1

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
(P)P (11,E, 5,a)	10 E Eo 12 a 4-1	nu4	1456.92485	-1.7	1.44E-02	3.0	0.9	2
(P)P (11,E, 4,a)	10 E Eo 14 a 3-1	nu4	1457.19181	-3.4	1.13E-02	3.0	-6.6	3
(P)P (11,A, 3,a)	10 A+ A2o 8 a 2-1	nu4	1458.10290	0.6	2.26E-02	3.2	-4.7	4
(P)P (11,E, 2,a)	10 E Eo 17 a 1-1	nu4	1458.49186	4.8	1.06E-02	0.6	-5.1	4
** (P)P (11,E, 1,a)	10 E Eo 19 * * *	**	1458.77786	-3.7	9.66E-03	3.3	-7.7	5
(R)P (8,E, 4,a)	7 E Ee 5 a 5-1	nu4	1458.94526	-0.2	6.12E-03	3.0	-5.4	4
** (S)P (8,A, 0,a)	7 A+ A2e 6 s 2-1	nu4	1460.46135	3.6	4.78E-03	3.7	3.8	6
(S)Q (10,E, 8,s)	10 E Eo 1 a10-1	nu4	1460.62026	-3.3	4.13E-04	3.0	13.3	3
** (N)P (10,A, 3,s)	9 A+ A2e 7 s 0 0	2nu2	1460.75397	1.5	2.61E-03	4.0	-0.9	5
(R)P (8,A, 3,s)	7 A+ A2e 4 a 4-1	nu4	1461.95688	-0.8	1.86E-02	2.2	1.2	7
(P)P (10,E, 1,s)	9 E Ee 16 s 0 1	nu4	1462.19014	-2.2	2.46E-02	3.5	-0.7	8
(P)P (10,E, 2,s)	9 E Ee 16 s 1-1	nu4	1463.29136	-2.6	2.47E-02	3.3	-1.0	8
(R)P (7,E, 5,s)	6 E Ee 2 s 6-1	nu4	1464.00063	-0.5	5.76E-03	3.8	3.9	8
(P)P (10,A, 3,s)	9 A+ A2e 8 s 2-1	nu4	1464.63156	7.7	4.97E-02	3.6	-0.1	9
(R)P (8,A, 3,a)	7 A- A2o 4 a 4-1	nu4	1464.81289	-1.2	1.06E-02	2.3	-6.4	4
(P)P (10,E, 4,s)	9 E Ee 11 s 3-1	nu4	1465.60441	1.4	2.74E-02	3.0	-1.0	8
** (Q)P (9,E, 1,a)	8 E Eo 13 s 1-1	nu4	1465.65246	-2.7	1.01E-03	2.7	14.8	3
(R)P (7,E, 5,a)	6 E Eo 3 a 6-1	nu4	1466.20783	3.1	7.11E-03	2.9	4.0	8
(P)P (10,E, 5,s)	9 E Ee 10 s 4-1	nu4	1466.82025	-0.2	3.36E-02	3.7	4.7	8
** (O)P (10,A, 3,a)	9 A- A2o 7 s 1 1	nu4	1466.89776	3.9	1.38E-02	3.3	-1.3	6
(R)P (8,E, 2,s)	7 E Ee 4 s 3-1	nu4	1467.34505	-0.1	7.54E-03	3.6	-2.1	6
(P)P (10,A, 6,s)	9 A- A2o 4 a 5-1	nu4	1467.77835	-1.2	7.83E-02	2.8	1.5	9
(R)P (10,E, 7,s)	9 E Ee 4 s 6-1	nu4	1468.45943	-1.9	4.95E-02	2.8	2.3	9
(P)P (10,E, 10,s)	9 E Ee 1 s 9-1	nu4	1468.73700	5.3	1.26E-01	3.2	1.9	9
(P)P (10,E, 8,s)	9 E Ee 5 s 7-1	nu4	1468.84993	-1.6	6.69E-02	3.9	5.3	9
(P)P (10,A, 9,s)	9 A+ A2e 1 s 8-1	nu4	1468.94324	0.4	1.75E-01	3.1	1.1	7
(R)P (8,E, 2,a)	7 E Ee 9 a 3-1	nu4	1469.17632	-1.3	3.32E-03	4.0	-7.2	5
(P)P (10,A, 9,a)	9 A- A2o 2 a 8-1	nu4	1469.52175	-1.2	1.79E-01	3.3	1.7	8
(P)P (10,E, 8,a)	9 E Ee 2 a 5-1	nu4	1469.89154	1.0	6.54E-02	2.9	0.1	9
(P)P (10,E, 5,a)	9 E Ee 10 a 4-1	nu4	1469.96398	0.6	3.41E-02	3.4	-2.0	8
(P)P (10,E, 7,a)	9 E Ee 6 a 6-1	nu4	1470.06265	1.6	4.76E-02	2.6	-6.9	7
(P)P (10,A, 6,a)	9 A+ A2e 4 a 5-1	nu4	1470.07208	1.3	8.62E-02	3.2	4.3	5
** (S)Q (12,E, 8,s)	12 E Ee 5 s10-1	nu4	1471.24527	-2.8	2.33E-04	4.1	-3.6	2
(P)P (10,A, 3,a)	9 A- A2o 8 a 2-1	nu4	1471.62126	-5.8	4.20E-02	3.8	-4.9	7
(R)P (7,E, 4,s)	6 E Ee 4 a 5-1	nu4	1471.85135	0.5	1.21E-02	3.5	2.3	3
** (S)P (6,E, 1,a)	5 E Ee 4 s 3-1	nu4	1472.72323	-0.9	1.22E-03	3.5	4.6	3
(R)P (7,E, 4,a)	6 E Ee 4 a 5-1	nu4	1474.42585	1.2	1.12E-02	1.8	-2.2	6
(R)P (9,A, 0,s)	8 A+ A2o 7 s 1 1	nu4	1474.72552	1.2	1.07E-01	3.0	1.8	8
** (O)P (13,A, 6,a)	12 A- A2e 9 s 4 1	nu4	1474.85020	-6.8	3.07E-04	0.0	-9.2	2
(P)P (6,E, 1,s)	5 E Ee 5 a 3-1	nu4	1474.95003	0.2	1.33E-03	2.7	9.3	3
(P)P (9,E, 1,s)	8 E Ee 14 s 0 1	nu4	1475.33550	0.5	5.21E-02	2.9	-0.6	9
(P)P (9,E, 2,s)	8 E Ee 13 s 1-1	nu4	1476.87232	-2.2	2.25E-02	2.5	-0.7	9
(R)P (7,A, 3,s)	6 A- A2e 3 s 4-1	nu4	1478.70317	-0.5	3.37E-02	1.5	3.7	8
** (S)P (7,A, 0,s)	6 A+ A2o 4 a 2-1	nu4	1479.14254	2.0	6.13E-03	3.8	5.6	7
(P)P (8,E, 1,a)	7 E Ee 12 s 1-1	nu4	1479.95208	-0.8	1.77E-03	3.9	11.9	4
(P)P (9,E, 4,a)	8 E Ee 9 s 3-1	nu4	1480.18304	0.9	6.21E-02	3.3	2.5	9
** (O)P (10,E, 2,s)	9 E Ee 17 a 0 1	nu4	1480.85039	-7.8	3.13E-04	3.2	-4.2	2
** (O)P (11,A, 3,a)	10 A+ A2o 9 s 1 1	nu4	1480.92777	-1.2	4.89E-04	2.5	13.4	2
(P)P (9,E, 1,a)	8 E Ee 15 a 0 1	nu4	1481.57667	-5.1	5.39E-02	2.8	-3.5	9
(P)P (9,E, 2,a)	8 E Ee 13 a 1-1	nu4	1482.05882	-3.8	5.64E-02	3.2	-2.9	9
(P)P (9,A, 3,a)	8 A+ A2o 6 a 2-1	nu4	1482.68791	-2.1	1.20E-01	3.6	-2.1	9
(P)P (9,A, 6,s)	8 A+ A2o 3 s 5-1	nu4	1482.95031	-1.3	1.78E-01	3.8	1.9	8
(P)P (9,E, 4,a)	8 E Ee 10 a 3-1	nu4	1483.24333	0.6	6.55E-02	2.9	-1.0	9
(P)P (9,E, 7,s)	8 E Ee 4 s 6-1	nu4	1483.87513	-1.1	1.13E-01	2.7	1.7	9
(P)P (9,E, 5,a)	8 E Ee 8 a 4-1	nu4	1483.94545	1.4	7.65E-02	3.7	0.1	9
(P)P (9,E, 8,s)	8 E Ee 3 s 7-1	nu4	1484.48053	0.6	1.50E-01	3.9	1.2	8
(P)P (9,A, 9,s)	8 A- A2e 1 s 8-1	nu4	1484.76631	4.5	4.29E-01	1.1	3.6	5
(P)P (9,E, 7,a)	8 E Ee 4 a 6-1	nu4	1484.89417	0.7	1.20E-01	1.0	3.9	7
(P)P (9,A, 9,a)	8 A+ A2o 1 a 8-1	nu4	1484.96601	-4.6	4.36E-01	2.2	5.7	4
(P)P (9,E, 8,a)	8 E Ee 3 a 7-1	nu4	1485.05372	-1.4	1.50E-01	3.8	-0.3	8
** (O)P (9,E, 2,a)	8 E Ee 14 s 0 1	nu4	1485.63436	0.2	6.85E-04	2.2	12.4	3
(P)P (7,E, 2,a)	6 E Ee 8 a 3 1	nu4	1486.24635	-2.0	9.90E-03	3.2	-6.7	7
** (S)P (8,A, 3,s)	7 A- A2e 6 s 2-1	nu4	1488.05868	-0.6	1.29E-02	3.7	-5.7	7
** (N)P (8,A, 3,s)	7 A+ A2e 5 s 0 0	2nu2	1488.49644	4.2	2.72E-03	3.4	9.9	5
(P)P (6,E, 5,s)	5 E Ee 2 s 5-1	nu4	1488.59321	-0.6	9.91E-03	2.9	1.4	7
(R)P (7,E, 1,s)	6 E Ee 9 s 2-1	nu4	1488.91352	-4.2	8.74E-03	2.2	-0.2	6
(P)P (8,E, 1,s)	7 E Ee 12 s 0 1	nu4	1489.26230	2.9	1.00E-01	3.8	1.0	7
(R)P (7,E, 1,a)	6 E Ee 9 a 2-1	nu4	1489.73795	2.0	3.80E-03	2.2	-0.7	4
(P)P (6,E, 4,a)	5 E Ee 2 a 5-1	nu4	1490.18498	-1.5	1.13E-02	1.5	-1.4	5
(P)P (8,E, 2,s)	7 E Ee 12 s 1-1	nu4	1491.30288	-1.2	1.01E-01	2.6	0.5	9
** (O)P (12,A, 6,a)	11 A+ A2e 8 a 4-1	nu4	1491.59640	5.9	6.95E-04	2.8	-16.6	3
(S)P (5,E, 1,s)	4 E Ee 4 a 3-1	nu4	1491.77148	-1.7	1.02E-03	3.3	7.3	4
** (S)P (6,A, 0,a)	5 A+ A2e 3 s 5-1	nu4	1492.19289	0.7	2.75E-03	3.4	1.6	7
** (O)P (9,E, 0,s)	8 E Ee 15 s 0 1	nu4	1492.79599	-5.1	7.57E-04	2.8	11.7	2
(P)P (8,A, 3,s)	7 A+ A2e 6 s 2-1	nu4	1493.52697	3.9	2.16E-01	3.1	1.8	6
(R)P (8,A, 0,a)	7 A+ A2e 7 a 1 1	nu4	1493.86318	-0.6	2.17E-01	2.5	0.5	6
(Q)P (5,E, 4,a)	4 E Ee 1 s 4 0	2nu2	1493.92737	1.0	6.09E-03	3.6	8.5	5
(P)P (8,E, 1,a)	7 E Ee 13 a 0 1	nu4	1494.24211	-0.3	1.06E-01	3.6	-2.2	9
** (Q)P (7,E, 1,a)	6 E Ee 10 s 1-1	nu4	1495.13209	-1.0	2.40E-03	3.7	-4.9	4
(P)P (8,E, 2,a)	7 E Ee 11 a 1-1	nu4	1495.24254	0.1	1.09E-01	3.6	-1.7	9
(P)P (8,E, 4,s)	7 E Ee 8 s 3-1	nu4	1495.52017	0.3	1.22E-01	3.7	1.7	9
(P)P (6,A, 3,s)	5 A+ A2e 2 s 4-1	nu4	1495.72115	-0.2	4.41E-02	3.7	3.6	8
(P)P (8,A, 3,a)	7 A- A2o 5 a 2-1	nu4	1496.17363	2.8	2.02E-01	3.2	-8.6	3
(P)P (8,E, 5,s)	7 E Ee 5 s 1-1	nu4	1497.33323	-0.6	1.45E-01	2.5	0.8	8
(R)P (6,A, 3,a)	5 A- A2o 3 a 4-1	nu4	1497.51536	1.0	4.05E-02	1.5	-1.1	8

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
(Q)P (5,A, 3,a)	4 A+ A2o 1 s 3 0	2nu2	1497.63262	-2.7	6.71E-03	3.0	6.3	3
(P)P (8,E, 4,a)	7 E Ee 8 a 3-1	nu4	1497.67493	1.7	1.31E-01	2.6	0.4	7
** (Q)P (7,E, 1,s)	6 E Ee 10 a 1-1	nu4	1499.11129	3.1	2.74E-03	3.9	-1.6	4
** (O)P (8,E, 2,a)	7 E Ee 12 s 0 1	nu4	1499.58364	2.8	1.46E-03	6.5	-6.7	2
(P)P (8,A, 6,a)	7 A+ A2e 3 a 5-1	nu4	1499.80268	0.4	3.87E-01	1.2	3.4	5
(P)P (8,E, 7,s)	7 E Ee 2 s 6-1	nu4	1499.94384	0.6	2.38E-01	3.4	1.0	8
(P)P (8,E, 8,s)	7 E Ee 2 s 7-1	nu4	1500.73347	3.6	3.31E-01	0.9	3.2	3
(R)P (6,E, 2,s)	5 E Ee 6 s 3 1	nu4	1501.89046	-1.4	2.98E-02	0.5	3.9	2
** (Q)P (10,A, 3,s)	9 A+ A2e 9 a 1 1	nu4	1502.23170	-8.1	1.12E-03	2.8	2.8	3
(S)Q (5,E, 1,a)	4 E Ee 3 s 1 0	2nu2	1502.35072	-3.3	7.99E-04	0.7	-4.7	2
** (S)P (9,A, 6,s)	9 A- A2o 2 a 8-1	nu4	1502.62492	-0.7	2.70E-03	2.1	8.7	4
(R)P (7,A, 0,s)	6 A+ A2o 5 s 1 1	nu4	1502.75536	6.1	3.62E-01	1.7	4.7	4
(R)P (6,E, 2,a)	5 E Ee 6 a 3 1	nu4	1503.42603	-1.1	2.23E-02	2.5	-2.2	7
** (O)P (11,A, 6,s)	10 A+ A2o 6 a 4 1	nu4	1503.55038	-3.9	8.78E-04	1.5	-8.5	3
(P)P (7,E, 1,s)	6 E Ee 11 s 0 1	nu4	1504.02175	4.2	1.72E-01	0.8	3.4	6
** (O)P (8,A, 3,a)	7 E- A2o 6 s 1 1	nu4	1504.86526	-5.3	2.06E-02	2.8	-7.8	6
(P)P (7,A, 3,s)	6 A- A2e 4 s 2-1	nu4	1509.13789	1.3	3.84E-01	1.9	5.3	4
** (Q)P (6,E, 1,a)	5 E Ee 8 s 1-1	nu4	1511.18649	-0.9	3.26E-03	2.8	-9.6	4
(P)P (7,A, 3,a)	6 A+ A2o 4 a 2-1	nu4	1511.31249	1.9	4.18E-01	1.6	2.4	4
** (S)P (5,A, 0,s)	4 A+ A2o 3 s 2-1	nu4	1511.44007	0.2	7.42E-03	2.9	2.6	3
** (S)Q (11,A, 6,a)	11 A+ A2e 3 s 8-1	nu4	1511.72277	-4.0	1.20E-03	6.2	3.9	2
(P)P (7,E, 4,a)	6 E Ee 7 a 3-1	nu4	1513.04362	1.5	2.34E-01	1.2	1.3	6
(R)P (5,A, 3,s)	4 A- A2e 1 s 4 1	nu4	1513.08180	-0.7	3.52E-02	2.5	5.4	7
(P)P (7,E, 5,s)	6 E Ee 5 s 4-1	nu4	1513.64802	-0.5	2.77E-01	0.8	3.5	4
(R)P (5,A, 3,a)	4 A+ A2o 2 a 4 1	nu4	1514.23228	1.7	3.65E-02	3.5	-0.9	7
** (S)Q (7,E, 5,a)	7 E Ee 2 s 7-1	nu4	1514.29061	3.7	1.38E-03	0.1	2.5	2
(P)P (7,E, 5,a)	6 E Ee 5 a 4-1	nu4	1514.60537	0.1	2.85E-01	0.8	2.3	4
(P)P (7,A, 6,s)	6 A+ A2o 1 s 5-1	nu4	1515.32445	0.4	7.12E-01	0.6	3.3	3
(P)P (7,A, 6,a)	6 A+ A2e 1 s 6-1	nu4	1515.88172	-1.9	7.13E-01	0.8	1.9	3
(P)P (7,E, 7,s)	6 E Ee 1 s 6-1	nu4	1516.63097	2.9	4.67E-01	1.7	1.7	3
(P)P (7,E, 7,a)	6 E Ee 1 a 6-1	nu4	1516.85172	-4.7	4.64E-01	2.7	1.3	3
** (S)Q (12,A, 6,a)	12 A- A2e 4 s 8-1	nu4	1518.08183	-2.1	5.30E-04	8.4	-8.3	2
(Q)P (4,E, 2,a)	3 E Ee 1 s 2 0	2nu2	1518.15497	-1.4	7.56E-03	2.3	3.0	4
** (S)Q (8,E, 5,a)	8 E Ee 3 s 7-1	nu4	1518.43361	0.2	2.03E-03	1.6	4.5	3
** (O)P (7,E, 2,s)	6 E Ee 11 a 0 1	nu4	1519.29626	3.8	1.94E-03	2.2	-2.2	3
(R)P (5,E, 2,s)	4 E Ee 4 s 3 1	nu4	1519.51659	-1.0	3.68E-02	2.9	0.9	5
(Q)P (6,E, 1,s)	3 E Ee 9 s 0 1	nu4	1519.66272	4.1	2.52E-01	0.8	3.7	5
(Q)P (4,E, 1,a)	3 E Ee 2 s 1 0	2nu2	1519.86495	-2.2	5.84E-03	3.8	1.7	2
(Q)P (4,A, 0,a)	3 A+ A2e 1 s 0 0	2nu2	1520.44895	-2.4	1.07E-02	2.8	3.6	3
(P)P (6,E, 2,s)	5 E Ee 8 s 1-1	nu4	1522.77640	-0.8	2.65E-01	1.1	-0.3	3
** (S)Q (9,E, 5,a)	9 E Ee 5 a 1 1	nu4	1523.12597	-1.9	1.66E-03	1.5	-2.5	2
** (O)P (7,A, 3,s)	6 A- A2e 5 a 1 1	nu4	1524.45697	-6.4	1.46E-02	1.9	-3.4	3
(P)P (6,E, 2,a)	5 E Ee 8 a 1-1	nu4	1524.70875	3.4	2.89E-01	1.5	2.0	4
(R)P (5,E, 1,s)	4 E Ee 6 s 2 1	nu4	1524.95389	-2.8	4.11E-02	3.2	0.5	5
(P)P (6,A, 3,s)	5 A+ A2e 4 s 2-1	nu4	1525.76253	0.6	6.10E-01	0.7	3.6	3
(R)P (5,E, 1,a)	4 E Ee 5 a 2 1	nu4	1525.84403	-1.4	2.90E-02	0.3	-0.1	2
** (O)P (8,E, 4,s)	7 E Ee 11 a 2 1	nu4	1526.76340	1.4	3.26E-03	3.7	2.9	2
(P)P (6,A, 3,a)	5 A- A2o 4 a 2-1	nu4	1527.06141	1.7	6.38E-01	0.8	2.1	3
(P)P (6,E, 4,a)	5 E Ee 5 a 3-1	nu4	1528.28962	0.0	3.85E-01	1.6	2.8	4
** (S)P (6,E, 2,a)	5 E Ee 9 s 0 1	nu4	1530.00918	4.0	4.31E-03	2.9	-2.7	5
(P)P (6,E, 5,s)	5 E Ee 3 s 4-1	nu4	1530.61417	0.1	4.78E-01	1.4	4.1	4
(P)P (6,E, 5,a)	5 E Ee 3 a 4-1	nu4	1531.15892	-1.9	4.80E-01	1.4	2.9	4
(P)P (6,A, 6,s)	5 A- A2o 1 s 5-1	nu4	1532.45054	2.2	1.25E+00	1.0	3.0	3
(P)P (6,A, 6,a)	5 A+ A2e 1 a 5-1	nu4	1532.68249	-4.7	1.24E+00	1.1	2.8	3
(R)P (5,A, 0,s)	4 E A2e 4 s 1 1	nu4	1533.79674	6.3	7.10E-01	1.2	4.0	3
** (N)P (10,E, 7,s)	9 E Ee 8 s 4 0	2nu2	1534.68683	0.1	7.91E-04	1.6	-9.4	2
** (O)P (7,A, 3,a)	6 A+ A2o 5 s 1 1	nu4	1534.92514	5.7	6.80E-03	3.7	-2.8	2
** (Q)P (11,E, 8,s)	10 E Ee 9 a 6 1	nu4	1535.63780	-1.8	6.29E-04	0.7	-3.2	2
(P)P (5,E, 1,s)	4 E Ee 8 s 0 1	nu4	1535.20871	1.7	3.21E-04	4.1	1.8	5
(Q)P (3,E, 2,a)	2 E Ee 6 s 1 0	2nu2	1536.46095	2.8	1.46E-02	2.5	5.4	4
(R)P (4,E, 2,s)	3 E Ee 3 s 3 1	nu4	1537.47055	-0.8	2.73E-02	9.2	-1.0	2
(Q)P (5,E, 1,a)	4 E Ee 7 a 0 1	nu4	1538.01023	5.0	3.62E-01	1.1	2.2	5
(Q)P (3,E, 1,a)	2 E Ee 1 s 1 0	2nu2	1538.07471	0.5	1.56E-02	3.4	5.4	4
(P)P (5,E, 2,s)	4 E Ee 6 s 1-1	nu4	1539.75957	-0.9	3.60E-01	2.1	3.7	4
(P)P (5,E, 2,a)	4 E Ee 7 a 1-1	nu4	1541.00408	2.0	3.88E-01	1.5	2.6	4
** (P)P (6,A, 3,a)	5 A- A2o 5 s 1 1	nu4	1541.60319	-6.6	1.74E-02	2.7	-5.0	3
(P)P (5,A, 3,s)	4 A- A2e 2 s 2-1	nu4	1542.97972	-0.2	8.77E-01	1.0	3.3	3
(R)P (4,E, 1,s)	3 E Ee 4 s 2 1	nu4	1543.22366	-1.6	5.58E-01	3.2	-0.9	6
(P)P (5,A, 3,a)	4 A+ A2o 4 a 2-1	nu4	1543.85493	0.0	9.24E-01	0.8	3.0	3
(R)P (4,E, 1,a)	3 E A2o 4 a 2 1	nu4	1544.01905	-0.4	4.79E-02	3.1	-1.9	5
(P)P (5,E, 4,s)	4 E Ee 2 s 3-1	nu4	1545.80435	-0.1	5.79E-01	3.5	5.3	4
** (O)P (8,E, 5,s)	7 E Ee 9 a 3 1	nu4	1546.02779	-1.3	3.19E-03	2.1	-11.7	2
(P)P (5,E, 4,a)	4 E Ee 4 a 3-1	nu4	1546.33131	-1.9	5.79E-01	2.5	3.6	4
** (O)P (5,E, 2,a)	4 E Ee 8 s 0 1	nu4	1546.56032	2.8	5.81E-03	3.1	10.6	3
** (S)Q (9,E, 4,s)	9 E Ee 6 a 6-1	nu4	1547.69840	2.5	2.05E-03	1.0	-1.4	3
** (Q)P (4,E, 1,s)	3 E Ee 5 s 1-1	nu4	1547.89621	0.2	3.72E-03	0.1	0.6	3
** (N)P (8,A, 6,s)	7 A- A2o 3 s 3 0	2nu2	1547.95041	0.2	1.72E-03	6.2	-9.1	2
(P)P (5,E, 5,s)	4 E Ee 2 s 4-1	nu4	1548.18411	1.2	7.47E-01	0.8	2.8	3
(P)P (5,E, 5,a)	4 E Ee 2 a 4 1	nu4	1548.42866	0.1	7.39E-01	0.8	2.1	3
** (M)P (4,E, 4,s)	7 E Ee 13 a 0 1	nu4	1549.11809	-0.3	6.60E-04	4.2	1.3	2
** (S)Q (5,A, 3,a)	5 A- A2o 1 s 5-1	nu4	1550.79788	1.8	4.64E-03	2.3	7.5	3
(R)P (4,A, 0,a)	3 A+ A2e 3 a 1 1	nu4	1552.15738	6.7	8.66E-01	1.2	3.5	3
** (S)Q (5,A, 3,s)	5 A+ A2e 1 a 5-1	nu4	1552.57680	-3.9	4.73E-03	2.0	4.8	3
(P)P (4,E, 1,s)	3 E Ee 6 s 0 1	nu4	1553.62943	1.1	3.55E-01	1.4	4.2	5
** (S)Q (6,A, 3,a)	6 A+ A2o 1 s 5-1	nu4	1553.80429	-0.5	8.29E-03	2.6	8.0	3

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
(P)P (4,E,1,a)	3 E Eo	6 a 0 1	nu4 1554.73399	2.6	3.91E-01	1.2	2.0	4
** (S)Q (6,A+,3,s)	6 A- A2e	2 a 5-1	nu4 1555.78658	-1.5	7.94E-03	3.7	0.1	5
(Q)P (2,E,1,a)	1 E Eo	1 s 1 0	2nu2 1556.90323	3.6	2.11E-02	1.8	3.6	6
(P)P (4,A+,3,s)	3 A+ A2e	2 s 2-1	nu4 1560.88956	-0.4	1.19E+00	1.1	3.5	3
** (O)P (6,E,4,a)	5 E Ee	7 s 2 1	nu4 1561.20060	-4.2	6.34E-03	1.1	-1.7	3
(P)P (4,A-,3,a)	3 A- A2o	2 a 2-1	nu4 1561.38333	-1.9	1.21E+00	0.9	3.3	3
(R)P (3,E,1,s)	2 E Ee	2 s 2 1	nu4 1561.76078	-1.4	4.48E-02	2.0	0.2	5
** (O)P (5,A-,3,s)	4 A- A2e	3 a 1 1	nu4 1562.09908	-5.9	1.23E-02	1.7	-9.2	5
(R)P (3,E,1,a)	2 E Eo	2 a 2 1	nu4 1562.36010	-0.1	4.57E-02	3.7	2.8	6
** (O)P (13,A+,12,s)	12 A+ A2o	2 a 10 1	nu4 1562.79262	-3.6	5.77E-04	2.1	5.3	2
** (M)P (7,E,4,s)	6 E Eo	11 a 0 1	nu4 1563.39857	-1.5	5.03E-04	0.3	4.5	2
** (O)P (6,E,4,s)	5 E Ee	7 a 2 1	nu4 1563.10613	-2.2	4.82E-03	3.2	-6.0	2
** (O)P (7,E,5,s)	6 E Ee	8 a 3 1	nu4 1563.65494	-2.0	8.06E-01	3.9	3.3	4
** (P)P (4,E,4,s)	3 E Eo	1 s 3-1	nu4 1563.82402	0.3	7.92E-01	0.7	2.1	3
(P)P (4,E,4,a)	3 E Ee	2 a 3-1	nu4 1564.08208	-3.9	6.20E-03	2.2	-12.5	2
** (S)Q (8,A+,3,a)	8 A- A2e	4 a 5-1	nu4 1564.22726	2.1	7.23E-04	4.0	-9.2	2
** (O)P (11,E,10,s)	10 E Eo	4 a 8 1	nu4 1565.60739	-1.2	1.07E-03	0.6	-5.5	2
** (N)P (8,E,7,s)	7 E Ee	4 a 4 0	2nu2 1565.69441	-1.8	2.02E-02	2.0	-9.7	7
(Q)Q (11,E,11,a)	11 E Eo	1 s 11 0	2nu2 1565.80805	0.0	9.88E-03	1.0	4.1	2
** (O)P (3,E,1,s)	2 E Ee	3 a 1-1	nu4 1565.98460	-1.6	2.03E-03	3.5	-6.7	4
** (S)Q (5,A+,3,a)	4 A+ A2o	4 s 1 1	nu4 1566.2158	6.0	1.28E-03	1.3	-11.4	2
** (O)P (9,A+,3,a)	8 A+ A2e	4 s 5-1	nu4 1566.22620	-1.4	4.43E-03	3.3	-6.4	4
** (N)P (10,A+,9,s)	9 A+ A2e	5 s 0 2	nu4 1566.34843	-1.2	2.03E-03	3.5	-6.7	4
** (P)P (9,E,8,s)	8 E Ee	5 s 0 2	nu4 1566.43124	-0.1	1.21E-03	0.7	-1.5	2
** (O)P (8,E,1,s)	7 E Ee	7 a 5 1	nu4 1566.95596	-1.4	3.04E-04	0.3	-13.5	2
** (M)P (8,E,5,s)	7 E Ee	12 s 1-1	nu4 1567.00504	-1.5	2.65E-04	1.6	5.1	2
** (Q)P (14,E,13,a)	14 E Eo	2 s 13 0	2nu2 1567.17712	-0.5	1.82E-03	0.7	-9.4	2
(R)P (3,A+,0,s)	2 A+ A2o	2 s 1 1	nu4 1567.99300	2.1	7.09E-01	1.1	4.5	3
** (S)Q (9,A-,3,a)	9 A- A2e	4 a 5-1	nu4 1569.54470	1.9	4.26E-03	0.1	-10.3	2
(R)Q (12,E,11,s)	12 E Ee	2 s 12 1	nu4 1570.15916	-4.2	6.35E-03	0.9	4.1	2
** (Q)P (11,E,10,a)	10 E Ee	6 s 8 1	nu4 1570.64654	0.3	1.28E-03	1.3	-11.4	2
** (S)Q (4,E,2,s)	4 E Eo	1 a 4-1	nu4 1570.68773	-3.6	2.65E-03	2.0	8.2	3
** (Q)P (10,E,10,s)	10 E Eo	1 s 10 0	2nu2 1571.25852	1.4	1.95E-02	2.8	-3.7	5
** (S)Q (5,E,2,s)	5 E Eo	3 a 4-1	nu4 1571.36617	-0.1	4.30E-03	2.2	-5.9	4
** (S)Q (10,A-,3,a)	10 A- A2e	5 s 5-1	nu4 1571.53001	-1.5	2.50E-03	2.6	-10.6	2
(P)P (3,E,1,s)	2 E Ee	4 s 0 1	nu4 1571.83146	-0.2	3.41E-01	0.9	3.5	4
(P)P (3,E,1,a)	2 E Ee	4 a 0 1	nu4 1572.48814	0.1	3.68E-01	1.4	3.3	5
(Q)Q (13,A-,12,a)	13 A- A2e	2 s 12 0	2nu2 1572.87814	-1.1	8.49E-03	1.0	-2.8	4
** (S)Q (5,E,2,s)	5 E Eo	3 a 4-1	nu4 1573.34940	-1.5	4.94E-03	3.1	2.9	5
** (O)P (9,E,8,s)	8 E Ee	5 s 6 1	nu4 1574.09503	0.5	3.14E-03	3.5	-15.1	4
** (S)Q (6,E,2,s)	6 E Ee	5 s 4-1	nu4 1574.38297	-0.8	5.23E-03	3.6	-6.5	5
(P)P (3,E,2,s)	2 E Ee	3 s 1-1	nu4 1575.85182	-0.7	4.92E-01	3.9	0.2	3
** (S)Q (7,E,2,s)	7 E Ee	6 s 4-1	nu4 1577.97652	-1.2	5.14E-03	3.7	-1.6	6
(Q)Q (12,E,11,a)	12 E Ee	3 s 11 0	2nu2 1578.21424	-1.5	9.14E-03	3.4	1.1	7
** (P)P (3,A-,3,s)	2 A- A2e	1 s 2-1	nu4 1579.36175	-0.2	1.49E+00	0.7	3.1	3
** (O)P (10,A+,9,s)	9 A+ A2e	3 a 7 1	nu4 1580.44409	-1.9	2.49E-03	0.2	0.7	2
** (O)P (8,E,7,s)	7 E Ee	5 a 5 1	nu4 1580.50270	1.0	4.22E-03	2.4	12.0	3
** (O)P (7,A+,6,s)	6 A+ A2o	3 a 4 1	nu4 1580.83558	-0.5	9.48E-03	2.9	-7.9	8
** (P)P (6,E,5,s)	5 E Ee	6 a 3 1	nu4 1581.33496	-1.0	5.22E-03	1.9	-12.8	5
(R)Q (10,A+,9,s)	10 A- A2e	1 s 10 1	nu4 1581.63490	-3.1	5.01E-02	3.0	8.5	5
** (O)P (5,E,4,s)	4 E Ee	5 a 2 1	nu4 1581.82158	-1.3	5.13E-03	3.5	-9.7	2
** (S)Q (3,E,2,s)	2 E Ee	4 s 0 1	nu4 1582.18362	-0.9	4.28E-03	5.2	9.7	2
** (N)P (8,E,8,s)	7 E Ee	6 a 5-1	nu4 1582.53224	-1.1	1.23E-03	2.7	-10.0	3
** (S)Q (11,A-,3,a)	11 A- A2e	6 a 5 0	2nu2 1582.81828	-3.3	9.18E-04	1.9	-3.1	2
** (Q)P (2,E,1,s)	1 E Ee	2 s 1-1	nu4 1582.87705	-1.3	3.90E-04	0.5	-1.3	2
(Q)Q (11,E,10,a)	11 E Ee	2 s 10 0	2nu2 1583.19061	-1.4	1.75E-02	3.2	-1.5	10
(Q)Q (14,A+,12,a)	14 A- A2e	3 s 12 0	2nu2 1583.61133	-2.9	2.73E-03	2.2	-11.4	5
** (O)P (3,E,2,s)	2 E Ee	4 a 0 1	nu4 1584.34444	0.2	1.90E-03	1.2	-6.3	2
** (Q)P (11,E,11,a)	10 E Ee	3 s 9 1	nu4 1584.37623	-0.2	1.03E-03	0.5	-11.7	2
(Q)P (7,E,7,a)	7 E Ee	1 s 7 0	2nu2 1584.62736	0.2	6.59E-02	3.9	1.2	9
** (S)Q (8,E,2,s)	8 E Ee	8 a 4-1	nu4 1585.48515	1.6	4.02E-03	3.8	-1.2	9
** (O)P (4,A+,3,s)	3 A+ A2e	3 a 1 1	nu4 1586.12028	6.8	7.34E-03	1.6	-6.3	10
(R)P (10,E,10,s)	9 E Ee	4 s 8 1	nu4 1586.61878	0.6	1.65E-03	0.7	-13.5	2
** (O)P (2,A+,0,s)	1 A+ A2e	2 a 1 1	nu4 1586.87147	-0.7	4.51E-01	1.6	2.6	4
** (S)Q (9,E,2,s)	9 E Ee	10 a 4-1	nu4 1586.97694	0.2	2.89E-03	8.0	7.5	2
(R)Q (9,E,8,s)	9 E Ee	2 s 9 1	nu4 1587.12189	-2.2	4.33E-02	3.0	6.4	10
(Q)Q (11,A-,9,s)	11 A- A2e	2 s 10 1	nu4 1587.29376	-0.7	3.34E-02	3.5	7.8	11
(Q)Q (12,A-,9,a)	12 A- A2o	2 a 10 1	nu4 1587.49175	-3.5	5.84E-03	3.7	14.0	6
(Q)Q (6,A+,6,a)	6 A+ A2e	1 s 6 0	2nu2 1588.02913	0.3	1.74E-01	2.2	3.5	6
(Q)Q (13,E,11,a)	13 E Ee	5 s 11 0	2nu2 1588.23449	-4.7	3.81E-03	3.1	8.5	4
(R)Q (13,E,10,s)	13 E Ee	6 s 11 1	nu4 1588.57227	1.4	3.25E-03	2.4	4.2	5
** (O)P (9,A+,9,s)	8 A+ A2o	2 s 7 1	nu4 1588.76877	0.2	5.18E-03	3.6	-8.3	8
** (S)Q (4,E,1,s)	4 E Eo	2 s 3 1	nu4 1588.84509	-0.7	4.66E-03	3.3	-1.3	9
(R)Q (14,E,10,s)	14 E Ee	6 s 11 1	nu4 1589.84509	-10.1	5.48E-04	0.8	0.3	2
** (S)Q (12,A+,3,s)	12 A+ A2e	7 a 5-1	nu4 1590.20078	0.3	6.46E-04	3.0	6.2	2
** (U)Q (7,A-,0,s)	7 A- A2o	4 a 4 1	nu4 1590.25643	-1.3	1.84E-03	4.0	-13.0	4
(P)P (2,E,1,s)	1 E Ee	2 s 0 1	nu4 1590.69160	-0.8	2.85E-01	0.8	1.8	4
(Q)Q (5,E,5,s)	5 E Ee	1 s 5 0	2nu2 1590.88041	0.4	1.02E-01	1.7	2.6	7
(P)P (2,E,1,a)	1 E Ee	3 a 0 1	nu4 1591.10494	-1.4	2.94E-01	1.1	1.5	4
** (S)Q (5,E,1,s)	5 E Ee	4 a 3-1	nu4 1591.33128	-0.6	6.62E-03	3.5	-0.2	7
(R)Q (11,E,8,s)	11 E Ee	5 a 9 1	nu4 1591.43837	-2.3	5.25E-03	3.9	10.5	7
(R)Q (10,E,8,s)	10 E Ee	3 s 9 1	nu4 1592.16478	1.0	3.25E-02	2.8	6.7	11
(Q)Q (9,E,8,s)	9 E Ee	3 a 9 1	nu4 1592.21111	0.2	5.75E-02	3.4	-1.6	10
** (S)Q (10,E,2,s)	10 E Ee	14 s 4-1	nu4 1592.39114	-0.1	1.37E-03	1.8	-13.4	2
(P)P (8,E,7,s)	8 E Ee	2 s 8 1	nu4 1592.44915	-1.1	7.36E-02	3.2	8.5	7

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
** (O)P (7,E,7,a)	6 E Eo	4 s 5 1	nu4 1592.77931	0.1	4.72E-03	3.7	-0.6	5
(R)Q (12,A+,9,s)	12 A- A2e	3 s 10 1	nu4 1592.99774	0.8	1.57E-02	2.5	9.8	10
** (S)Q (5,E,1,s)	5 E Ee	5 a 3-1	nu4 1593.60603	0.2	6.87E-03	3.4	-2.7	9
** (S)Q (6,E,1,a)	6 E Ee	6 s 3-1	nu4 1594.39513	-0.8	7.40E-03	0.7	3.9	4
** (O)P (6,A+,6,s)	5 A+ A2e	2 s 4 1	nu4 1594.62927	-0.3	9.28E-03	0.7	-13.3	2
(P)P (2,E,2,s)	1 E Ee	2 s 1-1	nu4 1594.79077	-0.8	5.42E-01	1.3	2.3	4
(Q)Q (3,A+,3,a)	3 A- A2o	1 s 3 0	2nu2 1594.89888	1.8	2.18E-01	1.8	6.2	5
(P)P (2,E,2,a)	1 E Ee	1 a 1-1	nu4 1595.07990	-2.8	5.35E-01	1.6	1.7	4
(Q)Q (5,E,4,s)	5 E Ee	1 s 4 0	2nu2 1595.33476	-4.0	1.12E-02	2.2	-7.0	9
** (O)P (8,E,8,s)	7 E Ee	5 a 6 1	nu4 1595.94998	1.2	2.53E-03	3.0	-10.3	3
(Q)Q (2,E,2,a)	2 E Ee	1 s 2 0	2nu2 1596.05758	3.0	8.84E-02	2.9	8.2	7
(R)Q (8,E,7,a)	8 E Ee	2 a 8 1	nu4 1596.41880	1.6	9.71E-02	1.7	0.8	6
(Q)Q (1,E,1,a)	1 E Ee	1 s 1 0	2nu2 1596.64912	3.6	4.56E-02	3.9	3.6	11
(Q)Q (4,A-,3,a)	4 A+ A2o	1 s 3 0	2nu2 1596.77124	-2.9	4.04E-02	3.6	-2.2	11
(R)Q (9,E,7,s)	9 E Ee	4 s 8 1	nu4 1596.89620	1.1	5.85E-02	2.2	6.4	8
** (S)Q (6,E,1,s)	6 E Ee	7 a 3-1	nu4 1597.09557	1.6	7.32E-03	3.5	-2.3	8
(R)Q (12,E,8,s)	12 E Ee	7 a 9 1	nu4 1597.13161	-4.9	2.84E-03	3.1	1.6	4
(R)Q (11,E,8,s)	11 E Ee	5 s 9 1	nu4 1597.29591	1.0	1.59E-02	3.6	4.3	6
** (S)Q (10,E,2,s)	10 E Ee	12 a 4-1	nu4 1597.49047	-1.9	1.44E-03	3.9	-6.5	2
(Q)Q (3,E,2,a)	3 E Ee	1 s 2 0	2nu2 1597.52415	-1.5	2.32E-02	3.6	-0.1	10
(R)Q (7,A+,6,s)	7 A- A2o	1 s 7 1	nu4 1597.62150	-0.6	2.22E-01	1.5	5.7	6
(Q)Q (2,E,1,a)	2 E Ee	1 s 1 0	2nu2 1597.64348	0.2	1.57E-02	3.5	10.0	7
** (O)P (6,A-,6,s)	5 A- A2o	3 a 4 1	nu4 1597.91759	0.1	9.43E-03	3.7	-2.0	5
** (O)P (4,E,4,s)	3 E Ee	4 s 2 1	nu4 1597.96623	-2.3	4.05E-03	3.7	-2.0	5
(Q)Q (9,A-,6,s)	9 A+ A2e	2 s 6 0	2nu2 1598.02637	-1.4	2.22E-02	2.7	12.4	11
** (S)Q (7,E,1,s)	7 E Ee	8 s 3-1	nu4 1598.06997	-0.1	5.98E-03	3.1	-5.7	9
(R)Q (13,A-,9,s)	13 A+ A2e	4 s 10 1	nu4 1598.66879	-0.3	6.55E-03	3.8	18.9	8
** (O)P (5,E,5,s)	4 E Ee	5 a 3 1	nu4 1599.09049	0.0	4.36E-03	3.6	-5.4	6
(Q)Q (3,E,1,a)	3 E Ee	2 s 1 0	2nu2 1599.19809	-2.1	4.40E-03	3.3	13.2	5
(Q)Q (5,A+,3,a)	5 A- A2o	2 s 3 0	2nu2 1599.30323	-5.7	1.96E-03	5.0	7.4	2
(Q)Q (4,E,2,a)	4 E Ee	3 s 2 0	2nu2 1599.59541	-3.6	3.71E-03	3.5	-1.2	7
(Q)Q (10,E,8,s)	10 E Ee	5 s 8 0	2nu2 1599.85823	-3.2	3.21E-02	1.6	0.8	4
(Q)Q (8,E,5,s)	8 E Ee	5 s 5 0	2nu2 1600.38446	-2.6	1.06E-02	2.7	13.3	12
(R)Q (7,A-,6,a)	7 A+ A2e	2 a 7 1	nu4 1600.58027	1.4	3.11E-01	0.3	5.6	5
** (O)P (3,A-,3,s)	2 A- A2e	2 a 1 1	nu4 1600.67982	-3.9	4.78E-03	3.9	-4.9	8
(R)Q (8,A-,6,s)	8 A+ A2o	2 s 3 1	nu4 1601.36672	1.8	6.81E-03	3.5	3.3	6
** (S)Q (7,E,1,s)	7 E Ee	8 a 3-1	nu4 1601.07043	1.0	3.12E-02	3.4	2.1	9
(R)Q (10,E,7,s)	10 E Ee	6 s 8 1	nu4 1601.49314	1.2	2.02E-01	1.3	7.1	6
(R)Q (8,A-,6,s)	8 A+ A2o	2 s 3 1	nu4 1601.91220	-1.9	6.28E-03	4.0	13.2	9
(Q)Q (7,E,4,s)	7 E Ee	4 a 4 0	nu4 1602.64505	-0.3	1.60E-01	1.3	3.9	7
(R)Q (10,E,6,s)	10 E Ee	2 s 6 1	nu4 1602.97739	-2.2	1.84E-02	3.2	6.9	9
(R)Q (9,E,7,a)	9 E Ee	4 a 8 1	nu4 1603.14683	1.8	5.88E-02	3.8	-2.8	10
(R)Q (6,E,5,s)	6 E Ee	3 a 6 1	nu4 1604.78726	-2.7	2.18E-01	1.5	6.2	6
** (S)Q (2,A+,0,a)	2 A- A2e	1 s 2-1	nu4 1604.80907	-0.4	6.27E-03	3.9	8.0	5
(Q)Q (9,E,5,s)	9 E Ee	7 s 5 0	2nu2 1605.40586	-0.9	1.21E-02	2.9	10.6	11
(Q)Q (9,A+,6,s)	9 A- A2o	3 s 7 1	nu4 1605.52593	1.3	1.23E-01	2.3	6.0	8
(R)Q (6,E,2,a)	6 E Ee	3 s 7 1	nu4 1605.77818	-0.8	1.47E-03	2.7	10.1	2
(Q)Q (12,E,7,s)	12 E Ee	6 s 8 0	2nu2 1605.85293	-2.1	3.17E-03	2.4	10.6	3
(R)Q (7,E,5,s)	7 E Ee	3 s 6 1	nu4 1605.96031	1.0	1.57E-01	1.9	4.2	7
(R)Q (11,E,7,s)	11 E Ee	7 s 8 1	nu4 1606.09091	0.5	1.50E-02	2.8	7.7	11
(Q)Q (8,E,4,s)	8 E Ee	6 s 4 0	2nu2 1606.27041	0.3	1.08E-02	3.4	10.9	12
(R)Q (8,A+,6,s)	8 A- A2e	3 a 7 1	nu4 1606.31605	-0.4	2.18E-01	2.3	1.3	7
** (S)Q (8,E,1,s)	8 E Ee	10 a 3-1	nu4 1606.46283	0.5	4.75E-03	2.6	-6.2	6
(Q)Q (11,E,8,s)	11 E Ee	6 s 8 0	2nu2 1607.48898	-1.2	1.16E-02	3.1	-11.1	8
(R)Q (5,E,4,s)	5 E Ee	2 s 5 1	nu4 1607.52511	-0.3	2.21E-01	1.6	5.0	4
** (S)Q (4,A+,0,a)	4 A- A2e	2 s 2-1	nu4 1608.20239	-0.2	2.54E-02	3.0	-6.0	12
** (S)Q (3,A+,0,s)	3 A- A2o	2 a 2-1	nu4 1608.23343	-1.8	1.78E-02	3.1	-1.5	10
(R)Q (11,A-,6,s)	11 A+ A2e	4 a 7 1	nu4 1608.27054	-2.5	1.20E-02	2.3	9.2	10
(R)Q (5,E,4,s)	5 E Ee	2 a 5 1	nu4 1609.06118	2.5	2.70E-01	1.8	1.7	6
(R)Q (8,E,5,s)	8 E Ee	5 s 6 1	nu4 1609.46549	1.0	1.04E-01	1.3	1.3	4
(R)Q (7,E,5,s)	7 E Ee	5 a 6 1	nu4 1609.50642	0.6	1.81E-01	2.0	2.0	5
(R)Q (10,A-,6,s)	10 A+ A2o	4 s 7 1	nu4 1609.63668	0.8	5.84E-02	3.9	1.3	9
(Q)Q (7,E,2,a)	7 E Ee	7 s 2 0	2nu2 1609.95897	2.4	3.60E-03	3.1	10.2	6
(P)P (1,E,1,s)	0 E Ee	1 s 0 1	nu4 1610.10146	-1.3	2.01E-01	2.9	-0.6	7
(R)Q (10,E,5,s)	10 E Ee	9 a 6 1	nu4 1610.14172	1.8	9.83E-03	3.8	11.7	10
(R)Q (6,E,4,s)	6 E Ee	4 s 5 1	nu4 1610.30236	0.6	2.36E-01	2.2	3.7	7
(P)P (1,E,1,s)	0 E Ee	1 a 0 1	nu4 1610.40837	-2.6	2.00E-01	2.5	-0.6	7
(R)Q (12,E,7,s)	12 E Ee	10 s 8 1	nu4 1610.68681	-0.1	5.31E-03	2.3	-1.1	5
(Q)Q (8,A-,3,s)	8 A+ A2o	4 s 3 0	2nu2 1611.15374	1.7	1.69E-02	3.8	9.2	11
(Q)Q (9,E,4,s)	9 E Ee	8 s 4 0	2nu2 1611.19372	0.0	1.11E-02	3.8	8.0	11
(R)Q (9,A-,6,s)	9 A+ A2e	3 a 7 1	nu4 1612.12296	-1.3	1.14E-01	2.7	0.9	8
(R)Q (4,A+,3,s)	4 A- A2e	1 s 4 1	nu4 1612.26753	-0.5	5.72E-01	1.6	5.8	4
(R)Q (6,E,4,s)	6 E Ee	4 a 5 1	nu4 1612.81742	1.1	2.71E-01	2.6	1.3	6
(R)Q (9,E,5,s)	9 E Ee	7 s 6 1	nu4 1613.07530	0.7	7.78E-02	2.6	2.2	11
(R)Q (7,E,4,s)	7 E Ee	6 s 5 1	nu4 1613.29217	0.5	1.78E-01	2.1	4.4	6
(R)Q (4,A-,3,s)	4 A+ A2e	2 a 4 1	nu4 1613.37098	1.7	6.68E-01	2.0	4.0	4
** (S)Q (5,A-,0,s)	5 A- A2o	4 a 2-1	nu4 1613.39706	1.7	3.90E-02	3.0	-3.7	8
(R)Q (12,A+,6,s)	12 A- A2e	5 a 7 1	nu4 1613.60406	2.1	5.60E-03	3.3	1.6	4
(R)Q (11,A+,6,s)	11 A- A2o	5 s 7 1	nu4 1613.75313	0.6	2.56E-02	2.6	3.5	10
** (S)Q (6,A+,0,a)	6 A- A2e	4 s 2-1	nu4 1613.87187	1.1	3.65E-02	3.6	-5.4	10
(R)Q (8,E,5,s)	8 E Ee	6 a 6 1	nu4 1614.34521	-0.6	1.09E-01	3.4	1.7	8
(R)Q (5,A-,3,s)	5 A+ A2e	2 s 4 1	nu4 1614.52314	0.0	6.79E-01	1.6	5.7	4
(Q)Q (8,E,2,a)	8 E Ee	9 s 2 0	2nu2 1614.85442	3.0	4.70E-03	3.0	4.5	7
(R)Q (13,E,7,s)	13 E Ee	12 s 8 1	nu4 1615.20357	-0.6	1.92E-03	0.4	5.0	2
(R)Q (5,A+,3,s)	5 A- A2o	3 a 4 1	nu4 1616.26607	0.9	7.67E-01	1.2	3.4	3

	(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)	
(Q)Q	(9,A+,3,a)	9A- A2o	5 s 3 0	2nu2	1616.35111	0.9	1.73E-02	2.9	4.8	8
(R)Q	(8,E,4,s)	8E Eo	7 s 5 1	nu4	1616.40663	0.2	1.07E-01	2.6	3.0	3
(R)Q	(10,E,4,a)	10E Ee	10 s 5 1	nu4	1616.42118	-1.7	9.68E-03	3.8	14.8	4
(R)Q	(6,A+,3,s)	6A- A2e	3 s 4 1	nu4	1617.00681	-0.4	5.57E-01	1.4	4.6	3
(Q)R	(0,A+,0,a)	1A+ A2e	1 s 0 0	2nu2	1617.05576	3.9	8.92E-02	2.5	6.1	5
(Q)R	(8,E,1,a)	8E Eo	11 s 1 0	2nu2	1617.28516	5.9	1.24E-03	2.2	10.0	2
(R)Q	(3,E,2,a)	3E Ee	3 s 3 1	nu4	1617.67315	0.9	3.69E-01	2.7	1.2	6
(R)Q	(12,A-,6,s)	12A- A2o	6 s 7 1	nu4	1617.81837	0.2	9.75E-03	3.5	5.4	10
(R)Q	(4,E,2,s)	4E Eo	4 s 3 1	nu4	1618.62494	-0.7	4.35E-01	0.6	3.0	3
(R)Q	(6,A-,3,a)	6A+ A2e	3 s 4 1	nu4	1619.31622	-0.5	6.16E-01	0.8	3.2	3
** (Q)	(9,E,5,a)	9E Eo	8 s **	**	1619.37210	-0.3	5.00E-02	3.4	-3.5	5
(R)Q	(9,E,4,s)	9E Eo	9 s 5 1	nu4	1619.56890	0.5	5.49E-02	3.4	1.2	9
(R)Q	(7,A-,3,s)	7A+ A2e	4 s 4 1	nu4	1619.62296	-0.7	3.79E-01	1.4	5.0	5
(R)Q	(4,E,2,a)	4E Ee	5 s 3 1	nu4	1619.80690	0.3	4.91E-01	1.3	2.9	3
(R)Q	(11,E,5,s)	11E Ee	11 s 6 1	nu4	1620.32821	1.4	1.20E-02	3.4	8.7	8
(R)Q	(5,E,2,s)	5E Eo	6 s 3 1	nu4	1620.60142	-1.2	4.09E-01	1.1	4.5	5
(R)Q	(8,E,4,a)	8E Ee	7 s 5 1	nu4	1620.74401	-0.2	1.08E-01	2.5	2.2	7
(R)Q	(2,E,1,s)	2E Ee	2 s 2 1	nu4	1621.35884	-1.2	3.66E-01	1.4	1.6	5
(R)Q	(11,E,4,a)	11E A2o	12 s 5 1	nu4	1621.54168	-0.4	6.01E-03	3.8	12.5	8
(R)Q	(10,E,3,a)	10A+ A2o	6 s 4 1	nu4	1621.76121	-0.4	1.54E-02	3.7	3.8	9
** (S)Q	(8,A+,0,a)	8A- A2e	6 s 2-1	nu4	1621.95239	2.6	3.56E-02	1.7	-1.6	8
(R)Q	(5,E,2,a)	5E Ee	6 s 3 1	nu4	1622.08705	-1.2	4.49E-01	1.0	2.9	4
(R)Q	(8,A+,3,s)	8A- A2e	5 s 4 1	nu4	1622.29993	-0.9	2.23E-01	0.9	6.6	5
(R)Q	(7,A+,3,a)	7A- A2o	4 s 4 1	nu4	1622.42647	-1.4	3.99E-01	1.2	3.2	4
(R)Q	(6,E,2,s)	6E Eo	8 s 3 1	nu4	1622.70842	-1.7	3.05E-01	0.4	3.4	4
(R)Q	(10,E,4,s)	10E Eo	11 s 5 1	nu4	1622.72144	1.3	2.71E-02	3.8	9.0	5
(R)Q	(12,E,5,s)	12E Ee	13 s 6 0	nu4	1623.87537	-0.1	3.39E-03	2.9	8.8	4
(Q)Q	(11,A-,6,s)	11A- A2e	5 s 6 0	2nu2	1624.64589	0.1	1.58E-02	3.4	-0.3	9
** (Q)	(10,E,5,a)	10E Eo	10 s **	**	1624.73415	0.3	1.99E-02	3.2	-1.8	0
(R)Q	(4,E,1,a)	4E Eo	5 s 2 1	nu4	1624.86273	-1.4	6.40E-01	3.1	4.4	4
(R)Q	(7,E,2,s)	7E Eo	10 s 3 1	nu4	1624.89556	-0.1	1.89E-01	2.0	3.1	6
(R)Q	(1,A+,0,s)	1A- A2o	1 s 1 1	nu4	1625.46453	-2.5	1.21E+00	1.4	1.9	3
(R)Q	(5,E,1,s)	5E Ee	7 s 2 1	nu4	1625.51711	-3.9	4.89E-01	2.0	3.5	4
(R)Q	(8,A-,3,a)	8A+ A2o	5 s 4 1	nu4	1625.60930	1.1	2.18E-01	1.5	3.2	5
(R)Q	(11,E,4,s)	11E Eo	13 s 5 1	nu4	1625.83006	2.0	1.04E-02	3.4	4.3	9
(R)Q	(2,A+,0,s)	2A- A2e	2 s 1 1	nu4	1626.67159	-1.4	2.04E-01	3.4	1.4	6
(R)Q	(7,E,2,a)	7E Ee	9 s 3 1	nu4	1626.82588	-2.1	1.09E-02	2.8	4.8	9
(R)Q	(11,A+,3,s)	11A- A2o	7 s 4 1	nu4	1626.93171	-3.6	1.05E-01	2.0	2.9	7
(R)Q	(8,E,2,s)	8E Eo	10 s 3 1	nu4	1626.93171	-3.6	1.05E-01	2.0	2.9	7
(R)Q	(6,E,1,s)	6E Ee	9 s 2 1	nu4	1627.04778	-4.3	3.50E-01	1.4	4.3	5
(R)Q	(4,A+,0,a)	4A- A2e	3 s 1 1	nu4	1627.32144	-6.3	1.53E+00	2.2	4.0	3
(R)Q	(10,A+,3,s)	10A- A2e	7 s 4 1	nu4	1627.62907	0.4	4.75E-02	3.6	2.5	5
(R)Q	(7,E,1,s)	7E Ee	10 s 2 1	nu4	1628.61048	-3.1	2.12E-01	0.9	3.4	6
** (P)Q	(8,E,2,s)	8E Eo	11 s 1 0	2nu2	1628.63689	6.4	3.85E-03	3.5	7.6	4
(R)Q	(12,E,4,s)	12E Eo	15 s 5 1	nu4	1628.88243	-0.3	3.51E-03	1.2	-0.8	4
** (Q)	(9,A+,3,s)	9A- A2o	6 s **	**	1628.92256	0.1	9.58E-02	2.3	1.2	7
(R)Q	(8,E,2,a)	8E Ee	11 s 3 1	nu4	1628.96950	0.9	1.09E-01	1.9	1.5	7
(R)Q	(9,E,2,s)	9E Eo	12 s 3 1	nu4	1629.11285	-0.3	5.33E-02	3.4	3.4	9
(R)Q	(6,A+,0,a)	6A- A2e	5 s 1 1	nu4	1629.19084	-6.7	7.50E-01	2.4	4.6	4
(R)Q	(7,E,1,a)	7E Eo	11 s 2 1	nu4	1629.31306	0.8	2.15E-01	3.7	1.5	7
(Q)Q	(10,E,1,a)	10E Eo	15 s 1 0	2nu2	1629.36371	-7.9	3.60E-03	3.3	8.2	5
** (Q)	(10,E,4,a)	10E Ee	11 s **	**	1629.59347	-0.8	1.80E-02	2.4	-0.4	1
(R)Q	(4,E,1,s)	4E Ee	7 s 1-1	nu4	1629.71463	2.2	2.61E-03	2.8	-6.0	5
(R)Q	(11,A-,3,s)	11A- A2e	8 s 4 1	nu4	1630.22217	6.6	1.86E-02	2.1	1.4	4
(R)Q	(8,E,1,s)	8E Ee	12 s 2 1	nu4	1630.23355	-0.6	1.14E-01	2.9	4.3	7
(R)Q	(7,A+,0,s)	7A- A2o	6 s 1 1	nu4	1630.30885	-5.4	4.14E-01	1.9	4.8	4
(P)Q	(1,E,1,s)	1E Ee	2 s 0 1	nu4	1630.45751	-0.6	2.67E-01	2.4	-0.4	6
(Q)Q	(11,E,5,a)	11E Eo	12 s 5 0	2nu2	1630.67485	-4.7	6.17E-03	3.4	-2.0	6
(R)Q	(10,A+,0,a)	10A- A2e	8 s 1 1	nu4	1630.72280	1.5	3.07E-02	2.6	-3.8	6
(P)Q	(1,E,1,a)	1E Eo	3 s 0 1	nu4	1630.85087	-1.4	2.50E-01	3.0	-2.4	7
(R)Q	(8,E,1,a)	8E Eo	12 s 2 1	nu4	1630.88848	3.7	1.13E-01	2.1	2.0	8
(R)Q	(9,A+,0,s)	9A- A2o	7 s 1 1	nu4	1630.94692	3.9	8.98E-02	2.9	2.0	8
(R)Q	(11,E,2,a)	11E Ee	15 s 3 1	nu4	1631.11477	-1.6	5.79E-03	2.8	9.4	8
** (Q)	(9,E,2,a)	9E Ee	14 s 3 1	nu4	1631.27704	2.4	2.28E-02	3.5	2.2	11
** (Q)	(9,E,1,s)	9E Ee	13 s **	**	1631.42230	2.8	5.54E-02	2.2	13.0	2
(R)Q	(12,A+,6,s)	12A- A2e	6 s 6 0	2nu2	1631.76583	4.0	4.12E-03	3.7	-4.2	8
(R)Q	(8,A+,0,a)	8A- A2e	7 s 1 1	nu4	1631.88397	-6.5	2.10E-01	0.9	5.1	4
(R)Q	(9,E,1,s)	9E Ee	14 s 2 1	nu4	1631.96193	2.8	5.18E-02	3.2	2.4	9
(P)Q	(2,E,1,a)	2E Eo	4 s 0 1	nu4	1632.05719	0.1	2.80E-01	3.7	-1.8	5
** (Q)	(9,E,1,a)	9E Eo	14 s **	**	1632.63263	5.5	5.24E-02	3.1	3.2	9
** (Q)	(10,A-,3,a)	10A+ A2o	7 s **	**	1632.83115	1.0	3.43E-02	3.9	0.3	0
(R)Q	(12,A+,3,s)	12A- A2e	9 s 4 1	nu4	1632.87338	-6.6	7.08E-03	2.8	10.9	10
(P)Q	(3,E,1,s)	3E Ee	6 s 0 1	nu4	1632.99920	1.1	2.57E-01	3.6	-1.9	7
(R)Q	(11,E,2,s)	11E Eo	16 s 3 1	nu4	1633.48190	3.9	1.13E-03	3.7	6.8	8
(P)Q	(3,E,1,a)	3E Eo	6 s 0 1	nu4	1634.06701	2.6	2.06E-01	2.8	-1.3	7
(R)Q	(11,E,1,a)	11E Eo	17 s 2 1	nu4	1634.53031	0.1	5.86E-03	3.9	5.1	8
(R)Q	(12,E,2,a)	12E Ee	17 s 3 1	nu4	1634.72233	0.4	2.61E-03	1.7	2.8	5
(P)Q	(10,E,1,a)	10E Eo	16 s 0 1	nu4	1634.83048	0.5	1.87E-02	3.2	1.2	7
(Q)Q	(11,E,4,a)	11E Ee	13 s 4 0	2nu2	1635.01127	-13.0	5.80E-03	1.0	11.6	2
** (S)Q	(9,A+,0,s)	9A- A2o	8 s 2-1	nu4	1635.67012	-6.0	2.47E-02	1.8	10.2	2
(R)Q	(12,E,2,s)	12E Eo	17 s 3 1	nu4	1635.77937	-6.8	2.80E-03	2.4	1.9	2
(P)Q	(3,E,2,s)	3E Ee	5 s 1-1	nu4	1636.88755	-0.6	2.61E-01	1.7	-1.5	6
(P)Q	(4,E,1,a)	4E Ee	7 s 0 1	nu4	1637.02896	5.1	1.08E-01	2.2	-1.2	7
** (Q)	(10,A+,0,a)	10A- A2e	9 s **	**	1637.11861	-12.7	1.68E-02	3.3	6.0	9
(R)Q	(1,E,1,a)	2E Eo	1 s 1 0	2nu2	1637.38951	0.4	7.09E-02	5.2	-2.4	2

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
(P)Q (5,E,1,s)	5 E Ee	9 s 0 1	nu4	1638.31879	4.2	7.62E-02	1.4	-2.5 6
(P)Q (4,E,2,s)	4 E Eo	6 s 1-1	nu4	1638.86779	-0.7	2.05E-01	2.0	-2.2 7
(Q)Q (13,A-,6,a)	13 A- A2e	7 s 6 0	2nu2	1639.69047	26.3	1.08E-03	2.1	12.5 2
(P)Q (4,E,2,a)	4 E Ee	7 a 1-1	nu4	1640.06776	2.0	1.64E-01	2.9	-0.6 6
(P)Q (3,A+,3,a)	3 A- A2o	2 s 2-1	nu4	1640.81344	-1.9	2.98E-01	1.1	-1.6 5
(P)Q (5,E,1,a)	5 E Eo	9 s 0 1	nu4	1640.99234	5.6	4.34E-02	3.6	-2.0 10
(P)Q (5,E,2,s)	5 E Eo	8 s 1-1	nu4	1641.48723	-0.7	1.27E-01	1.4	-2.5 8
(P)Q (4,A-,3,s)	4 A- A2e	2 s 2-1	nu4	1642.16533	-0.1	3.74E-01	0.0	1.3 2
(P)Q (4,A-,3,a)	4 A- A2o	3 s 2-1	nu4	1642.99367	-0.1	1.11E-01	0.8	0.2 4
(P)Q (5,E,2,a)	5 E Eo	8 s 1-1	nu4	1643.36976	3.3	9.01E-02	2.0	-0.2 7
(P)Q (6,E,2,s)	6 E Eo	10 s 1-1	nu4	1644.80480	-0.8	6.38E-02	3.0	-2.2 9
(P)Q (4,E,4,a)	4 E Eo	2 s 3-1	nu4	1645.09921	0.2	1.11E-01	1.0	-6.3 8
(P)Q (4,E,2,a)	4 E Ee	4 s 3-1	nu4	1645.57625	-2.0	9.54E-02	2.5	-5.8 5
** (O)Q (4,E,2,a)	4 E Ee	8 s 0 1	nu4	1645.62385	2.6	4.74E-03	2.3	-9.4 5
(P)Q (6,E,1,a)	6 E Eo	11 s 0 1	nu4	1645.90324	3.7	1.52E-02	3.1	2.7 5
** (S)R (1,A+,0,s)	2 A+ A2o	1 a 2-1	nu4	1646.40418	-3.2	3.43E-03	2.6	-11.5 3
(R)R (0,A+,0,a)	1 A+ A2e	2 a 1 1	nu4	1646.49176	1.4	7.24E-01	1.3	-0.4 3
(P)Q (7,E,1,s)	7 E Ee	12 s 0 1	nu4	1646.74201	2.7	1.02E-02	4.0	-3.7 10
(Q)P (11,E,5,s)	10 E Eo	20 s 5 0	2nu2	1647.00412	-0.8	2.29E-04	3.8	-7.5 2
(P)Q (5,E,4,s)	5 E Eo	4 s 3-1	nu4	1647.30914	-0.1	1.08E-01	2.1	-7.8 2
(Q)P (11,A-,6,s)	10 A- A2o	10 s 6 0	2nu2	1647.83085	-0.1	5.15E-04	1.2	-0.9 2
(P)Q (5,E,4,a)	5 E Ee	5 s 3-1	nu4	1648.16595	0.1	9.11E-02	2.0	-3.3 3
** (S)R (3,E,2,a)	4 E Ee	2 s 4-1	nu4	1648.26882	0.5	4.58E-03	3.7	6.6 3
** (O)Q (5,E,2,a)	5 E Ee	9 s 0 1	nu4	1648.67032	4.1	4.68E-03	3.0	-4.6 5
** (O)Q (4,E,2,s)	4 E Eo	7 s 0 1	nu4	1648.81124	5.1	3.41E-03	2.9	-9.7 5
(P)Q (7,E,2,s)	7 E Ee	12 s 1-1	nu4	1648.85313	-1.4	2.71E-02	2.3	0.1 7
(P)Q (6,A-,3,s)	6 A- A2o	4 s 2-1	nu4	1649.55786	1.8	1.08E-01	2.1	0.7 7
(P)Q (5,E,5,s)	5 E Ee	3 s 4-1	nu4	1649.71418	0.3	6.98E-02	3.6	-7.8 8
** (S)R (4,A-,3,a)	5 A- A2o	1 s 5-1	nu4	1649.93680	2.0	1.14E-02	3.3	3.7 10
(P)Q (6,E,4,s)	6 E Eo	6 s 3-1	nu4	1650.04952	0.0	7.45E-02	1.9	-4.1 9
** (S)R (3,E,2,s)	4 E Eo	1 a 4-1	nu4	1650.09453	-3.8	4.48E-03	2.8	0.1 6
(P)Q (5,E,5,s)	5 E Eo	3 s 4-1	nu4	1650.19853	-2.1	5.93E-02	3.9	-4.5 11
(Q)P (11,E,8,s)	10 E Eo	17 s 8 0	2nu2	1650.76108	0.6	2.04E-04	6.7	-7.3 3
(P)Q (7,A-,3,s)	7 A+ A2e	6 s 2-1	nu4	1651.12925	0.6	1.35E-02	0.9	-2.0 8
(P)Q (6,E,4,a)	6 E Ee	1 s 6-1	nu4	1651.43513	1.3	5.68E-02	3.7	-0.9 8
** (S)R (5,E,2,s)	7 E Ee	1 s 6-1	nu4	1651.47138	2.6	5.90E-03	3.5	-0.4 7
(P)Q (7,E,1,a)	7 E Eo	13 s 0 1	nu4	1651.66801	-0.7	4.26E-03	2.9	0.9 8
** (S)R (4,A+,3,s)	5 A+ A2e	1 a 5-1	nu4	1651.76226	-4.0	1.15E-02	3.8	0.6 9
(P)Q (8,E,1,s)	8 E Ee	14 s 0 1	nu4	1652.01237	0.3	3.22E-03	2.9	0.2 3
(P)Q (6,E,5,s)	6 E Ee	5 s 4-1	nu4	1652.29215	-0.5	6.04E-02	3.9	-12.1 5
** (O)Q (6,E,2,a)	6 E Ee	11 s 0 1	nu4	1652.50254	4.2	3.55E-03	1.5	-2.0 3
(P)Q (7,E,2,a)	7 E Ee	11 s 1-1	nu4	1652.73754	-0.2	1.35E-02	3.3	0.7 8
** (S)R (6,E,5,a)	7 E Ee	2 s 7-1	nu4	1652.87052	0.3	3.60E-02	3.5	8.6 5
** (S)R (6,E,5,s)	6 E Eo	5 s 1-1	nu4	1653.18497	-0.2	4.92E-02	2.8	-6.3 5
(P)Q (7,E,4,s)	7 E Eo	1 a 6-1	nu4	1653.30622	-4.4	6.34E-03	2.9	3.5 3
(P)Q (7,E,4,s)	7 E Eo	8 s 3-1	nu4	1653.35547	0.1	3.73E-02	3.7	-7.6 6
(P)Q (8,E,2,s)	8 E Eo	13 s 1-1	nu4	1653.62706	-2.4	9.36E-03	3.1	-0.9 7
(P)Q (7,A+,3,s)	7 A- A2o	5 s 2-1	nu4	1653.78725	2.7	3.64E-02	3.5	1.4 10
** (S)R (7,A-,6,a)	8 A- A2e	1 s 8-1	nu4	1654.13000	4.5	9.84E-03	2.8	5.1 4
(P)Q (6,A-,6,s)	6 A+ A2e	1 s 5-1	nu4	1654.20853	0.7	8.26E-02	2.3	-7.8 5
(P)Q (6,A-,6,a)	6 A- A2e	2 s 5-1	nu4	1654.69440	0.6	6.59E-02	2.9	7.1 5
** (S)R (6,E,5,s)	7 E Ee	1 s 7-1	nu4	1654.70444	-3.1	5.34E-03	3.7	-7.1 4
(P)Q (8,A+,3,s)	8 A- A2e	6 s 2-1	nu4	1655.01799	2.8	2.34E-02	2.1	3.1 9
** (S)R (8,E,7,s)	9 E Eo	1 s 9-1	nu4	1655.24655	4.7	3.92E-03	3.5	9.7 7
(P)Q (7,E,5,s)	7 E Ee	6 s 4-1	nu4	1655.38571	-0.7	3.83E-02	3.5	-5.8 12
(P)Q (7,E,4,a)	7 E Ee	8 s 3-1	nu4	1655.44883	1.5	2.67E-02	2.8	1.8 12
** (S)R (7,A+,6,s)	8 A+ A2o	1 a 8-1	nu4	1656.01171	-3.9	9.94E-03	2.9	3.8 9
** (S)R (9,E,8,a)	10 E Ee	2 s10-1	nu4	1656.21744	4.9	2.68E-03	3.7	8.6 4
(P)Q (7,E,5,a)	7 E Eo	7 s 4-1	nu4	1656.82971	1.2	2.85E-01	1.8	-0.3 12
(Q)R (2,E,2,a)	3 E Ee	1 s 2 0	2nu2	1657.12072	1.2	9.72E-02	2.5	0.8 6
(P)Q (7,A+,6,s)	7 A- A2o	2 s 5-1	nu4	1657.22312	-0.8	7.20E-02	2.5	-0.5 5
(P)Q (8,E,4,s)	8 E Eo	9 s 3-1	nu4	1657.25251	0.8	1.63E-02	2.2	-2.9 11
** (O)Q (7,A-,6,s)	7 A+ A2e	3 s 5-1	nu4	1657.49312	3.6	2.53E-03	3.4	-10.5 6
(P)Q (7,A-,6,a)	7 A- A2e	2 s 5-1	nu4	1658.05049	0.2	5.36E-02	3.9	0.7 11
(P)Q (7,E,7,s)	7 E Ee	2 s 6-1	nu4	1658.58886	0.6	2.39E-02	1.9	-2.6 12
** (O)Q (3,A+,3,a)	3 A- A2o	3 s 1 1	nu4	1658.93181	-5.1	4.48E-03	3.3	3.7 7
(P)Q (8,E,5,s)	8 E Ee	8 s 4-1	nu4	1659.02202	-0.6	1.86E-02	2.3	-1.4 8
(Q)R (2,A+,0,a)	3 A+ A2e	1 s 0 0	2nu2	1659.32992	-2.3	2.46E-01	2.1	6.3 4
(P)Q (8,A-,3,a)	8 A+ A2o	6 s 2-1	nu4	1659.50921	-2.5	1.52E-02	3.1	8.2 11
(P)Q (8,E,4,a)	8 E Ee	10 s 4-1	nu4	1660.00779	9.9	9.90E-03	3.3	6.3 10
** (O)Q (5,A+,3,s)	5 A- A2o	3 s 5-1	nu4	1660.35391	-6.7	1.29E-02	3.3	-8.2 10
(P)Q (8,A-,6,s)	8 A+ A2o	3 s 5-1	nu4	1660.55697	-0.3	3.73E-02	1.5	-4.3 2
(P)Q (8,E,1,s)	8 E Ee	2 s 2 1	nu4	1661.12480	-1.0	4.99E-01	0.2	-0.4 4
(P)Q (8,E,5,a)	8 E Eo	8 s 4-1	nu4	1661.18724	1.3	1.30E-02	2.4	10.1 5
** (O)Q (4,A+,3,s)	4 A- A2e	3 s 1 1	nu4	1661.28432	-6.2	8.71E-03	3.4	-2.6 6
(R)R (1,E,1,a)	2 E Eo	2 s 2 1	nu4	1661.67496	-0.2	4.61E-01	1.3	0.9 4
(P)Q (8,E,7,s)	8 E Ee	4 s 6-1	nu4	1661.83738	-1.1	1.69E-02	3.8	-5.6 9
(P)Q (8,A-,6,a)	8 A- A2e	4 s 5-1	nu4	1662.04377	1.4	2.72E-02	2.3	4.7 12
** (O)Q (7,A+,3,s)	7 A- A2o	6 s 1 1	nu4	1662.47902	-5.4	1.33E-02	2.7	-2.7 10
(P)Q (8,E,8,s)	8 E Eo	8 s 7-1	nu4	1662.52823	1.7	1.7E-02	2.1	-9.5 6
** (O)Q (7,E,2,s)	7 E Ee	13 s 0 1	nu4	1663.14266	-1.5	1.85E-03	7.3	-0.4 2
(P)Q (9,E,7,s)	9 E Eo	10 s 4-1	nu4	1663.21874	-0.3	7.30E-03	4.0	2.4 8
(P)Q (8,E,8,a)	8 E Ee	3 s 7-1	nu4	1663.34044	-1.5	9.07E-03	3.2	0.6 7
(P)Q (10,E,1,s)	10 E Ee	18 s 0 1	nu4	1664.36118	-8.2	2.70E-04	1.3	2.5 2

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)	
(P)Q (9,A, 6,s)	9 A-A2o	4 s 5-1	nu4	1664.49937	-1.4	1.62E-02	2.2	0.0	10
** (O)Q (8,A, 3,s)	8 A-A2e	7 a 1-1	nu4	1664.94918	-6.6	9.19E-03	2.2	-10.1	10
(P)Q (10,E, 2,s)	10 E Eo	18 s 1-1	nu4	1665.17233	-0.9	7.49E-04	2.1	3.9	2
** (Q)R (1,E, 1,s)	2 E Ee	3 a 1-1	nu4	1665.32884	-1.0	9.06E-04	0.4	7.3	2
** (S)R (2,A+, 0,a)	3 A+ A2e	2 s 2-1	nu4	1665.80704	-1.0	8.97E-03	2.6	5.1	11
(P)Q (9,E, 4,a)	9 E Ee	12 a 3-1	nu4	1665.84447	-1.7	3.06E-03	3.4	19.5	7
** (U)R (7,A-, 3,s)	8 A- A2e	3 a 7-1	nu4	1666.16571	-0.4	3.00E-04	3.8	17.2	2
(P)Q (9,E, 5,a)	9 E Eo	10 a 4-1	nu4	1666.29641	-0.3	4.24E-03	3.8	13.8	10
(P)Q (9,E, 8,s)	9 E Ee	5 s 7-1	nu4	1666.41483	-1.5	7.82E-03	3.4	-4.6	10
(P)Q (9,A-, 6,a)	9 A- A2e	4 s 5-1	nu4	1666.72033	1.1	1.02E-02	2.0	9.0	11
(P)Q (10,E, 4,s)	10 E Eo	13 s 3-1	nu4	1666.79085	2.0	1.66E-03	2.1	4.8	3
(P)Q (9,A-, 9,s)	9 A- A2e	1 s 8-1	nu4	1667.03750	0.6	1.15E-02	3.4	-4.1	10
(P)Q (9,E, 7,a)	9 E Eo	6 a 6-1	nu4	1667.08983	1.7	6.27E-03	3.5	15.7	7
(Q)P (10,E, 1,s)	9 E Ee	19 a 1-0	2nu2	1667.80073	-0.3	4.00E-04	2.4	-10.0	3
** (S)R (3,E, 1,a)	4 E Eo	2 s 3-1	nu4	1668.17794	-0.8	4.72E-03	3.1	1.8	7
(Q)P (10,A-, 6,s)	9 E Ee	18 a 4-0	2nu2	1668.83107	-1.1	4.59E-04	2.7	-3.0	3
(P)Q (10,A+, 3,s)	10 A+ A2o	5 s 5-1	nu4	1668.97397	-1.0	5.35E-03	2.9	-1.2	8
** (P)Q (10,E, 7,s)	10 A- A2e	9 s *	**	1669.59380	-12.3	4.37E-03	3.8	11.0	4
** (S)R (3,E, 1,s)	4 E Ee	4 a 3-1	nu4	1669.79559	-2.0	3.31E-03	1.5	4.4	4
(Q)P (10,A-, 6,s)	9 A- A2o	9 a 6-0	2nu2	1670.20317	-1.7	4.69E-03	2.3	-3.2	6
(P)Q (10,E, 10,s)	10 E Eo	2 s 9-1	nu4	1670.71823	-1.4	9.40E-04	1.3	-5.2	3
(P)R (1,E, 1,s)	2 E Ee	4 a 0-1	nu4	1671.11955	0.2	2.82E-03	2.4	6.3	2
(P)R (1,E, 1,a)	2 E Ee	4 a 0-1	nu4	1671.19544	0.1	8.96E-02	2.8	-7.9	5
(P)Q (10,E, 8,a)	10 E Ee	7 a 7-1	nu4	1671.80115	0.2	8.87E-02	1.6	-6.5	5
(P)Q (10,E, 7,a)	10 E Eo	7 a 6-1	nu4	1671.97997	2.2	2.20E-03	2.7	11.6	3
** (S)R (4,E, 2,s)	5 E Ee	3 a 4-1	nu4	1672.06111	0.9	1.81E-03	3.4	9.8	2
** (S)R (5,A+, 3,a)	6 A+ A2o	1 s 5-1	nu4	1672.45730	-1.7	6.88E-03	2.9	2.3	6
** (Q)Q (6,A-, 3,a)	6 A- A2e	5 s 1-1	nu4	1672.55560	0.0	1.42E-02	3.3	-2.5	11
** (O)Q (5,A-, 3,s)	5 A- A2e	5 s 1-1	nu4	1673.17082	5.9	7.82E-03	4.0	-4.2	8
(P)Q (11,A-, 6,s)	11 A- A2o	6 s 1-1	nu4	1673.62162	7.4	7.19E-03	3.4	-8.1	10
** (S)R (6,E, 4,a)	7 E Ee	2 s 6-1	nu4	1673.97546	0.1	1.62E-03	2.2	10.1	3
** (S)R (5,A-, 3,s)	6 A- A2e	2 s 5-1	nu4	1674.55304	0.3	6.94E-03	3.3	0.4	10
(Q)R (3,A+, 3,a)	4 A+ A2o	1 s 3-0	2nu2	1674.58813	-1.7	1.48E-02	2.7	-1.1	5
** (S)R (7,E, 5,a)	8 E Eo	3 s 7-1	nu4	1676.20133	-2.8	2.59E-01	2.1	4.1	5
(R)R (2,E, 2,s)	3 E Ee	3 s 3-1	nu4	1676.41976	0.5	5.34E-03	3.2	-8.3	6
(R)R (2,E, 2,a)	3 E Ee	3 s 3-1	nu4	1676.50386	-0.6	7.58E-01	2.4	1.7	4
** (S)R (8,A+, 6,a)	9 A+ A2e	1 s 8-1	nu4	1677.26947	0.7	6.81E-01	1.4	1.0	4
** (S)R (7,E, 5,s)	8 E Ee	3 a 7-1	nu4	1678.15288	0.2	8.85E-03	3.9	1.8	9
(Q)R (3,E, 2,a)	4 E Ee	3 s 2-0	2nu2	1678.47643	-1.1	6.07E-03	3.8	2.9	4
** (O)Q (5,E, 4,a)	5 E Ee	7 s 2-1	nu4	1678.96493	-3.4	1.34E-01	2.2	3.1	7
** (S)R (8,A-, 6,s)	9 A- A2o	2 s 8-1	nu4	1680.07724	-3.8	3.54E-03	3.4	2.6	7
(Q)R (3,E, 1,a)	4 E Ee	3 s 1-0	2nu2	1680.23061	-0.6	8.82E-03	3.4	-0.1	7
** (O)Q (4,E, 4,s)	4 E Eo	5 s 2-1	nu4	1680.70270	-3.1	1.22E-01	1.1	0.9	4
** (S)R (10,E, 8,a)	11 E Ee	3 s 10-1	nu4	1680.70270	-3.1	1.22E-01	1.1	0.9	4
(P)Q (11,A-, 3,a)	11 A- A2o	10 a 2-1	nu4	1681.11599	-1.5	1.71E-03	0.9	2.3	2
** (O)Q (6,E, 4,a)	6 E Ee	9 s 2-1	nu4	1681.21006	-0.7	1.84E-03	2.3	-0.6	3
** (S)R (9,E, 7,s)	10 E Ee	3 s 9-1	nu4	1681.33527	16.7	2.60E-04	2.5	3.9	2
(R)R (2,E, 1,s)	3 E Ee	4 s 2-1	nu4	1681.38727	-4.6	3.65E-03	2.4	-4.6	5
** (O)Q (5,A-, 4,s)	5 A- A2e	7 s 2-1	nu4	1681.85580	-0.1	2.88E-03	0.8	-4.4	3
** (R)R (2,E, 1,a)	3 E Ee	4 s 2-1	nu4	1682.19164	-1.4	3.52E-01	1.0	0.2	2
** (O)Q (7,E, 4,s)	7 E Ee	10 s 2-1	nu4	1682.32981	-1.9	3.08E-03	2.4	3.4	3
** (O)Q (7,E, 4,a)	7 E Ee	10 s 2-1	nu4	1682.69259	-3.4	2.76E-03	2.0	-17.8	3
(R)R (2,E, 1,a)	3 E Ee	4 a 2-1	nu4	1682.92107	-0.8	2.75E-01	0.6	-2.1	2
** (O)Q (8,A-, 3,a)	8 A- A2o	7 s 1-1	nu4	1683.38923	0.9	3.60E-03	1.7	-9.8	3
** (Q)R (2,E, 1,s)	3 E Ee	5 s 1-1	nu4	1686.86367	0.1	2.95E-03	3.1	3.5	7
** (N)Q (9,E, 4,s)	9 E Eo	14 s *	**	1687.06203	5.4	9.95E-04	4.3	-13.0	2
** (N)Q (7,E, 5,s)	7 E Ee	7 s 2-0	2nu2	1687.36777	2.6	4.67E-04	4.4	7.3	2
** (S)R (3,A-, 0,s)	4 A- A2o	3 s 2-1	nu4	1689.84399	0.2	1.32E-02	3.6	-4.5	12
(Q)P (9,A-, 0,s)	8 A- A2o	9 a 2-0	2nu2	1689.89499	0.9	1.59E-03	2.4	-3.7	5
(Q)P (9,E, 1,s)	8 E Ee	17 a 0-1	2nu2	1689.97485	0.7	7.85E-04	0.9	-5.2	3
** (S)R (4,E, 1,a)	5 E Ee	4 s 3-1	nu4	1690.34994	-0.7	5.24E-03	3.4	-5.5	9
(Q)P (9,A-, 3,s)	8 A- A2e	8 a 3-0	2nu2	1690.66452	0.1	1.67E-03	0.9	-0.8	3
(R)R (2,A+, 0,s)	3 A+ A2e	3 s 1-0	nu4	1691.03827	6.7	7.18E-01	3.1	0.9	3
(Q)P (9,E, 4,s)	8 E Ee	16 a 4-0	2nu2	1691.35218	-0.8	8.22E-04	0.7	-3.3	2
(R)R (3,A-, 3,s)	4 A- A2e	1 s 4-1	nu4	1691.73732	-0.2	1.75E+00	0.7	2.2	3
(Q)P (9,E, 5,s)	8 E Ee	16 a 5-0	2nu2	1692.34508	-1.4	8.01E-04	1.6	-5.3	3
(P)R (2,E, 1,s)	3 E Ee	6 s 0-1	nu4	1692.59708	1.1	1.56E-01	2.5	-4.5	6
(R)R (3,A+, 3,a)	4 A+ A2o	2 a 4-1	nu4	1692.80092	1.6	1.53E+00	0.8	1.8	3
** (S)R (5,E, 2,a)	6 E Ee	5 s 4-1	nu4	1693.04412	-0.7	6.71E-03	3.0	-1.1	7
(P)R (2,E, 1,a)	3 E Ee	6 s 0-1	nu4	1693.63612	2.7	1.48E-01	2.0	-4.6	7
** (S)R (4,E, 4,s)	5 E Ee	1 s 4-0	2nu2	1694.57988	-3.8	1.61E-01	2.7	2.7	7
** (S)R (5,E, 2,s)	6 E Ee	5 s 4-1	nu4	1695.37537	0.3	6.45E-03	2.9	-5.0	5
** (S)R (6,A-, 3,a)	7 A- A2o	2 s 5-1	nu4	1695.61272	-1.0	1.27E-02	3.1	-2.4	7
(P)R (2,E, 2,s)	3 E Ee	5 s 1-1	nu4	1696.51367	-0.6	4.26E-02	3.3	-11.7	9
(P)R (2,E, 2,a)	3 E Ee	5 s 1-1	nu4	1697.21486	-0.2	4.04E-02	3.3	-9.9	9
** (O)Q (5,E, 5,s)	5 E Ee	6 s 3-1	nu4	1697.45057	-1.7	1.81E-03	9.4	5.8	2
** (S)R (6,A+, 3,s)	7 A+ A2e	3 s 5-1	nu4	1697.95520	0.6	1.23E-02	3.7	-7.2	8
(R)R (3,E, 2,s)	4 E Ee	4 s 3-1	nu4	1698.03202	-0.6	4.77E-01	1.6	-0.3	4
** (O)Q (9,A-, 3,s)	9 A- A2e	9 s 1-1	nu4	1698.15930	-8.1	1.69E-03	2.3	-14.1	2
(Q)R (4,A-, 3,s)	5 A- A2o	2 s 3-0	2nu2	1698.44364	-4.0	3.00E-01	0.4	0.0	4
(R)R (3,E, 2,a)	4 E Ee	5 s 3-1	nu4	1699.17614	0.2	3.80E-01	0.4	-1.4	4
** (S)R (8,E, 5,s)	9 E Ee	5 s 8-1	nu4	1700.36804	-1.7	4.17E-03	1.5	1.9	3
** (R)R (7,E, 4,s)	8 E Ee	4 s 6-1	nu4	1700.40727	0.9	5.61E-03	3.9	1.5	4
** (O)Q (7,E, 5,s)	7 E Ee	10 s 3-1	nu4	1701.03292	-0.6	2.71E-03	2.6	-3.7	2
(Q)R (4,E, 2,s)	5 E Ee	4 s 2-0	2nu2	1701.39541	-2.8	1.19E-01	0.5	0.2	3
** (S)R (9,A-, 6,a)	10 A- A2e	2 s 8-1	nu4	1702.55014	-2.4	5.31E-03	3.4	-3.9	9

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)	
** (S)R (8,E, 5,s)	9 E Ee	5 a 7-1	nu4	1702.73370	1.9	4.40E-03	3.4	6.3	3
(Q)R (4,E, 1,a)	5 E Eo	5 s 7-0	2nu2	1703.23392	-1.8	1.02E-01	2.1	0.8	8
(R)R (3,E, 1,s)	4 E Ee	6 s 2-1	nu4	1703.38578	-2.6	2.00E-01	3.0	-3.6	7
(Q)R (4,A+, 0,a)	5 A+ A2e	3 s 0-0	2nu2	1703.85861	-1.4	1.96E-01	0.7	2.3	5
** (O)Q (7,E, 5,s)	7 E Ee	9 a 3-1	nu4	1704.08006	-1.5	2.68E-03	2.7	12.5	3
(R)R (3,E, 1,a)	4 E Eo	5 a 2-1	nu4	1704.19576	-1.4	1.34E-01	1.1	-5.1	6
** (S)R (9,A+, 6,s)	10 A+ A2o	3 a 8-1	nu4	1704.93257	2.1	5.21E-03	3.5	-6.6	7
** (Q)R (3,E, 1,a)	4 E Eo	6 s 1-1	nu4	1706.41811	-1.2	4.80E-03	3.3	-13.2	5
(R)R (4,E, 4,a)	5 E Ee	2 a 5-1	nu4	1708.30601	2.3	7.10E-01	1.1	0.8	3
** (S)R (11,E, 8,s)	12 E Eo	5 s 10-1	nu4	1708.94972	1.9	8.97E-04	1.9	-7.0	3
** (Q)R (3,E, 1,s)	4 E Ee	7 a 1-1	nu4	1709.08448	2.3	4.67E-03	2.8	-1.9	8
** (S)R (4,A+, 0,a)	5 A+ A2e	4 s 2-1	nu4	1709.78682	0.3	1.57E-02	1.8	-3.0	10
** (M)Q (9,E, 4,a)	9 E Ee	16 s 0-1	nu4	1711.35888	-2.3	3.29E-04	3.5	-10.4	2
(Q)P (8,E, 2,s)	7 E Ee	15 a 2-0	2nu2	1712.52487	0.6	1.37E-03	0.3	-0.8	3
** (S)R (5,E, 1,a)	6 E Ee	6 s 3-1	nu4	1713.00317	-0.6	5.02E-03	2.7	-2.9	7
(R)R (4,A+, 3,s)	5 A+ A2e	2 s 4-1	nu4	1713.70878	0.1	9.99E-01	0.6	0.2	3
(P)R (3,E, 1,s)	4 E Ee	8 s 0-1	nu4	1714.64040	2.8	1.72E-01	2.7	-5.8	6
** (S)R (5,E, 1,s)	6 E Ee	7 a 3-1	nu4	1715.75169	1.6	5.01E-03	2.8	-5.8	4
** (O)Q (6,A+, 6,a)	6 A- A2e	3 s 4-1	nu4	1715.91430	-1.2	2.63E-03	1.4	-2.9	2
(S)R (6,E, 2,a)	7 E Ee	6 s 4-1	nu4	1716.12067	-1.0	5.32E-03	3.9	-1.1	6
(P)R (3,E, 1,a)	4 E Ee	7 a 0-1	nu4	1716.36200	5.1	1.54E-01	2.5	-4.6	7
(Q)P (8,A-, 6,s)	7 A- A2o	7 a 6-0	2nu2	1716.78100	-0.6	2.09E-03	2.3	-2.5	4
(Q)R (5,E, 4,a)	6 E Ee	3 s 4-0	2nu2	1717.12634	-3.9	1.55E-01	1.1	0.0	2
** (O)Q (7,A-, 6,a)	7 A- A2e	4 s 4-1	nu4	1718.02191	-0.8	3.58E-03	1.4	-14.7	5
(P)R (3,E, 2,s)	4 E Ee	6 s 1-1	nu4	1718.27480	-0.7	7.08E-02	2.1	-10.9	5
(R)R (6,E, 5,s)	7 E Ee	7 a 4-1	nu4	1718.88935	1.7	5.04E-03	3.2	-7.4	6
(Q)P (8,E, 7,s)	7 E Ee	13 a 7-0	2nu2	1719.02006	1.6	7.13E-04	0.7	1.4	2
** (S)R (7,A+, 3,a)	8 A+ A2o	3 s 5-1	nu4	1719.11227	-1.7	8.78E-03	3.0	-5.6	
(P)R (3,E, 2,a)	4 E Ee	7 a 1-1	nu4	1719.43694	1.9	6.47E-02	3.4	-9.8	7
(R)R (4,E, 2,s)	5 E Eo	6 s 3-1	nu4	1719.70957	-1.1	2.69E-01	1.7	-1.1	4
** (O)Q (8,A+, 6,a)	8 A- A2e	5 s 4-1	nu4	1720.11690	-1.1	1.35E-03	3.0	-12.7	5
(Q)R (4,E, 2,a)	5 E Ee	6 s 3-1	nu4	1721.15077	-1.1	1.84E-01	1.9	-3.0	7
(Q)R (5,A+, 3,a)	6 A+ A2o	2 s 3-0	2nu2	1721.29751	-2.2	2.32E-01	2.7	1.2	7
(P)R (3,A-, 3,s)	4 A- A2e	2 s 2-1	nu4	1721.63497	0.0	4.32E-02	3.7	-14.6	12
(R)R (5,E, 5,s)	6 E Ee	2 s 5-1	nu4	1721.74507	0.0	7.63E-01	1.9	2.0	4
** (S)R (7,A-, 3,s)	8 A- A2e	4 a 5-1	nu4	1721.89313	2.0	8.80E-03	2.6	-5.4	6
** (S)R (8,E, 4,a)	9 E Ee	6 s 6-1	nu4	1721.97336	-2.8	3.78E-03	3.9	8.0	4
** (O)Q (9,A-, 6,a)	9 A- A2e	6 s 4-1	nu4	1722.14282	1.4	2.78E-03	3.4	5.2	2
** (O)Q (7,A+, 6,s)	7 A+ A2o	4 a 4-1	nu4	1722.19160	-1.1	2.76E-03	3.1	-1.8	4
(P)R (3,A+, 3,a)	4 A+ A2o	3 a 2-1	nu4	1722.42361	-0.2	4.08E-02	3.1	-10.7	11
(R)R (5,E, 5,a)	6 E Eo	3 s 2-1	nu4	1723.82701	2.7	5.07E-01	1.6	0.7	4
(R)R (4,E, 1,s)	5 E Ee	7 s 2-1	nu4	1724.57913	-3.8	9.75E-02	2.3	-5.1	8
** (S)R (9,E, 6,s)	10 E Eo	6 s 7-1	nu4	1724.70640	-2.9	2.17E-03	2.4	-7.2	5
** (O)R (3,E, 2,a)	4 E Ee	8 s 0-1	nu4	1724.99192	1.4	1.48E-03	2.3	-1.9	2
(Q)R (4,E, 1,a)	5 E Eo	7 a 2-1	nu4	1725.37115	-1.9	5.65E-02	3.0	-3.8	7
(S)R (5,E, 1,a)	6 E Eo	7 s 1-0	2nu2	1726.38819	0.8	7.01E-02	2.5	-0.7	6
** (S)R (10,A+, 6,a)	11 A+ A2e	3 s 8-1	nu4	1727.30830	-3.0	2.76E-03	3.8	-2.3	7
** (S)R (9,E, 5,s)	10 E Ee	7 a 7-1	nu4	1727.51256	2.5	2.34E-03	3.2	1.0	4
** (N)Q (8,E, 7,s)	8 E Ee	6 s 4-0	2nu2	1727.82691	0.5	4.61E-04	2.2	7.6	2
** (O)R (3,E, 2,s)	4 E Ee	7 a 0-1	nu4	1728.21837	5.3	1.04E-03	4.0	-0.8	2
** (Q)R (4,E, 1,a)	5 E Eo	8 s 1-1	nu4	1728.81283	-1.0	4.91E-03	4.0	-6.0	7
** (Q)R (6,A+, 4,s)	7 A+ A2e	1 s 6-0	2nu2	1729.03147	-3.1	4.37E-01	1.2	4.0	4
(R)R (5,E, 4,s)	6 E Ee	4 s 5-1	nu4	1729.23406	0.7	4.47E-01	0.9	0.3	4
** (S)R (10,A-, 6,s)	11 A- A2o	4 a 8-1	nu4	1730.13025	3.1	2.84E-03	2.1	1.0	2
(R)R (5,E, 4,a)	6 E Ee	4 a 5-1	nu4	1731.69362	1.0	3.06E-01	1.9	-0.6	4
** (S)R (11,E, 7,s)	12 E Ee	6 a 9-1	nu4	1732.62042	2.3	7.04E-04	4.6	-10.5	2
** (S)R (5,E, 1,s)	6 E Ee	8 a 3-1	nu4	1732.70001	-1.8	2.37E-04	3.1	13.2	2
(Q)P (7,E, 1,s)	6 E Ee	13 a 1-0	2nu2	1734.41966	0.8	2.36E-03	5.1	12.2	2
(Q)P (7,E, 2,s)	6 E Eo	13 a 2-0	2nu2	1734.79362	0.2	1.97E-03	3.3	-3.2	2
(Q)R (6,E, 5,a)	7 E Eo	4 s 5-0	2nu2	1734.95311	4.4	1.50E-01	1.0	-2.8	3
(Q)P (7,A-, 3,s)	6 A- A2o	3 s 4-1	nu4	1735.44984	0.0	4.00E-03	3.4	2.2	8
(S)R (5,A-, 0,s)	6 A+ A2e	4 a 2-1	nu4	1735.80875	-0.2	5.18E-01	2.1	0.2	4
(R)R (6,A-, 6,s)	7 A- A2o	1 s 7-1	nu4	1735.89392	2.1	1.27E-02	3.6	-5.0	6
(P)R (4,E, 1,s)	5 E Ee	9 s 0-1	nu4	1736.50554	-0.3	1.22E+00	1.0	2.0	3
(Q)P (7,E, 5,s)	6 E Ee	12 a 5-0	2nu2	1737.83826	4.2	1.51E-01	2.5	-2.1	7
(R)R (5,A+, 3,a)	6 A+ A2o	3 a 4-1	nu4	1738.06710	-0.4	1.36E-03	0.6	-11.0	2
(R)R (4,A+, 0,a)	5 A+ A2e	5 a 1-1	nu4	1738.84444	7.5	3.19E-01	1.1	-2.0	4
** (S)R (6,E, 1,s)	7 E Ee	8 a 3-1	nu4	1739.50105	3.3	3.69E-03	3.3	-9.9	2
** (S)R (7,E, 2,a)	8 E Ee	9 a 0-1	nu4	1739.66546	-1.0	3.52E-03	2.4	-4.3	2
(Q)R (5,E, 4,a)	6 E Ee	9 a 0-1	nu4	1740.01132	5.9	1.17E-01	0.8	-6.1	2
(Q)R (6,E, 4,a)	7 E Ee	4 s 4-0	2nu2	1740.30407	-1.7	1.05E-01	1.4	-1.1	4
(P)R (4,E, 2,s)	5 E Eo	8 s 1-1	nu4	1740.59538	-0.6	7.40E-02	2.2	-10.7	5
(R)R (5,E, 2,s)	6 E Eo	8 s 3-1	nu4	1741.41915	-1.7	1.29E-01	2.1	-4.1	7
(P)R (4,A-, 2,s)	5 E Ee	8 a 1-1	nu4	1742.43349	3.4	6.61E-02	3.2	-6.2	9
(P)R (4,A+, 3,s)	5 A+ A2e	4 s 2-1	nu4	1743.75009	0.8	6.88E-02	3.9	-12.0	5
(Q)R (6,A-, 3,a)	7 A- A2o	3 s 3-0	2nu2	1744.75288	0.5	1.45E-01	1.7	-0.9	4
(P)R (4,A-, 3,a)	5 A- A2o	4 a 2-1	nu4	1744.95101	1.7	6.14E-02	3.9	-8.8	9
(Q)R (7,E, 7,a)	8 E Ee	1 s 7-0	2nu2	1745.06533	-0.7	2.05E-01	2.2	1.7	7
(R)R (5,E, 1,s)	6 E Ee	9 s 1-1	nu4	1745.70378	-4.3	3.98E-02	3.6	-9.7	8
(P)R (4,E, 4,s)	5 E Ee	9 a 3-1	nu4	1746.60392	0.0	1.15E-02	3.5	-12.3	9
(P)R (4,E, 4,s)	5 E Ee	5 a 3-1	nu4	1747.41081	-0.1	1.03E-02	3.8	-10.7	9
(R)R (6,E, 5,a)	7 E Ee	5 a 6-1	nu4	1748.08628	0.6	2.02E-01	1.7	-4.5	3
(Q)R (6,E, 2,a)	7 E Ee	7 s 2-0	2nu2	1748.10306	2.6	5.22E-02	1.7	-1.0	3
(Q)R (6,E, 1,a)	7 E Eo	9 s 1-0	2nu2	1750.15397	1.9	3.92E-02	3.6	-1.9	10



(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
(Q)R (6,A+, 0,a) 7 A+ A2e 5 s 0 0 2nu2 1750.89639 4.1 6.99E-02 1.8 -6.5 2								
** (S)R (6,E, 1,a) 7 E Ee 10 s 3 1 nu4 1751.50177 -1.0 2.12E-03 0.4 -3.9 2								
(R)R (6,E, 4,a) 7 E Ee 6 s 5 1 nu4 1751.74322 0.6 2.02E-01 2.2 -3.7 3								
(Q)R (7,A+, 6,a) 8 A+ A2e 2 s 6 0 nu2 1751.93841 -2.1 2.78E-01 2.8 1.2 5								
** (S)R (6,E, 1,a) 8 E Ee 2 s 8 1 nu4 1754.46941 -0.9 2.93E-04 4.1 11.0 2								
(R)R (6,E, 4,a) 8 E Ee 5 s 5 1 nu4 1754.98094 1.5 2.39E-01 2.5 -1.2 7								
(R)R (6,E, 4,a) 7 E Ee 5 s 5 1 nu4 1755.11088 -0.4 1.14E-01 1.7 -2.8 7								
** (S)R (11,A+, 6,a) 12 A+ A2e 5 s 8 1 nu4 1755.83377 2.0 1.09E-03 4.4 -11.4 2								
** (Q)R (5,E, 1,s) 6 E Ee 10 a 1-1 nu4 1755.90227 3.7 4.42E-03 2.4 12.8 2								
(Q)P (6,E, 1,s) 5 E Ee 11 a 1 0 2nu2 1756.50977 0.2 2.79E-03 3.1 2.4 4								
(Q)P (6,E, 2,s) 5 E Ee 11 a 2 0 2nu2 1756.93926 -0.5 2.74E-03 2.5 4.8 3								
(Q)P (6,A+, 3,s) 5 A+ A2e 6 a 3 0 2nu2 1757.69085 -0.2 4.87E-03 3.7 2.4 10								
(R)R (6,A+, 3,s) 7 A+ A2e 4 a 4 1 nu4 1757.92654 -0.6 2.33E-01 1.4 -1.4 6								
(Q)R (7,E, 5,a) 8 E Ee 5 s 5 0 2nu2 1758.37054 -1.4 9.08E-02 2.1 0.6 8								
(Q)P (6,E, 4,s) 5 E Ee 10 a 4 0 2nu2 1758.81617 0.8 1.96E-03 0.7 -0.3 3								
(R)R (5,A+, 0,s) 6 A+ A2e 5 s 1 1 nu4 1759.50664 6.1 2.60E-01 1.2 -4.0 4								
(R)R (7,A+, 6,s) 8 A+ A2e 2 s 7 1 nu4 1759.81477 1.3 5.24E-01 1.8 1.5 4								
(Q)R (8,E, 9,a) 9 E Ee 2 s 8 0 2nu2 1760.45558 3.2 1.70E-01 1.8 2.1 7								
(R)R (6,A+, 3,a) 7 A+ A2e 4 a 4 1 nu4 1760.67203 -1.3 1.21E-01 2.1 -2.6 8								
(P)R (5,E, 1,s) 6 E Ee 11 s 0 1 nu4 1760.81204 4.2 9.70E-02 2.4 -7.4 8								
(R)R (6,E, 2,s) 7 E Ee 10 s 3 1 nu4 1763.09265 0.0 5.39E-02 3.3 -6.0 8								
** (S)R (8,E, 2,a) 9 E Ee 10 a 4-1 nu4 1763.67586 -0.7 2.05E-03 2.7 -5.6 4								
** (S)R (7,E, 1,s) 8 E Ee 10 a 3-1 nu4 1763.94291 0.7 2.41E-03 3.5 -9.8 6								
(Q)R (7,E, 4,a) 8 E Ee 6 s 4 0 2nu2 1764.04450 0.2 5.89E-02 2.9 -0.6 9								
(P)R (5,E, 1,a) 6 E Ee 11 a 0 1 nu4 1764.51130 3.9 7.25E-02 2.2 -3.2 7								
(R)R (7,A+, 6,a) 8 A+ A2e 3 a 7 1 nu4 1764.56396 -0.4 2.48E-01 2.1 -2.6 7								
(R)R (6,E, 2,a) 7 E Ee 12 a 1-1 nu4 1764.81549 -1.4 2.59E-02 2.6 -5.9 10								
(R)R (8,E, 8,s) 9 E Ee 2 s 9 1 nu4 1765.50445 -1.8 3.07E-01 1.2 2.3 4								
(R)R (6,E, 1,s) 7 E Ee 10 s 2 1 nu4 1766.74470 -3.2 1.55E-02 2.1 -6.1 8								
(R)R (6,E, 1,a) 7 E Ee 11 s 2 1 nu4 1767.39561 0.8 5.94E-03 3.1 -5.4 9								
** (S)R (9,A+, 3,a) 10 A+ A2e 5 s 5-1 nu4 1767.42157 -1.4 2.72E-03 1.5 -7.8 4								
(R)R (7,E, 5,s) 8 E Ee 5 s 6 1 nu4 1767.51806 1.1 1.48E-01 2.2 -2.5 7								
(P)R (5,A+, 3,a) 6 A+ A2e 4 a 2-1 nu4 1768.30907 2.1 5.88E-02 0.5 -4.9 2								
(Q)R (7,A+, 3,a) 8 A+ A2e 4 a 3 0 2nu2 1768.76769 1.9 7.85E-02 2.5 -0.9 9								
(P)R (5,E, 4,s) 6 E Ee 6 s 3-1 nu4 1768.98117 0.1 1.60E-02 1.7 -14.2 10								
(P)R (5,E, 4,a) 6 E Ee 7 a 3-1 nu4 1770.31148 1.4 1.43E-02 3.4 -9.7 10								
(R)R (8,E, 8,s) 9 E Ee 12 a 1-1 nu4 1770.49798 -1.7 1.38E-01 4.4 -1.3 2								
** (Q)R (5,E, 2,s) 6 E Ee 11 s 4 1 nu4 1771.16249 3.0 2.33E-03 5.3 15.6 2								
(P)R (5,E, 5,s) 6 E Ee 5 s 4-1 nu4 1771.39226 -0.2 5.76E-03 4.0 -12.8 5								
** (S)R (9,A+, 3,s) 10 A+ A2e 5 s 5-1 nu4 1771.58645 0.2 2.55E-03 3.2 -10.7 6								
(P)R (5,E, 5,a) 6 E Ee 5 s 4-1 nu4 1772.22445 -0.4 5.32E-03 4.0 -5.9 5								
(R)R (7,E, 5,a) 8 E Ee 6 a 6 1 nu4 1772.33123 -0.5 6.57E-02 2.9 -4.0 6								
(Q)R (7,E, 2,a) 8 E Ee 9 s 2 0 2nu2 1772.34960 3.0 2.84E-02 2.6 3.1 5								
(R)R (7,E, 4,s) 8 E Ee 7 s 5 1 nu4 1774.24218 0.3 8.61E-02 3.4 -1.7 8								
(Q)R (7,E, 1,a) 8 E Ee 11 s 1 0 2nu2 1774.71223 6.7 2.00E-02 4.0 -5.2 10								
(R)R (8,E, 7,s) 9 E Ee 4 s 8 1 nu4 1774.85859 1.2 1.71E-01 2.8 -0.4 7								
(R)R (9,A+, 9,a) 10 A+ A2e 1 a 10 1 nu4 1775.26764 8.4 2.42E-01 2.1 -3.0 4								
** (Q)R (6,E, 1,a) 8 E Ee 11 s 3 1 nu4 1775.45949 -1.7 2.74E-03 3.2 -3.0 4								
** (S)R (7,E, 1,s) 8 E Ee 11 s 3 1 nu4 1776.12804 1.0 2.65E-04 6.7 2.7 2								
** (Q)R (5,E, 2,s) 6 E Ee 11 s 0 1 nu4 1776.20418 4.0 1.37E-03 3.3 -3.9 2								
** (S)R (12,A+, 6,a) 13 A+ A2e 5 s 8-1 nu4 1777.82756 1.2 4.42E-04 4.1 -6.3 2								
(Q)P (5,A+, 0,s) 4 A+ A2e 5 a 0 0 2nu2 1778.24041 -0.5 6.47E-03 2.7 1.5 9								
(Q)P (5,E, 1,s) 4 E Ee 9 a 1 0 2nu2 1778.39682 -0.4 3.21E-03 3.7 3.1 6								
** (S)R (11,E, 5,s) 12 E Ee 11 a 7-1 nu4 1778.69890 2.4 4.08E-04 9.8 -12.3 2								
(Q)P (5,E, 2,s) 4 E Ee 9 a 2 0 2nu2 1778.87630 -0.4 2.91E-03 3.2 2.2 7								
(R)R (9,A+, 9,s) 10 A+ A2e 1 s 10 1 nu4 1779.72920 -2.8 3.91E-01 1.0 3.4 4								
(R)R (7,A+, 3,s) 8 A+ A2e 5 a 4 1 nu4 1779.96596 -0.8 9.26E-02 1.9 -3.3 8								
** (Q)R (6,E, 1,s) 7 E Ee 11 a 1-1 nu4 1780.53494 -0.2 2.11E-03 0.4 -1.3 2								
** (Q)R (5,A+, 6,a) 6 A+ A2e 5 a 1 1 nu4 1781.56247 -6.2 3.90E-03 2.8 -5.8 7								
(Q)R (8,E, 5,s) 9 E Ee 7 s 5 0 2nu2 1782.28788 -0.8 4.22E-02 3.5 -3.2 8								
(R)R (8,A+, 6,s) 9 A+ A2e 3 s 7 1 nu4 1783.13160 1.3 1.95E-01 1.7 -1.8 7								
(R)R (7,A+, 3,a) 8 A+ A2e 5 a 4 1 nu4 1783.22311 1.1 3.56E-02 3.6 -2.9 9								
(R)R (9,E, 8,a) 10 E Ee 4 a 9 1 nu4 1783.78285 1.6 7.26E-02 1.7 0.6 9								
** (S)R (8,E, 1,a) 9 E Ee 11 s 3-1 nu4 1783.93496 0.1 1.61E-03 4.5 4.3 2								
(Q)R (9,A+, 9,a) 10 A+ A2e 2 s 9 0 2nu2 1785.82062 -0.7 1.43E-01 1.8 -0.4 7								
** (P)R (7,E, 2,s) 8 E Ee 11 s 1 0 2nu2 1786.18773 6.8 1.78E-03 2.5 2.2 3								
(R)R (7,E, 2,a) 8 E Ee 11 a 3 1 nu4 1786.46472 0.8 7.37E-03 1.3 -2.2 3								
(P)R (6,E, 2,s) 7 E Ee 12 s 1-1 nu4 1787.05034 -1.3 3.74E-02 3.1 -9.4 7								
(R)R (7,E, 1,s) 8 E Ee 12 s 2 1 nu4 1787.71346 -0.6 5.14E-03 1.6 -7.2 4								
(Q)R (8,E, 4,a) 9 E Ee 8 s 4 0 2nu2 1788.20153 0.1 2.70E-02 3.9 -4.2 10								
(R)R (7,E, 2,a) 8 E Ee 12 a 2 1 nu4 1788.31465 3.6 1.47E-03 1.2 4.6 2								
** (S)R (8,E, 1,s) 9 E Ee 12 a 3-1 nu4 1789.06472 -1.0 1.65E-03 1.0 9.0 2								
(R)R (6,A+, 0,a) 7 A+ A2e 7 a 1 1 nu4 1789.32857 -0.6 7.89E-02 3.2 -2.0 9								
(P)R (6,A+, 3,s) 7 A+ A2e 6 s 2-1 nu4 1789.49646 3.9 4.66E-02 3.5 -11.2 8								
(R)R (10,E, 10,a) 11 E Ee 1 a 11 1 nu4 1789.62879 14.8 7.54E-02 3.6 1.3 9								
(R)R (8,A+, 6,a) 9 A+ A2e 3 a 7 1 nu4 1789.65441 -1.4 6.93E-02 2.8 -1.2 9								
(R)R (9,E, 8,s) 10 E Ee 3 s 9 1 nu4 1789.72970 1.0 1.04E-01 2.2 -1.0 8								
(R)R (6,E, 1,a) 7 E Ee 13 a 0 1 nu4 1789.75076 -0.5 3.63E-02 2.5 -1.5 8								
(R)R (8,E, 5,s) 9 E Ee 7 s 6 1 nu4 1790.38437 0.8 5.59E-02 3.3 -2.8 9								
(P)R (6,E, 2,a) 7 E Ee 11 a 1-1 nu4 1790.88161 -0.1 2.67E-02 2.7 -9.3 6								
(P)R (6,E, 4,s) 7 E Ee 8 s 3-1 nu4 1791.80670 0.1 3.39E-02 2.9 -13.2 11								
** (Q)R (5,A+, 3,a) 6 A+ A2e 5 s 1 1 nu4 1791.92152 5.8 2.19E-03 0.4 -5.9 2								
(R)R (9,E, 7,a) 10 E Ee 4 a 8 1 nu4 1792.01759 -1.3 4.51E-02 2.9 0.6 7								
** (S)R (10,A-, 7,a) 11 A- A2e 6 s 5-1 nu4 1792.18570 -0.6 1.34E-03 2.0 -1.1 2								
(Q)R (8,A-, 3,a) 9 A- A2e 5 s 3 0 2nu2 1793.17283 0.9 3.53E-02 4.0 -4.1 9								

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
(R)R (10,E, 10,s) 11 E Eo 2 s 11 1 nu4 1793.76199 -3.5 1.14E-01 2.0 2.2 8								
(P)R (6,E, 4,a) 7 E Ee 8 a 3-1 nu4 1793.84057 1.6 1.20E-02 3.7 -6.2 12								
(P)R (6,E, 5,s) 7 E Ee 6 s 4-1 nu4 1794.03032 -0.2 7.56E-03 2.6 -10.5 6								
(P)R (6,E, 5,a) 7 E Ee 7 a 4-1 nu4 1795.40974 1.4 6.47E-03 2.0 -8.4 8								
(P)R (6,A-, 6,s) 7 A- A2e 2 s 5-1 nu4 1796.01695 0.1 5.88E-03 1.2 -5.8 3								
(R)R (8,E, 4,s) 9 E Eo 9 s 5 1 nu4 1796.63850 0.5 3.14E-02 2.6 -3.2 6								
(P)R (6,A+, 6,a) 7 A+ A2e 3 a 5-1 nu4 1796.86348 0.5 5.18E-03 2.6 -2.2 3								
(Q)R (8,E, 2,a) 9 E Ee 11 s 2 0 2nu2 1797.05615 -0.3 1.19E-02 2.1 -4.2 9								
(Q)R (9,E, 8,a) 10 E Ee 5 s 8 0 2nu2 1797.32946 -3.3 3.33E-02 3.5 -4.4 7								
** (R)R (8,E, 1,s) 9 E Ee 13 s * * * 1797.79985 2.4 2.18E-04 7.7 1.8 2								
(R)R (9,E, 7,s) 10 E Ee 6 s 8 1 nu4 1798.57945 1.3 5.90E-02 3.1 -1.3 5								
(R)R (10,A-, 9,a) 11 A- A2e 2 a 10 1 nu4 1798.90457 3.8 8.94E-02 1.4 2.3 4								
(Q)P (4,E, 1,s) 3 E Ee 7 a 1 0 2nu2 1800.00238 -0.7 3.14E-03 3.2 4.1 7								
(Q)P (6,A+, 0,a) 9 A+ A2e 7 s 0 0 2nu2 1800.50735 1.6 1.40E-02 3.4 1.0 7								
** (Q)R (6,A-, 3,a) 7 A- A2e 6 s 1 1 nu4 1800.72441 -5.4 6.49E-03 3.9 2.0 9								
(Q)R (10,E, 10,a) 11 E Ee 2 s 10 0 2nu2 1800.84591 -1.1 3.57E-02 2.3 -3.0 3								
(Q)P (4,A-, 3,s) 3 A+ A2e 4 a 3 0 2nu2 1801.43201 1.2 3.49E-03 0.2 8.9 2								
(R)R (8,A+, 3,s) 9 A+ A2e 6 s 4 1 nu4 1801.85707 1.2 3.21E-02 3.6 -5.5 8								
** (R)R (8,E, 4,a) 9 E Ee 9 s * * * 1801.97029 0.8 8.57E-03 3.2 -2.1 9								
(R)R (11,E, 11,a) 12 E Eo 2 a 12 1 nu4 1803.61044 22.9 4.26E-02 3.8 0.5 8								
** (S)R (8,A+, 0,s) 9 A+ A2e 8 s 2-1 nu4 1804.38444 7.4 6.44E-03 2.7 -8.2 8								
(R)R (10,A+, 9,s) 11 A+ A2e 2 s 10 1 nu4 1804.42200 1.0 1.21E-01 0.5 -9.7 4								
** (R)R (8,A-, 3,s) 9 A- A2e 6 s * * * 1805.74411 -0.4 7.55E-02 3.2 -2.8 8								
(R)R (8,E, 2,a) 9 E Ee 12 s 3 1 nu4 1806.35799 0.9 6.73E-02 2.4 -1.4 5								
(R)R (9,A+, 6,a) 10 A+ A2e 4 s 7 1 nu4 1806.35799 0.9 6.73E-02 2.4 -1.4 5								
(R)R (9,E, 5,a) 10 E Eo 9 a 6 1 nu4 1806.47484 -1.4 1.76E-02 2.3 -1.3 3								
(Q)R (9,E, 7,a) 10 E Ee 5 s 7 0 2nu2 1806.92025 -1.9 1.62E-02 3.8 -3.1 8								
(R)R (11,E, 11,s) 12 E Ee 2 a 12 1 nu4 1807.59593 -3.8 6.13E-02 3.1 0.9 6								
(R)R (10,E, 8,a) 11 E Ee 5 a 9 1 nu4 1807.90925 -2.0 2.62E-02 2.6 -0.6 8								
** (R)R (8,E, 2,a) 9 E Ee 13 s * * * 1808.12143 2.5 1.18E-03 4.3 -9.1 2								
** (S)R (9,E, 1,a) 10 E Ee 13 s 3-1 nu4 1808.49915 1.5 7.45E-04 3.7 -6.2 2								
(R)R (8,E, 1,s) 9 E Ee 14 s 2 1 nu4 1808.63936 3.1 1.69E-03 2.3 3.4 2								
(R)R (7,A+, 0,a) 8 A+ A2e 7 s 1 1 nu4 1808.63936 3.1 1.69E-03 2.3 3.4 2								
(P)R (7,E, 1,s) 8 E Ee 14 s 0 1 nu4 1809.49232 0.3 2.49E-02 3.6 -8.6 9								
(P)R (7,E, 2,s) 8 E Eo 13 s 1-1 nu4 1811.17766 -2.2 1.96E-02 2.7 -6.9 4								
(R)R (9,E, 4,a) 10 E Eo 10 s 5 1 nu4 1812.49885 -1.5 1.11E-02 3.5 -1.8 8								
(P)R (7,A-, 3,s) 8 A- A2e 6 s 2-1 nu4 1812.68400 2.9 2.36E-02 3.6 -9.5 7								
(R)R (9,E, 5,s) 10 E Ee 9 s 6 1 nu4 1813.11413 0.9 1.90E-02 3.3 -1.9 8								
(Q)R (10,A-, 9,a) 11 A- A2e 3 s 9 0 2nu2 1813.34918 -4.4 3.31E-02 3.3 -3.6 8								
(R)R (11,E, 10,a) 12 E Ee 1 a 11 1 nu4 1813.61863 5.8 2.47E-02 3.0 8								
(R)R (10,E, 8,s) 11 E Ee 5 s 9 1 nu4 1813.61863 5.8 2.47E-02 3.0 8								
(Q)R (9,A-, 6,a) 10 A- A2e 4 s 6 0 2nu2 1814.81843 -0.1 1.54E-02 2.7 -1.7 7								
(P)R (7,E, 4,s) 8 E Eo 9 s 3-1 nu4 1815.08809 0.8 9.01E-03 3.6 -9.8 8								
(Q)R (11,E, 11,a) 12 E Eo 3 s 11 0 2nu2 1815.50989 -1.4 1.81E-02 3.2 -2.0 8								
(P)R (7,E, 1,a) 8 E Eo 15 a 0 1 nu4 1815.62595 -5.1 1.51E-02 3.9 0.3 8								
(P)R (7,E, 2,a) 8 E Ee 13 a 1-1 nu4 1816.25354 -3.9 1.34E-02 3.1 0.3 5								
(R)R (10,E, 7,a) 11 E Eo 6 a 8 1 nu4 1816.27204 -3.5 1.63E-02 3.9 1.0 5								
(P)R (7,A+, 3,s) 8 A+ A2e 6 a 2-1 nu4 1817.12339 -2.1 2.12E-02 2.3 0.6 7								
(R)R (12,A+, 12,a) 13 A+ A2e 1 a 13 1 nu4 1817.25258 32.5 4.50E-02 3.8 1.9 8								
(R)R (9,A-, 3,s) 10 A- A2e 8 a 3-1 nu4 1817.65297 -4.3 3.7E-02 2.5 2.6 6								
(P)R (7,E, 4,a) 8 E Ee 10 a 3-1 nu4 1818.02506 0.4 7.28E-03 2.9 -2.8 7								
(R)R (9,E, 4,s) 10 E Eo 11 s 5 1 nu4 1818.85993 1.5 1.04E-02 2.9 -2.7 4								
(P)R (7,A+, 6,s) 8 A+ A2e 3 s 5-1 nu4 1818.87765 -1.1 6.29E-03 2.4 -13.6 5								
(R)R (11,E, 10,s) 12 E Eo 4 s 11 1 nu4 1818.92900 1.1 3.18E-02 3.2 -0.2 8								
(P)R (7,E, 5,a) 8 E Eo 8 a 4-1 nu4 1819.17369 1.8 5.02E-03 3.5 -1.4 6								
(P)R (7,A-, 6,a) 8 A- A2e 4 a 5-1 nu4 1820.29169 1.4 5.49E-03 3.4 -7.1 6								
(R)R (12,A-, 12,s) 13 A- A2e 1 s 13 1 nu4 1821.22481 -3.0 6.34E-02 4.0 1.9 6								
(Q)P (3,E, 1,s) 2 E Ee 5 a 1 0 2nu2 1821.25658 -0.5 2.55E-02 2.9 7.2 3								
(Q)P (3,E, 2,s) 2 E Eo 5 a 2 0 2nu2 1821.81458 0.9 1.48E-03 2.2 -4.5 2								
(R)R (10,E, 7,s) 11 E Ee 7 s 10 1 nu4 1822.16171 0.6 1.84E-02 3.0 -1.1 9								
** (Q)R (7,A-, 3,s) 8 A- A2e 7 a 1 1 nu4 1822.61541 -6.3 5.02E-03 3.7 -9.2 7								
(R)R (11,A-, 9,a) 12 A- A2e 2 a 10 1 nu4 1823.35251 -3.3 2.88E-02 2.8 2.7 7								
(R)R (9,A-, 3,s) 10 A- A2e 7 s 4 1 nu4 1823.55685 0.6 1.08E-02 3.2 0.0 8								
** (S)R (11,A-, 3,s) 12 A- A2e 7 a 5-1 nu4 1823.66816 1.0 5.05E-04 2.4 -0.2 2								
** (R)R (10,A-, 6,a) 11 A+ A2e 4 a 7 1 nu4 1823.85522 -2.4 2.02E-02 2.0 1.8 8								
(Q)R (10,E, 8,a) 11 E Ee 6 s 8 0 2nu2 1823.95977 -1.0 7.52E-03 3.5 -1.8 8								
** (Q)R (8,E, 1,a) 9 E Ee 16 s 1-1 nu4 1824.49078 -2.8 9.60E-04 2.0 -3.0 2								
(Q)R (9,E, 1,a) 10 E Eo 15 s 1 0 2nu2 1825.02176 -3.5 2.55E-02 2.9 7.2 3								
(R)R (9,E, 2,s) 10 E Ee 11 s 3 1 nu4 1827.07299 2.3 2.09E-03 3.6 0.4 8								
(R)R (12,E, 11,s) 13 E Eo 4 a 12 1 nu4 1827.97536 7.6 1.26E-02 2.0 4.5 8								
(R)R (11,E, 9,s) 12 A- A2e 3 s 10 1 nu4 1828.95649 0.9 3.23E-02 3.0 -5.7 2								
(Q)R (11,E, 10,a) 12 E Ee 4 s 10 0 2nu2 1829.00031 -4.6 7.91E-03 0.8 -4.0 2								
(R)R (10,A-, 6,s) 11 A- A2e 5 s 7 1 nu4 1829.40771 0.7 2.06E-02 3.1 -1.6 7								
(Q)R (12,A+, 12,a) 13 A+ A2e 2 s 12 0 2nu2 1829.78354 -1.0 1.82E-02 3.5 0.4 8								
(R)R (13,E, 13,a) 14 E Eo 1 a 14 1 nu4 1830.57502 43.5 1.11E-02 2.1 4.3 7								
(R)R (10,E, 5,a) 11 E Ee 11 a 6 1 nu4 1830.60690 -0.9 6.28E-03 3.6 2.4 8								
(R)R (11,E, 8,a) 12 E Ee 7 a 9 1 nu4 1832.40303 -5.0 8.48E-03 3.8 2.1 8								
(Q)R (10,E, 7,a) 11 E Ee 10 s 1 0 2nu2 1832.90748 -3.7 3.36E-03 3.8 0.8 4								
(R)R (12,E, 11,s) 13 E Eo 3 s 12 0 2nu2 1834.24504 2.3 1.56E-02 2.0 -1.3 5								
(P)R (8,E, 2,s) 9 E Ee 16 s 0 1 nu4 1834.57825 -2.4 1.02E-02 3.4 -5.4 7								
(R)R (13,E, 13,a) 14 E Ee 2 s 14 1 nu4 1834.64235 -0.3 1.59E-02 2.3 6.1 6								
(R)R (10,E, 5,s) 11 E Ee 11 s 6 1 nu4 1835.63605 1.3 5.84E-03 4.0 0.6 9								
(P)R (8,E, 2,s) 9 E Ee 16 s 1-1 nu4 1835.84215 -2.7 8.64E-03 4.0 -2.0 9								
(R)R (10,E, 4,a) 11 E Ee 12 a 5 1 nu4 1836.51121 -0.4 3.93E-03 3.7 4.2 4								
** (S)R (9,A-, 0,s) 10 A+ A2e 8 a 2-1 nu4 1836.89086 0.3 1.39E-03 2.7 -11.2 4								



(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)	
(P)R (8,A+, 3,s)	9 A+ A2e	8 s 2-1	nu4	1837.45000	7.6	1.20E-02	3.2	-4.3	9
(R)R (11,E, 8,s)	12 E E	7 s 9-1	nu4	1837.79212	0.3	9.56E-03	3.9	2.3	9
(R)R (12,E, 10,s)	13 E E	4 s 11-1	nu4	1838.42077	-5.5	7.04E-03	3.6	3.0	10
(P)R (8,E, 4,s)	9 E E	11 s 3-1	nu4	1838.81259	1.7	4.71E-03	0.5	-2.9	2
(Q)R (10,A+, 6,s)	11 A+ A2e	5 s 6-0	2nu2	1840.23097	1.6	2.62E-03	1.0	4.2	2
(P)R (8,E, 5,s)	9 E E	10 s 4-1	nu4	1840.52819	0.2	3.45E-03	3.2	-2.8	3
(R)R (11,E, 7,s)	12 E E	8 s 8-1	nu4	1840.61475	-2.0	5.02E-03	3.9	1.2	8
(Q)R (11,A+, 9,s)	12 A+ A2o	3 s 9-0	2nu2	1840.64622	6.3	6.73E-03	3.8	-2.0	4
** (S)R (10,E, 1,s)	11 E E	16 s 3-1	nu4	1840.77319	-13.0	2.66E-04	3.1	-6.0	2
(R)R (10,E, 4,s)	11 E E	13 s 5-1	nu4	1840.85821	2.1	3.09E-03	3.6	-0.1	10
** (Q)R (7,A+, 3,s)	8 A+ A2o	7 s 1-1	nu4	1841.00316	1.1	1.87E-03	1.4	6.0	3
(R)R (10,A-, 3,s)	11 A- A2o	7 s 4-1	nu4	1841.56464	1.8	4.63E-03	3.7	2.9	7
(P)R (8,E, 1,s)	9 E E	17 s 0-1	nu4	1842.05009	-7.8	5.45E-03	3.3	6.4	6
(P)R (8,E, 2,s)	9 E E	15 s 1-1	nu4	1842.27618	-5.3	5.45E-03	2.2	7.7	8
** (Q)R (6,E, 5,s)	7 E E	9 s 3-1	nu4	1842.72458	-1.2	3.25E-04	3.9	11.0	2
(P)R (8,E, 4,s)	9 E E	12 s 3-1	nu4	1842.85243	-1.5	3.33E-03	3.9	1.8	7
(Q)R (13,E, 13,s)	14 E E	2 s 11-0	2nu2	1843.66022	-0.3	4.35E-03	3.3	1.0	5
(R)R (12,E, 10,s)	13 E E	6 s 11-1	nu4	1843.87514	1.8	8.08E-03	3.1	-1.4	8
(Q)R (12,E, 11,s)	13 E E	5 s 11-0	2nu2	1844.23503	-4.1	3.62E-03	3.8	-6.4	2
(P)R (8,A+, 6,s)	9 A+ A2e	4 s 5-1	nu4	1844.25230	1.5	3.39E-03	2.7	-10.6	2
(P)R (8,A-, 3,s)	9 A- A2o	8 s 2-1	nu4	1844.33440	-5.8	8.90E-03	3.3	2.6	3
** (Q)R (8,E, 2,s)	9 E E	16 s 0-1	nu4	1844.89974	-2.4	4.22E-04	3.0	3.5	2
(P)R (8,E, 7,s)	9 E E	6 s 6-1	nu4	1844.96895	1.9	1.03E-03	1.8	-11.2	2
(R)R (10,A+, 3,s)	11 A+ A2e	8 s 4-1	nu4	1844.95283	6.3	2.89E-03	3.3	-1.0	7
(R)R (11,E, 7,s)	12 E E	10 s 8-1	nu4	1845.52247	0.1	4.75E-03	3.6	-8.4	6
(R)R (10,E, 2,s)	11 E E	15 s 3-1	nu4	1845.72215	-1.7	1.25E-03	1.7	2.8	2
(R)R (13,A+, 12,s)	14 A+ A2o	2 s 11-1	nu4	1847.36430	5.1	1.46E-02	3.1	0.3	3
(R)R (11,A-, 6,s)	12 A- A2e	5 s 7-1	nu4	1847.93116	2.1	6.00E-03	3.6	1.3	7
(R)R (12,A-, 9,s)	13 A- A2o	3 s 10-1	nu4	1848.13080	-6.9	7.68E-03	3.2	-2.1	5
(R)R (11,A+, 6,s)	12 A+ A2o	6 s 7-1	nu4	1852.21150	0.4	5.76E-03	1.8	1.3	4
(R)R (13,E, 11,s)	14 E E	5 s 12-1	nu4	1853.15320	-9.8	2.98E-03	2.9	-3.2	4
(R)R (12,A+, 9,s)	13 A+ A2e	4 s 10-1	nu4	1853.24458	0.1	8.47E-03	3.1	-2.6	7
** (Q)R (8,E, 2,s)	9 E E	17 s 0-1	nu4	1853.40157	-7.6	4.48E-04	0.4	-1.0	2
(R)R (11,E, 5,s)	12 E E	13 s 6-1	nu4	1854.33926	5.0	1.80E-03	3.6	2.7	4
** (S)R (10,A+, 0,s)	11 A+ A2e	10 s 2-1	nu4	1855.10688	-4.1	2.00E-03	3.2	-5.3	3
(R)R (14,E, 13,s)	15 E E	0 s 14-1	nu4	1855.70240	8.0	2.44E-03	3.3	1.4	5
(R)R (12,E, 8,s)	13 E E	9 s 9-1	nu4	1856.92693	-0.5	2.25E-03	3.3	-0.3	4
(R)R (11,E, 5,s)	12 E E	13 s 6-1	nu4	1857.90001	0.3	1.55E-03	1.2	0.5	3
(R)R (13,E, 11,s)	14 E E	5 s 12-1	nu4	1858.60582	3.6	3.48E-03	3.5	-5.4	6
(Q)R (13,A-, 12,s)	14 A- A2e	3 s 12-0	2nu2	1859.03265	-2.9	3.48E-03	3.4	-0.5	6
** (Q)R (9,A-, 3,s)	10 A- A2e	8 s 1-1	nu4	1859.12523	1.6	1.38E-03	3.4	3.0	4
(Q)R (11,E, 7,s)	12 E E	9 s 7-0	2nu2	1859.18019	16.0	4.70E-04	4.6	0.9	2
(R)R (9,A+, 4,s)	10 A+ A2o	9 s 1-1	nu4	1859.71605	-1.2	7.28E-03	3.8	1.4	5
(R)R (11,E, 4,s)	12 E E	14 s 5-1	nu4	1859.83655	5.5	1.06E-03	1.1	5.9	4
(P)R (9,E, 1,s)	10 E E	18 s 0-1	nu4	1860.07253	-8.1	3.71E-03	3.6	1.3	6
(Q)R (12,A+, 9,s)	13 A+ A2e	8 s 9-0	2nu2	1860.13364	0.7	7.44E-05	0.6	4.5	2
(P)R (9,E, 2,s)	10 E E	18 s 1-1	nu4	1860.96838	-0.9	3.03E-03	3.8	0.4	6
(R)R (14,E, 13,s)	15 E E	4 s 14-1	nu4	1861.28123	10.8	3.22E-03	3.8	2.1	5
(R)R (12,E, 8,s)	13 E E	9 s 9-1	nu4	1861.45796	-0.2	2.39E-03	2.9	2.1	3
** (Q)R (1,A+, 0,s)	0 A+ A2o	1 s 0-0	2nu2	1862.28769	-0.9	1.44E-03	2.1	-0.4	7
(P)R (8,E, 4,s)	9 E E	14 s 2-1	nu4	1862.42716	2.7	5.52E-04	2.1	8.7	5
(R)R (11,E, 4,s)	12 E E	15 s 5-1	nu4	1862.60906	-0.1	8.10E-04	2.0	2.3	5
(Q)R (11,E, 8,s)	12 E E	18 s 8-0	2nu2	1862.66463	3.8	7.07E-05	1.0	3.8	2
(P)R (9,E, 4,s)	10 E E	13 s 3-1	nu4	1862.92888	1.8	1.79E-03	1.0	-3.2	6
(Q)R (10,A-, 6,s)	10 A- A2o	10 s 6-0	2nu2	1863.48519	-0.2	1.40E-04	2.5	-1.7	3
(R)R (13,E, 10,s)	14 E E	6 s 11-1	nu4	1863.51716	-10.0	1.67E-03	2.8	-2.0	5
** (Q)R (7,E, 5,s)	8 E E	11 s 3-1	nu4	1863.87378	1.2	3.03E-04	2.1	3.1	4
** (P)R (8,E, 4,s)	9 E E	14 s ***	**	1864.13198	5.8	3.91E-04	2.7	0.8	4
(Q)R (9,A-, 3,s)	9 A- A2e	10 s 3-0	2nu2	1864.24305	-1.8	6.46E-05	0.2	3.2	2
(P)R (9,E, 5,s)	10 E E	12 s 4-1	nu4	1864.37486	0.3	1.43E-03	3.4	-5.1	6
(R)R (11,A+, 3,s)	12 A+ A2o	8 s 8-1	nu4	1864.38921	-0.2	1.10E-03	3.2	-0.1	7
(R)R (12,E, 7,s)	13 E E	10 s 8-1	nu4	1864.74759	7.9	1.28E-03	2.6	-1.6	6
(Q)R (9,E, 4,s)	9 E E	18 s 4-0	2nu2	1864.96912	-1.3	6.33E-05	0.0	4.1	2
(Q)R (10,E, 7,s)	10 E E	19 s 7-0	2nu2	1865.10953	0.8	1.13E-04	0.3	-2.0	3
(Q)R (11,A-, 9,s)	11 A- A2e	7 s 9-0	2nu2	1865.14090	5.1	2.32E-04	1.7	7.1	3
** (P)R (9,A-, 3,s)	10 A- A2e	9 s ***	**	1865.52118	-12.5	4.27E-03	3.7	1.5	0
(P)R (9,A+, 6,s)	10 A+ A2o	5 s 5-1	nu4	1865.69535	-0.8	2.15E-03	2.8	-7.5	7
(Q)R (9,E, 5,s)	9 E E	18 s 5-0	2nu2	1866.00388	-1.1	1.06E-04	1.1	-0.7	2
(R)R (11,A-, 6,s)	12 A- A2e	6 s 6-0	2nu2	1866.09318	4.3	2.56E-04	0.0	3.8	2
(P)R (9,E, 7,s)	10 E E	8 s 6-1	nu4	1866.90459	-1.8	7.26E-04	1.7	-13.9	5
(Q)R (10,E, 8,s)	10 E E	17 s 8-0	2nu2	1867.32163	9.9	1.74E-04	3.6	-5.4	2
(Q)R (9,A+, 6,s)	9 A+ A2o	9 s 6-0	2nu2	1867.43969	-1.1	3.40E-04	3.8	-4.0	3
(P)R (9,E, 4,s)	10 E E	14 s 3-1	nu4	1868.23867	-3.6	1.15E-03	1.7	9.7	3
(R)R (12,E, 7,s)	13 E E	12 s 8-1	nu4	1868.59495	-1.4	1.19E-03	2.8	-6.2	5
(P)R (9,A-, 6,s)	10 A- A2e	5 s 5-1	nu4	1868.76255	-0.2	1.74E-03	3.8	4.7	6
(P)R (9,E, 2,s)	10 E E	17 s 1-1	nu4	1868.84055	4.7	1.82E-03	1.7	11.8	6
(Q)R (7,E, 2,s)	7 E E	15 s 2-0	2nu2	1870.07517	0.5	6.49E-05	1.2	1.2	3
(Q)R (8,A-, 6,s)	8 A- A2o	8 s 6-0	2nu2	1871.34262	-1.7	8.23E-04	1.7	0.9	5
(R)R (12,A+, 6,s)	13 A+ A2e	6 s 7-1	nu4	1871.58582	13.4	1.53E-03	2.8	3.4	7
(Q)R (7,E, 4,s)	7 E E	14 s 4-0	2nu2	1871.75659	-0.7	3.00E-04	3.5	0.1	5
(Q)R (9,E, 8,s)	9 E E	15 s 8-0	2nu2	1872.05923	-1.3	4.49E-04	3.8	-1.8	4
(R)R (13,A+, 9,s)	14 A+ A2o	8 s 11-1	nu4	1872.89545	1.5	9.07E-03	1.3	-0.1	7
(R)R (14,A-, 12,s)	15 A- A2o	3 s 11-1	nu4	1873.14347	7.7	3.05E-03	2.4	-0.3	6
(Q)R (7,E, 5,s)	7 E E	14 s 5-0	2nu2	1873.17585	-0.9	5.26E-04	1.5	-0.2	2
(Q)R (14,E, 13,s)	15 E E	0 s 13-0	2nu2	1873.39269	1.1	7.57E-04	3.9	-1.5	5

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)	
(Q)Q (8,E,7,s)	8 E Ee	15 a 7 0	2nu2	1873.60895	-1.5	6.67E-04	1.7	0.9	5
(Q)Q (6,A+,3,s)	6 A+ A2e	6 a 3 0	2nu2	1873.75338	0.0	6.37E-04	1.7	2.5	5
(Q)Q (10,E,10,s)	10 E Eo	8 a 10 0	2nu2	1874.24974	-1.3	4.58E-04	1.4	-2.8	4
(R)R (12,A-,6,s)	13 A- A2o	7 s 7 1	nu4	1874.71938	-2.9	1.38E-03	1.7	1.2	6
(Q)Q (6,E,4,s)	6 E Eo	12 a 4 0	2nu2	1874.89141	-0.4	6.22E-04	2.7	2.6	5
** (Q)R (8,A+,3,s)	9 A+ A2e	9 a 1 1	nu4	1875.05039	-8.0	9.27E-04	0.9	-5.8	4
(Q)Q (7,A+,6,s)	7 A- A2o	7 a 6 0	2nu2	1875.10257	-0.6	1.76E-03	2.1	-0.2	5
(Q)Q (5,E,1,s)	5 E Ee	11 a 1 0	2nu2	1875.16606	0.4	6.01E-05	3.6	1.1	3
** (Q)R (10,E,1,s)	11 E Eo	20 s 1-1	nu4	1875.39062	5.0	2.09E-04	2.5	-6.3	3
(Q)Q (9,A-,9,s)	9 A+ A2e	5 a 9 0	2nu2	1875.46650	-1.3	1.45E-03	1.2	-1.1	5
(Q)Q (5,E,2,s)	5 E Eo	11 a 2 0	2nu2	1875.65042	0.0	2.58E-04	1.5	4.3	4
(Q)Q (6,E,5,s)	6 E Ee	12 a 5 0	2nu2	1876.48292	0.6	1.18E-03	2.2	9.8	2
(Q)Q (8,E,8,s)	8 E Eo	14 a 8 0	2nu2	1876.60860	0.4	1.09E-03	3.1	2.3	5
(R)R (13,A-,9,s)	14 A- A2e	5 s 10 1	nu4	1877.21065	-0.2	1.95E-03	2.9	-0.7	6
(Q)Q (7,E,7,s)	7 E Eo	13 a 7 0	2nu2	1877.66530	1.8	1.43E-03	1.4	0.0	5
(Q)Q (5,E,4,s)	5 E Eo	10 a 4 0	2nu2	1877.74776	0.9	1.18E-03	1.0	1.8	4
(Q)Q (4,E,2,s)	4 E Eo	9 a 2 0	2nu2	1877.98479	0.0	4.65E-04	1.8	2.9	4
** (Q)R (7,A-,6,s)	8 A- A2e	5 s 4 1	nu4	1878.36473	-1.2	4.38E-04	2.6	14.2	4
(Q)Q (6,A-,6,s)	6 A- A2o	6 a 6 0	2nu2	1878.62927	3.1	3.49E-03	3.1	-2.1	8
(Q)Q (4,A+,3,s)	4 A+ A2e	4 a 3 0	2nu2	1878.89743	0.9	2.19E-03	1.2	0.8	6
(Q)Q (3,E,1,s)	3 E Ee	7 a 1 0	2nu2	1879.37188	-0.9	2.05E-04	2.3	5.6	4
(Q)Q (5,E,5,s)	5 E Ee	10 a 5 0	2nu2	1879.49327	3.4	2.04E-03	1.1	-0.1	4
(R)R (12,E,5,s)	13 E Ee	15 s 6 1	nu4	1879.87807	-5.7	3.71E-04	2.0	3.1	4
(Q)Q (3,E,2,s)	3 E Eo	7 a 2 0	2nu2	1879.93197	0.1	8.21E-04	1.7	2.1	4
** (P)R (9,E,2,s)	10 E Eo	19 s **	**	1880.17295	-3.8	2.12E-04	0.9	-9.4	4
(Q)Q (4,E,4,s)	4 E Eo	8 a 4 0	2nu2	1880.25209	2.7	2.12E-03	1.2	-0.2	4
(Q)Q (2,E,1,s)	2 E Ee	5 a 1 0	2nu2	1880.85430	-0.7	3.55E-04	0.8	1.3	3
(Q)Q (3,A-,3,s)	3 A+ A2e	4 a 3 0	2nu2	1880.90214	1.8	3.82E-03	3.2	-1.4	8
** (Q)R (8,E,5,s)	9 E Eo	12 s 3 1	nu4	1881.57006	-0.5	3.37E-04	2.8	9.0	4
(Q)Q (1,E,1,s)	1 E Ee	3 a 1 0	2nu2	1881.86602	0.0	7.63E-04	1.7	3.1	4
(R)R (12,E,4,s)	13 E Ee	16 s 5 1	nu4	1882.36732	7.1	2.38E-04	1.1	8.8	4
** (Q)R (7,A+,6,s)	8 A+ A2o	5 s 4 1	nu4	1882.98833	1.5	2.89E-04	3.6	8.5	5
(R)R (12,E,4,s)	13 E Ee	17 s 5 1	nu4	1884.10922	4.8	1.88E-04	3.7	5.9	4
** (M)R (9,A-,5,s)	10 E Eo	16 s 0 1	nu4	1884.91830	0.8	1.08E-04	2.7	-1.9	3
** (P)R (8,E,5,s)	9 E Ee	13 s **	**	1884.97314	2.7	2.08E-04	1.7	3.0	5
(R)R (12,A-,3,s)	13 A- A2o	9 a 4 1	nu4	1886.33730	-1.1	2.26E-04	2.1	9.8	5
(P)R (10,E,2,s)	11 E Eo	20 s 1-1	nu4	1886.47223	5.2	9.44E-04	0.8	12.4	5
(P)R (10,E,7,s)	11 E Ee	10 s 6-1	nu4	1890.59621	-0.8	3.18E-04	3.0	-5.0	5
(R)R (13,E,7,s)	14 E Ee	14 s 8 1	nu4	1891.33164	-6.8	2.83E-04	1.4	2.6	5
(P)R (10,E,8,s)	11 E Eo	8 s 7-1	nu4	1891.47928	-2.1	2.29E-04	2.9	-10.7	4
** (Q)R (9,A+,3,s)	10 A+ A2o	9 s 1 1	nu4	1891.55827	-1.2	6.60E-04	1.4	0.6	4
(P)R (14,E,10,s)	15 E Ee	17 s 11 1	nu4	1892.70988	1.0	3.84E-04	0.6	0.3	0
(P)R (10,A-,6,s)	11 A- A2e	6 s 5-1	nu4	1893.81839	-1.5	6.50E-04	1.9	19.8	5
** (N)R (9,E,5,s)	10 E Ee	13 s 2 0	2nu2	1898.08377	-4.6	1.38E-04	2.5	16.5	2
** (Q)R (8,A+,6,s)	9 A+ A2e	6 s 4 1	nu4	1899.67388	0.9	4.42E-04	2.2	16.6	5
** (Q)R (10,E,4,s)	11 E Eo	17 a 2 1	nu4	1902.99757	0.4	1.90E-04	1.6	12.0	4
** (P)R (8,A-,6,s)	9 A- A2o	6 s **	**	1904.80155	0.3	2.41E-04	2.1	12.0	4
(P)R (11,E,4,s)	12 E Eo	18 s 3-1	nu4	1911.75777	-3.0	1.14E-04	2.6	20.6	3
** (M)R (9,E,4,s)	10 E Ee	18 s 0 1	nu4	1913.53002	-8.2	9.30E-05	4.0	7.2	2
(P)R (11,E,8,s)	12 E Ee	10 s 8-1	nu4	1915.23670	-0.2	9.03E-04	2.1	9.1	3
(P)R (11,A-,4,s)	12 A- A2e	4 s 8-1	nu4	1915.83654	-4.4	1.30E-04	3.8	-2.2	4
** (M)R (8,E,5,s)	9 E Ee	15 s 1-1	nu4	1919.12782	-5.1	4.56E-05	1.7	0.3	2
(Q)R (1,A+,0,s)	2 A+ A2o	3 a 0 0	2nu2	1920.42203	-1.2	6.13E-04	3.0	-1.3	5
(Q)R (1,E,1,s)	2 E Ee	5 a 1 0	2nu2	1920.62057	-0.2	2.34E-04	3.1	-0.6	3
** (Q)R (9,A-,6,s)	10 A- A2e	7 s 4 1	nu4	1920.73281	0.1	3.18E-04	3.7	17.7	4
(Q)R (2,E,1,s)	3 E Ee	7 a 1 0	2nu2	1938.97002	-0.6	1.42E-04	2.7	-1.0	5
(Q)R (2,E,2,s)	3 E Eo	7 a 2 0	2nu2	1939.55826	0.3	8.97E-05	3.8	-1.4	4
(Q)R (3,A+,0,s)	4 A+ A2o	5 a 0 0	2nu2	1956.64465	-0.2	7.14E-05	1.5	-1.2	3
(Q)R (3,E,2,s)	4 E Eo	9 a 2 0	2nu2	1957.39133	-0.5	2.61E-04	2.5	3.2	3
(Q)R (3,A-,3,s)	4 A- A2e	7 a 0 0	2nu2	1958.36668	-0.7	7.74E-05	2.5	-5.2	3
(Q)R (5,A-,5,s)	6 A+ A2o	7 a 0 0	2nu2	1991.04961	1.1	4.80E-05	3.8	-3.6	4
(Q)R (5,E,4,s)	6 E Eo	12 a 4 0	2nu2	1993.82281	-0.6	2.80E-05	5.1	1.5	4
(Q)R (6,E,1,s)	7 E Ee	15 a 1 0	2nu2	2007.82592	1.3	5.92E-05	3.2	0.4	3
(Q)R (6,E,2,s)	7 E Eo	15 a 2 0	2nu2	2008.27253	0.8	6.05E-05	3.0	-1.2	5
(Q)R (6,A+,3,s)	7 A+ A2e	8 a 3 0	2nu2	2009.04970	0.1	1.25E-04	3.3	-3.0	5
(Q)R (6,E,4,s)	7 E Eo	14 a 4 0	2nu2	2010.20787	-0.3	6.78E-05	3.0	1.8	4
(Q)R (6,E,5,s)	7 E Ee	14 a 5 0	2nu2	2011.82013	-0.7	6.93E-05	3.5	7.8	4
(Q)R (6,A-,6,s)	7 A- A2o	7 a 6 0	2nu2	2013.98669	-0.2	9.77E-05	3.9	2.3	4
(Q)R (7,A+,0,s)	8 A+ A2o	8 a 0 0	2nu2	2024.00279	1.0	1.35E-04	3.8	-3.0	5
(Q)R (7,E,1,s)	8 E Eo	17 a 1 0	2nu2	2024.13197	0.8	1.93E-05	3.9	1.4	3
(Q)R (7,E,2,s)	8 E Eo	17 a 2 0	2nu2	2024.52889	0.4	7.73E-05	2.4	-0.6	4
(Q)R (7,A-,3,s)	8 A- A2e	8 a 3 0	2nu2	2025.22160	0.3	1.53E-04	2.6	-2.6	5
(Q)R (7,E,4,s)	8 E Eo	16 a 4 0	2nu2	2026.25758	-0.5	8.06E-05	3.8	-4.3	5
(Q)R (7,E,5,s)	8 E Ee	16 a 5 0	2nu2	2027.70681	-1.1	8.94E-05	3.4	1.6	5
(Q)R (7,A+,6,s)	8 A+ A2o	8 a 6 0	2nu2	2029.66434	-1.5	1.69E-04	2.6	-0.4	5
(Q)R (7,E,7,s)	8 E Ee	15 a 7 0	2nu2	2032.25451	-1.0	6.86E-05	2.3	7.0	3
(Q)R (8,E,1,s)	9 E Ee	19 a 1 0	2nu2	2040.18913	-0.3	5.98E-05	3.0	-0.1	5
(Q)R (8,E,2,s)	9 E Eo	19 a 2 0	2nu2	2040.53266	-0.5	6.37E-05	3.9	-0.2	5
(Q)R (8,A+,3,s)	9 A+ A2e	13 a 2 1	nu4	2041.13421	-1.6	1.30E-04	3.8	-3.0	5
(Q)R (8,E,5,s)	9 E Ee	18 s 5 0	2nu2	2043.11303	-0.9	9.87E-05	3.9	-3.4	5
(Q)R (8,A-,6,s)	9 A- A2o	9 a 6 0	2nu2	2045.04535	-1.0	1.72E-04	2.9	-1.2	4
(Q)R (8,E,7,s)	9 E Ee	17 a 7 0	2nu2	2047.35357	-1.1	8.57E-05	3.3	-0.2	5
(Q)R (8,E,8,s)	9 E Eo	15 a 8 0	2nu2	2050.38771	-1.1	6.72E-05	2.7	2.3	3
(Q)R (9,A+,0,s)	10 A+ A2o	11 a 0 0	2nu2	2055.96850	1.5	7.99E-05	2.4	2.6	5
(Q)R (9,E,2,s)	10 E Eo	21 a 2 0	2nu2	2056.34873	0.7	4.31E-05	2.6	3.1	4

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
(Q)R (9,A-, 3,s)	10 A- A2e	10 a 3 0	2nu2 2056.85424	1.5	8.74E-05	3.4	-4.1	4
(Q)R (9,E, 4,s)	10 E Eo	20 a 4 0	2nu2 2057.62150	-0.5	5.42E-05	3.2	6.5	4
(Q)R (9,E, 5,s)	10 E Ee	20 a 5 0	2nu2 2058.71072	-0.6	5.90E-05	3.4	2.8	5
(Q)R (9,A+, 6,s)	10 A+ A2o	10 a 6 0	2nu2 2060.20644	-0.1	1.21E-04	3.4	-7.4	4
(Q)R (9,E, 7,s)	10 E Ee	19 a 7 0	2nu2 2062.21803	0.5	7.04E-05	3.6	-1.5	4
(Q)R (10,A+, 3,s)	11 A+ A2e	12 a 3 0	2nu2 2072.44775	1.0	5.11E-05	4.0	2.6	4
(Q)R (10,E, 4,s)	11 E Eo	22 a 4 0	2nu2 2073.07202	1.8	2.88E-05	6.9	2.3	3
(Q)R (10,A-, 6,s)	11 A- A2o	11 a 6 0	2nu2 2075.22434	-0.1	7.60E-05	2.7	-0.7	4
(Q)R (10,E, 7,s)	11 E Ee	21 a 7 0	2nu2 2076.93188	1.4	4.50E-05	4.3	0.5	4
(Q)R (10,E, 8,s)	11 E Eo	18 a 8 0	2nu2 2079.22468	3.5	5.01E-05	2.6	-1.5	3
(Q)R (10,A+, 9,s)	11 A+ A2e	7 a 9 0	2nu2 2082.26904	5.4	9.93E-05	3.6	-6.7	3
(Q)R (11,A+, 6,s)	12 A+ A2o	12 a 6 0	2nu2 2090.17607	0.1	3.82E-05	3.6	2.9	3
(Q)R (11,A-, 9,s)	12 A- A2e	8 a 9 0	2nu2 2096.09250	0.9	5.92E-05	3.8	-9.4	3

Note: (I): Assignment; (II) Identification of the upper level; (III): Vibrational band;  
 (IV): Observed wavenumber in  $\text{cm}^{-1}$ ; (V) (Obs-calc) wavenumber in  $10^{-3} \text{cm}^{-1}$ ;  
 (VI)  $S_0$  in  $\text{cm}^{-2} \text{atm}^{-1}$  at 296 K; (VII) Experimental uncertainty in %;  
 (VIII):  $S_0-S_c/S_0$  in %; (IX): number of spectra used for the measurements.

Line-by-line prediction for the  $2\nu_2/\nu_4$  system of ammonia  $^{14}\text{NH}_3$  between 1253 and 2134  $\text{cm}^{-1}$ .

(I)	(II)	(III)	(IV)	(V)	(VI)	(VII)	(VIII)	(IX)
* S P 12 7 a 11	Ex 4 a 9-1 nu4	c1253.84756	0.0	0.173E-04	2613.17796	1359.32885	0.0	
* S P 12 7 a 11	Ex 4 a 9-1 nu4	c1256.09640	0.0	0.170E-04	2614.96760	1358.87122	0.0	
* R P 15 13 a 14	Ex 2 a14-1 nu4	c1263.02824	0.0	0.106E-04	3010.78978	1747.76485	0.0	
* R P 15 13 a 14	Ex 2 a14-1 nu4	c1265.21894	-6.3	0.105E-04	2923.64635	1658.42705	1.0	
* S P 11 7 a 10	Ex 2 a 9-1 nu4	1266.72870	-26.3	0.235E-04	2391.29848	1124.56715	0.0	
* R P 16 12 a 15	A2o 3 a13-1 nu4	n1267.49246	0.0	0.137E-04	3417.71750	2150.27904	0.0	
* S P 13 6 a 12	A2o 5 a 8-1 nu4	c1268.51493	0.0	0.217E-04	2926.59256	1658.07925	0.0	
* S P 13 6 a 12	Ex 2 a 9-1 nu4	c1268.67642	0.0	0.216E-04	2932.71235	1124.03568	0.0	
* Q P 15 13 a 14	Ex 2 a13-0 2nu2	c1272.38091	0.0	0.155E-04	3020.91370	1748.53216	0.0	
* Q P 14 13 a 13	Ex 1 a13-0 2nu2	n1277.08856	0.0	0.199E-04	2780.82459	1453.73603	0.0	
* S P 12 6 a 11	A2e 3 a 8-1 nu4	1277.39640	-32.7	0.494E-04	2682.96210	1450.56243	1.0	
* R P 15 12 a 14	A2o 2 a13-1 nu4	c1277.97048	0.0	0.354E-04	3116.43000	1816.45573	0.0	
* S P 12 6 a 11	A2o 4 a 8-1 nu4	c1280.08220	0.0	0.478E-04	2695.23360	1405.15377	0.0	
* S P 10 7 a 9	Ex 1 a 9-1 nu4	c1280.34029	0.0	0.182E-04	2188.91078	908.57496	0.0	
* S P 10 7 a 9	Ex 1 a 9-1 nu4	c1282.09599	0.0	0.185E-04	2190.06398	907.96503	0.0	
* R P 15 12 a 14	Ex 5 a12-1 nu4	c1288.04972	0.0	0.135E-04	2985.00837	1696.95789	0.0	
* R P 14 12 a 13	A2o 1 a13-1 nu4	c1288.59486	0.0	0.557E-04	2833.23415	1544.63569	0.0	
* Q P 15 12 a 14	A2e 3 a12-0 2nu2	c1289.91873	0.0	0.291E-04	3128.99551	1839.07397	0.0	
* S P 11 6 a 10	A2e 2 a 8-1 nu4	1290.31600	-35.3	0.641E-04	2461.55485	1171.23532	0.0	
* S P 11 6 a 10	Ex 1 a 7-1 nu4	c1292.13731	0.0	0.123E-04	2968.77752	1696.64181	0.0	
* S P 11 6 a 10	A2o 3 a 8-1 nu4	1292.55720	22.7	0.831E-04	2463.31577	1170.76084	1.0	
* T P 12 3 a 11	A2e 5 a 6 2nu2	1295.47765	0.0	0.125E-04	2795.95405	1500.40405	0.0	
* Q P 14 12 a 13	A2e 4 a12-0 2nu2	c1297.45717	0.0	0.785E-04	2842.83918	1545.38132	0.0	
* R P 14 11 a 13	Ex 4 a12-1 nu4	c1297.50157	0.0	0.135E-04	2926.26195	1628.76733	0.0	
* R P 15 10 a 14	Ex 6 a11-1 nu4	c1298.05720	0.0	0.124E-04	3294.04406	1995.97688	0.0	
* S P 12 11 a 13	Ex 8 a 7-1 nu4	c1300.22147	-32.2	0.518E-04	2744.62581	1474.65599	1.0	
* R P 14 11 a 13	Ex 4 a12-1 nu4	c1302.52553	0.0	0.479E-04	3290.67894	1628.15646	0.0	
* R P 15 10 a 14	Ex 8 a11-1 nu4	c1302.86597	0.0	0.194E-04	3298.42397	1995.55410	0.0	
* Q P 13 12 a 12	A2e 1 a12-0 2nu2	1302.99347	-39.8	0.901E-04	2572.95742	1269.95997	1.0	
* S P 11 5 a 11	Ex 1 a 8-1 nu4	1303.97310	-4.2	0.104E-03	2259.62339	955.65077	1.0	
* S P 10 6 a 9	A2o 2 a 8-1 nu4	1305.90350	9.8	0.105E-03	2251.01085	955.10643	1.0	
* T P 11 3 a 10	A2e 4 a 6 2nu2	c1306.88637	0.0	0.189E-04	2573.82086	1266.93735	0.0	
* R P 15 10 a 14	Ex 6 a11-1 nu4	c1307.04928	0.0	0.271E-04	3371.74052	2062.79828	0.0	
* R P 14 10 a 13	Ex 4 a11-1 nu4	c1309.59681	0.0	0.255E-04	3013.74785	1740.14728	0.0	
* S P 13 9 a 12	Ex 12 a 6-1 nu4	c1310.27181	0.0	0.153E-04	3038.61908	1728.34758	0.0	
* R P 15 9 a 14	A2e 5 a10-1 nu4	c1311.11479	0.0	0.340E-04	3373.55332	2062.43817	0.0	
* S P 11 5 a 11	Ex 6 a 7-1 nu4	c1313.82047	-21.1	0.618E-04	2523.64417	1210.51006	1.0	
* Q P 14 11 a 13	Ex 5 a11-0 2nu2	c1313.76139	0.0	0.382E-04	2942.53034	1628.76733	0.0	
* R P 13 11 a 12	Ex 2 a12-1 nu4	1314.02974	-43.6	0.693E-04	2667.60044	1353.56634	1.0	
* R P 14 10 a 13	Ex 6 a11-1 nu4	1314.64530	18.9	0.560E-04	3180.46124	1703.63799	0.0	
* R P 14 10 a 13	Ex 12 a 6-1 nu4	1315.08550	0.0	0.135E-04	3043.45519	1728.05529	0.0	
* S P 11 5 a 10	Ex 7 a 7-1 nu4	1315.80550	19.6	0.601E-04	2525.88453	1210.08099	1.0	
* S P 9 6 a 8	A2e 1 a 8-1 nu4	1318.34980	38.3	0.729E-04	2377.34830	759.02033	1.0	
* S P 10 6 a 9	A2e 11 a 7-1 nu4	c1319.01929	0.0	0.215E-04	2371.12555	1052.10640	0.0	
* S P 9 6 a 8	A2o 1 a 8-1 nu4	1320.08738	-10.4	0.744E-04	2078.47368	758.38526	1.0	
* S P 14 3 a 13	A2o 8 a 5-1 nu4	c1320.57445	0.0	0.111E-04	3434.50878	2022.93218	0.0	
* R P 15 10 a 14	Ex 6 a10-0 2nu2	c1320.76577	0.0	0.589E-04	3092.59841	1771.74237	0.0	
* R P 13 10 a 12	Ex 3 a11-1 nu4	c1321.88924	0.0	0.332E-04	2752.40109	1430.51691	0.0	
* R P 15 8 a 14	Ex 11 a 9-1 nu4	c1322.04446	0.0	0.140E-04	3443.86017	2121.81062	0.0	
* Q P 13 11 a 12	Ex 3 a11-0 2nu2	1322.21497	-8.4	0.945E-04	2676.50991	1354.29411	1.0	
* R P 15 8 a 14	Ex 12 a 6-1 nu4	1322.38160	-21.3	0.798E-04	2798.58204	1476.18344	0.0	
* T P 12 2 a 11	Ex 12 a 5-0 2nu2	c1323.24589	0.0	0.103E-04	2841.19516	1517.94098	0.0	
* R P 14 9 a 13	A2e 4 a10-1 nu4	1325.70145	2.3	0.111E-03	2907.01158	1771.31036	0.0	
* S P 12 4 a 11	Ex 9 a 6-1 nu4	1326.49272	-34.8	0.262E-04	3475.83298	1475.83298	0.0	
* R P 15 6 a 10	Ex 5 a 7-1 nu4	1326.79440	-7.3	0.954E-04	2322.05699	895.26756	1.0	
* R P 15 7 a 14	Ex 12 a 8-1 nu4	n1326.96421	0.0	0.116E-04	3501.07234	2174.10813	0.0	
* R P 13 7 a 12	Ex 4 a11-1 nu4	1326.97818	26.6	0.123E-03	2756.88609	1429.10557	1.0	
* R P 13 7 a 12	Ex 12 a 8-1 nu4	c1328.00928	0.0	0.262E-04	3704.14728	2174.10813	0.0	
* Q P 12 11 a 11	Ex 1 a11-0 2nu2	1328.51179	-6.2	0.964E-04	2426.80659	1098.29418	1.0	
* S P 10 5 a 9	Ex 5 a 7-1 nu4	1329.02560	14.3	0.947E-04	2323.79730	994.77313	1.0	
* R P 15 7 a 14	Ex 14 a 8-1 nu4	c1329.75939	0.0	0.108E-04	3503.60181	2173.83620	0.0	
* R P 14 8 a 13	Ex 9 a 9-1 nu4	c1330.83048	0.0	0.388E-04	3162.57624	1891.74499	0.0	
* U P 9 3 a 8	A2e 3 a 7-1 nu4	c1331.60835	0.0	0.172E-04	2817.78722	856.17882	0.0	
* S P 13 3 a 12	A2o 7 a 5-1 nu4	1331.98340	-7.7	0.331E-04	3084.63133	1752.64820	0.0	
* R P 13 3 a 12	A2o 2 a10-1 nu4	1333.00686	-25.7	0.120E-03	3831.86702	1498.85659	1.0	
* R P 15 6 a 14	A2e 7 a 7-1 nu4	c1334.20569	0.0	0.190E-04	3553.07739	2218.89848	0.0	
* R P 14 8 a 13	Ex 9 a 9-1 nu4	1335.21138	-20.4	0.496E-04	3166.55558	1831.37216	0.0	
* S P 11 4 a 10	Ex 8 a 6-1 nu4	1335.25570	-19.1	0.817E-04	2577.76266	1242.50505	1.0	
* R P 12 10 a 11	Ex 10 a 6-1 nu4	c1335.39726	0.0	0.176E-04	2620.00139	1284.60633	0.0	
* R P 12 10 a 11	Ex 1 a11-1 nu4	c1335.44063	0.0	0.129E-04	2510.74722	1175.32160	0.0	
* R P 15 6 a 14	Ex 8 a 7-1 nu4	n1336.34008	0.0	0.158E-04	3554.99555	2218.65547	0.0	
* Q P 13 10 a 12	Ex 4 a10-0 2nu2	1337.27057	-56.3	0.964E-04	2767.79311	1430.51691	1.0	
* R P 13 9 a 12	A2e 3 a10-1 nu4	1338.17080	7.5	0.278E-04	3090.60455	1752.43300	0.0	
* R P 13 9 a 12	A2e 3 a10-1 nu4	1338.42300	14.5	0.295E-03	2866.76403	1498.34248	1.0	
* S P 11 4 a 10	Ex 7 a 6-1 nu4	1338.53050	18.9	0.775E-04	2580.63514	1242.10653	1.0	
* R P 12 10 a 11	Ex 2 a11-1 nu4	1339.33299	-35.1	0.163E-03	3513.94456	1174.60866	0.0	
* R P 13 10 a 12	Ex 12 a 8-1 nu4	c1339.52658	0.0	0.380E-04	3224.01318	1884.51145	0.0	
* Q P 14 9 a 13	A2o 4 a 9-0 2nu2	c1340.55425	0.0	0.256E-04	3112.31371	1771.74237	0.0	
* S P 9 5 a 8	Ex 3 a 7-1 nu4	1341.19140	-0.6	0.107E-03	2410.12629	798.93483	1.0	
* S P 9 5 a 8	Ex 3 a 7-1 nu4	1343.11540	-7.0	0.108E-03	2141.43061	798.37451	0.0	
* R P 14 7 a 13	Ex 12 a 8-1 nu4	c1343.26905	0.0	0.885E-04	2902.78514	1559.51145	0.0	
* R P 14 7 a 13	Ex 12 a 8-1 nu4	1343.47340	-1.5	0.413E-04	2227.46757	1883.99402	1.0	
* S P 12 3 a 11	A2o 6 a 5-1 nu4	1343.96980	-11.6	0.888E-04	2844.73618	1500.76522	0.0	
* R P 12 3 a 11	A2o 2 a10-1 nu4	c1346.02129	0.0	0.145E-03	2590.38887	1244.37178	0.0	
* Q P 14 10 a 12	Ex 2 a10-0 2nu2	1346.65859	-0.8	0.218E-03	2521.98027	1175.32160	0.0	
* R P 14 6 a 13	A2e 6 a 7-1 nu4	c1347.53461	0.0	0.707E-04	2477.13487	1029.61381	0.0	
* P 10 2 a 9	Ex 8 a 5-1 nu4	c1348.35964	0.0	0.233E-04	3218.30719	1969.94630	0.0	
* R P 13 8 a 12	Ex 7 a 9-1 nu4	1348.89910	-18.1	0.144E-03	2376.42640	1027.53549	0.0	
* S P 12 3 a 11	A2e 6 a 5-1 nu4	1349.06590	-6.9	0.773E-04	2849.47064	1500.40405	1.0	
* T P 12 1 a 11	Ex 13 a 4-0 2nu2	c1349.08321	0.0	0.155E-04	2877.52928	1528.43337	0.0	
* Q P 13 13 a 12	A2o 3 a 2nu2	1350.38032	57.7	0.140E-03	1489.85659	1929.32140	1.0	
* R P 14 6 a 13	A2e 7 a 7-1 nu4	1350.55050	-41.6	0.643E-04	3279.87606	1929.32140	0.0	
* R P 12 9 a 11	A2e 2 a10-1 nu4	1351.33500	6.2	0.597E-03	2595.10152	1242.76714	0.0	
* S P 10 4 a 9	Ex 6 a 6-1 nu4	1351.55910	15.3	0.141E-03	2738.63605	1027.07848	1.0	
* S P 10 4 a 9	Ex 8 a 1-1 nu4	c1352.57889	2.4	0.103E-03	2965.18390	1612.65777	1.0	
* S P 13 2 a 12	Ex 16 a 4-1 nu4	c1353.12392	0.0	0.179E-04	3223.13837	1770.01299	0.0	
* Q P 11 10 a 10	Ex 1 a10-0 2nu2	1353.60313	10.0	0.192E-03	2192.39035	938.78822	1.0	
* R P 14 5 a 13	Ex 15 a 6-1 nu4	n1354.17543	0.0	0.295E-04	3321.91790	1967.74247	0.0	
* R P 14 5 a 13	Ex 15 a 6-1 nu4	c1356.16705	0.0	0.145E-03	2605.81799	1305.64892	0.0	
* S P 8 5 a 7	Ex 2 a 7-1 nu4	1356.30430	32.8	0.680E-04	2777.99395	1621.69293	0.0	
* R P 14 5 a 13	Ex 15 a 6-1 nu4	c1356.50902	0.0	0.232E-04	3323.98900	1967.47665	0.0	
* S P 11 3 a 10	A2o 5 a 5-1 nu4	1356.79240	0.0	0.201E-03	2624.08137	1267.28897	1.0	

R P 13	7 a	12	Ex 10	a 8-1	nu4	1357.29522	5.4	0.137E-03	2969.55808	1612.26340	1.0
* S P 9	5 a	7	Ex 16	a 5-1	nu4	1358.02650	-49.6	0.698E-04	1979.09701	1621.06555	1.0
R P 14	4 a	13	Ex 16	a 5-1	nu4	c1359.73710	0.0	0.221E-04	3358.53654	1998.00673	0.0
* S P 11	10 a	12	Ex 10	a 8-1	nu4	1359.25914	0.0	0.137E-04	2969.76232	1600.68726	1.0
R P 12	9 a	11	Ex 10	a 8-1	nu4	1360.46523	-44.9	0.471E-03	2604.84150	1244.37178	1.0
R P 13	6 a	12	Ex 16	a 5-1	nu4	1360.73889	15.7	0.214E-03	3019.16437	1658.42705	1.0
* S P 13	2 a	12	Ex 16	a 5-1	nu4	c1360.76185	0.0	0.139E-04	3130.50935	1769.74967	0.0
* S P 11	10 a	12	Ex 10	a 8-1	nu4	1360.82768	-1.2	0.185E-03	2627.76507	1266.33135	1.0
R P 14	4 a	13	Ex 16	a 5-1	nu4	1361.39008	0.0	0.149E-04	3359.59598	1998.56090	0.0
* T P 13	0 a	12	Ex 16	a 5-1	nu4	c1361.54862	0.0	0.316E-04	3145.19056	1783.59992	0.0
* S P 9	5 a	7	Ex 16	a 5-1	nu4	1361.75510	94.4	0.368E-04	2921.05371	1559.51151	0.0
R P 13	6 a	12	Ex 16	a 5-1	nu4	c1361.88736	0.0	0.122E-04	3287.61876	1871.92929	0.0
* P 11	1 a	11	Ex 11	a 5-1	nu4	c1361.93344	0.0	0.294E-04	2657.12890	1295.19577	0.0
R P 12	1 a	11	Ex 10	a 8-1	nu4	c1361.94018	0.0	0.369E-03	2667.06641	1305.12737	0.0
* S P 9	5 a	7	Ex 16	a 5-1	nu4	c1361.94018	0.0	0.201E-03	2194.73251	831.00303	0.0
R P 14	3 a	13	Ex 10	a 8-1	nu4	c1364.17057	0.0	0.266E-04	3387.10358	1922.93218	1.0
R P 11	9 a	10	Ex 10	a 8-1	nu4	1364.50674	-33.5	0.730E-03	2372.31851	1007.80842	1.0
R P 13	6 a	12	Ex 16	a 5-1	nu4	1364.89364	9.8	0.230E-03	3022.97191	1658.07925	1.0
* S P 12	1 a	11	Ex 14	a 5-1	nu4	1364.93155	6.4	0.128E-04	2897.15290	1400.62426	0.0
* S P 12	2 a	11	Ex 14	a 5-1	nu4	1365.10106	29.9	0.429E-03	2883.34813	1510.25026	1.0
R P 14	3 a	13	Ex 10	a 8-1	nu4	1365.26320	0.0	0.145E-04	3387.87345	1922.61025	0.0
* S P 9	5 a	7	Ex 16	a 5-1	nu4	1365.50310	18.4	0.201E-03	2196.44145	830.94019	0.0
* S P 12	1 a	11	Ex 14	a 5-1	nu4	1365.51819	0.0	0.207E-03	2724.85048	1352.52428	1.0
R P 13	5 a	12	Ex 13	a 6-1	nu4	1367.89296	45.7	0.101E-03	3064.84628	1696.95789	1.0
* Q P 15	4 a	14	Ex 19	a 4-0	2nu2	1369.41051	0.0	0.127E-04	3656.74329	2287.33278	0.0
* U P 9	1 a	9	Ex 5	a 5-1	nu4	c1369.48129	0.0	0.134E-04	2450.50662	1081.02772	0.0
R P 16	15 a	15	Ex 14	a 5-1	nu4	c1369.78817	209.4	0.401E-03	2617.20943	1644.83133	0.0
R P 11	8 a	10	Ex 4	a 9-1	nu4	c1369.84115	0.0	0.138E-03	2404.21673	1070.37730	0.0
* S P 10	3 a	9	Ex 4	a 5-1	nu4	1370.33490	-12.9	0.390E-03	2422.88602	1052.54983	0.0
R P 12	7 a	11	Ex 9	a 8-1	nu4	1370.61320	3.9	0.963E-03	2379.32438	1000.62438	0.0
* Q P 13	7 a	12	Ex 9	a 7-0	2nu2	1371.09404	0.0	0.110E-04	2983.73131	1612.65277	0.0
R P 12	7 a	11	Ex 7	a 8-1	nu4	1371.25540	5.0	0.383E-03	2730.12612	1358.87122	1.0
R P 13	5 a	12	Ex 13	a 6-1	nu4	1371.34030	13.8	0.890E-04	3067.98073	1696.44181	0.0
* S P 12	1 a	11	Ex 14	a 5-1	nu4	1371.34909	-38.0	0.400E-04	2889.29120	1511.99789	0.0
P P 16	16 a	15	Ex 1	a 15-1	nu4	1371.66921	-38.0	0.136E-02	3112.50914	1740.83613	1.0
P P 16	16 a	15	Ex 1	a 15-1	nu4	1371.79663	39.0	0.135E-02	3113.96118	1742.16845	1.0
* Q P 12	8 a	11	Ex 8	a 8-0	2nu2	1372.18222	-4.4	0.183E-03	2677.86748	1305.64862	0.0
R P 15	14 a	11	Ex 18	a 3-1	nu4	1373.12777	0.0	0.158E-03	3120.21200	2311.58828	0.0
* S P 13	1 a	12	Ex 18	a 3-1	nu4	c1373.46802	0.0	0.190E-04	3155.86733	1780.39613	0.0
* S P 10	3 a	9	Ex 4	a 5-1	nu4	1373.61620	10.2	0.371E-03	2425.72158	1052.10640	0.0
R P 13	4 a	12	Ex 14	a 5-1	nu4	1373.94240	-15.6	0.409E-03	2779.50839	1400.62438	0.0
R P 13	4 a	12	Ex 14	a 5-1	nu4	1373.99091	24.2	0.875E-04	3102.33607	1728.34758	1.0
* Q P 14	5 a	13	Ex 16	a 5-0	2nu2	1374.46175	0.0	0.128E-04	3342.20422	1967.74247	0.0
P P 16	15 a	15	Ex 1	a 14-1	nu4	1374.62837	-4.3	0.158E-02	3231.01311	1856.38431	1.0
P P 16	15 a	15	Ex 1	a 14-1	nu4	1375.23141	-15.1	0.160E-02	3232.63583	1857.19139	1.0
* Q P 15	2 a	14	Ex 23	a 2-0	2nu2	1375.51158	0.0	0.191E-04	3703.63383	2328.12225	0.0
* R P 11	8 a	10	Ex 3	a 9-1	nu4	1375.60440	6.1	0.689E-03	2445.37497	1069.77148	1.0
* R P 11	8 a	10	Ex 3	a 9-1	nu4	c1375.78181	0.0	0.440E-04	2456.41972	1088.62246	0.0
* U P 8	2 a	7	Ex 5	a 6-1	nu4	c1375.81859	0.0	0.159E-04	2073.21284	697.39533	0.0
* Q P 15	1 a	14	Ex 25	a 1-0	2nu2	1376.58475	0.0	0.237E-04	3714.87285	2338.28810	1.0
R P 13	4 a	12	Ex 15	a 5-1	nu4	1376.66001	-4.1	0.616E-04	3710.71571	1728.05529	1.0
P P 16	15 a	15	Ex 1	a 13-1	nu4	1377.12208	3.9	0.479E-03	3340.21786	1945.83431	0.0
* S P 11	2 a	10	Ex 12	a 4-1	nu4	1377.78420	3.9	0.118E-03	2662.74905	1284.96524	1.0
* Q P 10	9 a	9	Ex 2	a 9-0	2nu2	1378.24030	9.8	0.754E-03	2198.72726	981.48794	1.0
* S P 9	5 a	7	Ex 2	a 6-1	nu4	1378.38670	-2.7	0.204E-03	2032.83724	654.45027	1.0
P P 16	15 a	15	Ex 1	a 13-1	nu4	1378.48328	-34.2	0.484E-03	3342.17911	1946.87737	0.0
* Q P 14	4 a	13	Ex 17	a 4-0	2nu2	1378.87347	0.0	0.257E-04	3377.68015	1998.00673	0.0
R P 11	7 a	10	Ex 4	a 8-1	nu4	1378.98757	-21.5	0.291E-03	2503.56687	1124.56715	0.0
* R P 11	7 a	10	Ex 4	a 8-1	nu4	1379.04077	9.2	0.129E-03	3131.68806	1728.05529	1.0
R P 12	6 a	11	Ex 10	a 8-1	nu4	1379.36010	4.8	0.712E-03	2784.51339	1405.15377	1.0
P P 16	13 a	15	Ex 6	a 12-1	nu4	1379.78032	83.5	0.305E-03	3040.52761	2060.75564	1.0
* S P 8	4 a	7	Ex 3	a 6-1	nu4	1380.30880	-14.2	0.208E-03	2034.18082	653.87060	1.0
* S P 12	1 a	11	Ex 12	a 4-1	nu4	1380.44410	-6.9	0.741E-04	3133.28406	1793.44544	0.0
* Q P 14	3 a	13	Ex 10	a 8-1	nu4	c1381.34056	0.0	0.705E-04	3044.26861	1922.93218	0.0
R P 12	5 a	11	Ex 11	a 6-1	nu4	1381.39767	-11.4	0.270E-03	2825.87540	1444.47659	1.0
P P 16	13 a	15	Ex 6	a 12-1	nu4	1381.59254	-75.9	0.320E-03	3442.98424	2061.38411	1.0
* R P 16	13 a	15	Ex 6	a 12-1	nu4	1382.00322	114.2	0.407E-03	3522.29023	2152.5882	0.0
* Q P 12	7 a	11	Ex 7	a 7-0	2nu2	1382.15349	19.4	0.107E-03	2741.48040	1359.32885	1.0
* S P 11	2 a	10	Ex 12	a 4-1	nu4	1382.83010	-22.2	0.104E-03	2667.43865	1284.60633	0.0
* S P 13	1 a	12	Ex 17	a 3-1	nu4	1383.06258	0.0	0.371E-04	3152.72020	1778.29939	0.0
* S Q 14	12 a	14	Ex 1	a 14-1	nu4	c1383.15564	0.0	0.414E-04	2928.53742	1545.38132	0.0
* Q P 11	8 a	10	Ex 5	a 8-0	2nu2	1383.38742	-34.8	0.558E-03	2455.76820	1070.37730	1.0
* P 14	0 a	12	Ex 12	a 11-1	nu4	c1383.55559	0.0	0.123E-04	3471.29847	2053.74288	0.0
* S P 12	1 a	11	Ex 12	a 4-1	nu4	c1383.96958	0.0	0.135E-04	3153.77155	1780.39613	0.0
* R P 13	1 a	12	Ex 19	a 2-0	2nu2	1384.03372	0.0	0.171E-04	3164.17331	1780.13959	0.0
P P 16	11 a	15	Ex 10	a 10-1	nu4	1384.05563	120.4	0.142E-03	3615.80435	2231.75076	1.0
* Q P 14	2 a	13	Ex 21	a 2-0	2nu2	1384.37493	0.0	0.457E-04	3424.41828	2040.70414	0.0
P P 16	15 a	15	Ex 1	a 11-1	nu4	1384.60601	-2.0	0.134E-03	3345.40125	2152.5882	1.0
* S P 9	3 a	8	Ex 2	a 3-5-1	nu4	1384.67720	-12.3	0.622E-03	2241.33686	856.65843	1.0
* Q P 10	8 a	9	Ex 2	a 8-0	2nu2	c1384.69820	0.0	0.184E-04	2238.60108	853.90676	0.0
* S P 9	3 a	8	Ex 2	a 3-5-1	nu4	1384.69820	0.0	0.149E-04	2270.27698	885.74843	0.0
* S Q 14	12 a	14	Ex 1	a 14-1	nu4	c1385.28958	0.0	0.423E-04	2929.92175	1544.63569	0.0
* Q P 14	1 a	13	Ex 23	a 1-0	2nu2	1385.35540	0.0	0.669E-04	3435.67554	2050.32014	0.0
R P 11	7 a	10	Ex 6	a 9-1	nu4	1385.39980	10.1	0.876E-03	2509.43447	1124.03568	1.0
* S P 12	1 a	11	Ex 15	a 5-1	nu4	1385.65021	14.6	0.504E-03	2914.40214	1640.62438	0.0
P P 16	10 a	15	Ex 12	a 9-1	nu4	1385.91539	62.8	0.103E-03	3691.34633	2305.41552	1.0
* R P 12	5 a	11	Ex 11	a 6-1	nu4	1386.30382	12.1	0.300E-03	2830.40785	1444.10524	1.0
* P 11	0 a	10	Ex 10	a 2-0	2nu2	c1386.59687	0.0	0.171E-03	2685.38002	1298.72244	0.0
* S P 14	1 a	13	Ex 21	a 2-0	2nu2	c1386.82070	0.0	0.153E-04	3440.56595	2053.74288	0.0
* P 14	2 a	13	Ex 22	a 2-1	nu4	c1386.90182	0.0	0.111E-04	3426.94517	2040.04335	0.0
* S P 9	3 a	8	Ex 2	a 3-5-1	nu4	1387.33660	23.9	0.611E-03	2424.51303	856.17882	1.0
R P 11	7 a	10	Ex 10	a 8-1	nu4	1387.33970	11.7	0.860E-03	2559.63033	1137.23532	0.0
P P 16	11 a	15	Ex 11	a 10-1	nu4	1387.57661	0.0	0.153E-03	3619.74305	2332.12444	0.0
P P 16	9 a	15	Ex 7	a 8-1	nu4	1387.57896	0.0	0.156E-03	3529.06493	2331.48597	0.0
R P 12	4 a	11	Ex 12	a 5-1	nu4	c1387.60717	0.0	0.269E-03	2864.04712	1476.17634	0.0
* S P 15	1 a	14	Ex 23	a 1-1	nu4	1387.61682	4.6	0.680E-02	2928.51742	1546.68414	0.0
P P 16	15 a	14	Ex 1	a 14-1	nu4	1388.05517	5.7	0.676E-02	2929.07275	1541.86715	

PP 16 6 15 A2o 10 5 5-1 nu4 n1391.14326 0.0 0.796E-04 3916.99282 2525.84956 0.0  
SP 10 2 9 Ee 10 4-1 nu4 1391.23540 0.0 0.244E-03 2461.59358 1070.35781 1.0  
SQ 15 12 15 A2o 11 5-1 nu4 c1391.93721 0.0 0.298E-04 3231.01311 1839.07397 1.0  
P 12 4 11 Eo 13 5 1 nu4 1392.10375 21.3 0.226E-03 2067.93460 1475.93298 1.0  
Q 13 3 12 A2o 9 3 0 2nu2 c1392.50034 0.0 0.141E-03 3145.19056 1752.64820 1.0  
PP 15 13 14 Ee 4 5-12 nu4 1392.69694 -1.9 0.128E-02 3140.46198 1747.76485 1.0  
P 15 8 14 Eo 16 3-1 nu4 c1392.96624 0.0 0.308E-04 2921.41309 1528.43337 1.0  
Q 10 1 11 Eo 13 5 1 nu4 1393.26510 5.3 0.215E-03 908.57499 570.57499 1.0  
PP 12 3 9 A2o 7 4 1 nu4 1393.34880 13.2 0.498E-02 2894.11270 1505.76522 1.0  
PP 16 9 15 A2o 8 4-1 nu4 n1393.50023 0.0 0.170E-03 3765.28051 2371.78028 1.0  
P 15 8 14 Eo 4 5-12 nu4 1393.84225 -19.1 0.132E-02 3142.16832 1748.53216 1.0  
Q 11 7 10 Eo 5 4 1 nu4 1393.90155 14.6 0.474E-03 1124.56715 1.0  
PP 11 6 10 A2o 4 7 1 nu4 1393.98220 6.9 0.186E-02 2564.74235 1170.76084 1.0  
Q 13 2 12 Ee 19 2 0 2nu2 n1394.16032 0.0 0.890E-04 3164.17331 1770.01299 0.0  
S 15 12 15 A2o 2 4-14 nu4 c1394.18011 0.0 0.303E-04 3232.63583 1838.45573 1.0  
SP 7 4 6 Ee 1 5 6-1 nu4 1394.20360 27.1 0.118E-03 1890.87703 496.67614 1.0  
PP 16 3 15 A2o 13 2-1 nu4 n1394.45111 0.0 0.581E-04 4011.44315 2616.99204 0.0  
PP 15 12 14 A2o 3 5-11 nu4 1394.72144 37.4 0.168E-02 3223.17343 1838.45573 1.0  
R 10 8 9 Ee 3 4 9 1 nu4 c1392.74010 0.0 0.102E-02 2251.44441 853.90676 1.0  
R 11 5 10 Eo 9 4 6 1 nu4 1394.89610 -29.3 0.534E-03 2605.41109 1210.51206 1.0  
Q 13 1 12 Eo 21 5 1 0 2nu2 n1394.95800 0.0 0.161E-03 3173.35413 1780.39613 1.0  
S 10 2 9 Eo 10 4 4-1 nu4 1395.28480 -4.4 0.225E-03 2465.23154 1069.94630 1.0  
P 12 1 11 Ee 17 4 1 nu4 n1395.47782 0.0 0.318E-04 2928.91119 1528.43337 1.0  
SP 7 4 6 Ee 1 5 6-1 nu4 1395.92410 -40.1 0.122E-03 1891.96319 496.03508 1.0  
PP 16 1 15 Ee 28 0 0 1 nu4 n1396.35686 0.0 0.275E-04 4040.28388 2643.27202 0.0  
PP 15 11 14 Ee 8 5-10 nu4 1396.49178 -267.3 0.580E-03 3311.48556 1920.96705 0.0  
P 15 12 12 Ee 13 5 1 nu4 1399.76092 -21.5 0.176E-03 1839.07397 1070.35781 1.0  
PP 16 2 15 Ee 28 5 1-1 nu4 n1396.51514 0.0 0.302E-04 4030.38380 2633.87226 0.0  
PP 16 8 15 Ee 17 4 7-1 nu4 n1396.51481 0.0 0.655E-04 3826.91528 2430.40047 0.0  
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PP 12 2 11 Ee 15 5 3 1 nu4 c1397.83011 0.0 0.199E-03 2916.08164 1518.25026 0.0  
P 15 10 14 Eo 10 9 9-1 nu4 1398.12038 69.1 0.417E-03 3393.66757 1975.55410 1.0  
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SP 13 2 12 Ee 20 4 1 nu4 n1398.43663 0.0 0.250E-04 3168.44962 1790.01299 0.0  
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PP 15 9 14 A2o 6 8-1 nu4 n1399.51438 34.4 0.626E-03 2402.43817 1362.49817 0.0  
PP 16 7 15 Ee 18 6 6-1 nu4 n1399.53623 0.0 0.503E-04 3081.31502 2481.78779 0.0  
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PP 15 10 14 Ee 10 5 1 nu4 1401.45150 -18.2 0.599E-03 2442.59095 1242.59095 1.0  
PP 15 7 14 Ee 10 4 9-1 nu4 1401.55502 -24.3 0.449E-03 3397.53433 1995.97688 1.0  
PP 15 7 14 Ee 16 6 9-1 nu4 1401.69594 -53.9 0.196E-03 3575.53753 2173.83620 1.0  
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P 12 1 11 Ee 18 4 1 nu4 n1402.99757 0.0 0.110E-04 3931.43094 1528.43337 1.0  
PP 15 9 14 A2o 7 4 8-1 nu4 1404.04994 35.1 0.678E-03 3466.84332 2062.79689 1.0  
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P 13 2 12 Eo 23 1 0 1 2nu2 n1405.60446 0.0 0.143E-04 3175.35413 1769.74967 0.0  
P 12 2 11 Ee 17 4 1 nu4 n1405.66093 0.0 0.115E-03 2923.91119 1518.25026 0.0  
T 7 1 6 Ee 3 4 0 2nu2 c1405.77560 0.0 0.136E-04 3456.53845 550.75859 0.0  
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P 15 1 14 Ee 26 0 1 nu4 n1405.97981 0.0 0.107E-03 3744.08269 2338.10888 0.0  
Q 12 1 11 Ee 19 5 1 0 2nu2 c1405.98968 0.0 0.256E-03 3494.69514 1528.73467 0.0  
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P 15 2 14 Ee 26 3 1-1 nu4 n1406.18138 0.0 0.119E-03 3734.11965 2327.93827 0.0  
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PP 14 13 13 Ee 2 5-12 nu4 1406.22035 -11.1 0.492E-02 2859.03109 1452.80963 1.0  
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P 15 7 14 Ee 16 6 5-1 nu4 n1409.10376 0.0 0.208E-03 3983.21189 2174.10813 0.0  
P 15 12 13 Ee 13 1-1 nu4 1409.15313 0.0 0.599E-02 2954.53131 1545.38132 1.0  
PP 15 4 14 Ee 24 5 3-1 nu4 n1409.33921 0.0 0.989E-04 3696.46774 2287.12853 0.0  
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PP 14 11 13 Ee 6 10-1 nu4 n1409.57220 0.0 0.489E-04 2704.76900 1295.39577 0.0  
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PP 14 11 13 Ee 27 4 1 nu4 n1410.95130 0.0 0.105E-04 3748.44999 2338.10888 1.0  
PP 14 11 13 Ee 7 2-1 nu4 1411.34396 -2.5 0.228E-02 4004.11524 1628.76733 1.0  
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PP 15 6 14 A2o 10 5-1 nu4 n1411.78551 -98.4 0.514E-03 3610.94843 2219.89488 1.0  
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PP 16 3 15 A2o 14 4 1 nu4 n1411.87161 0.0 0.591E-04 4029.21127 2617.33966 0.0  
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P 15 5 14 Ee 20 4 1 nu4 n1412.41800 0.0 0.105E-03 3669.02583 2256.60793 0.0  
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R 14 11 13 Ee 7 1 1 nu4 1412.59120 5.7 0.103E-02 2679.73508 1266.73735 1.0  
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P 14 11 13 Ee 18 4 1 nu4 n1413.18668 0.0 0.280E-04 2931.43094 1518.25026 0.0  
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P 14 7 13 Ee 14 6 6-1 nu4 1413.70530 2.2 0.710E-03 3297.69910 1883.99402 1.0  
P 14 11 13 Ee 18 5 5-1 nu4 1414.18480 -25.8 0.117E-02 3343.50878 1929.32140 1.0  
P 14 5 13 Ee 18 4 4-1 nu4 1414.31933 -126.4 0.487E-03 3181.38612 1967.47665 1.0  
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R 10 1 9 Ee 7 6 1 nu4 1416.67610 1.0 0.213E-02 3411.44913 994.77793 0.0  
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SP 7 3 6 A2o 2 5-1 nu4 1417.48470 1.8 0.745E-03 3199.10645 1521.62193 0.0  
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P 14 3 13 A2o 12 4 1 nu4 n1417.55024 0.0 0.282E-04 3416.73063 1998.80673 0.0  
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R 10 7 8 Ee 24 4 1 nu4 n1418.42627 0.0 0.119E-03 3705.70095 2287.33278 0.0  
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\* P P 13 3 s 12 A2e 11 s 2-1 nu4 1428.81261 21.5 0.243E-02 1172.43100 1522.43100 1.0  
\* P P 10 4 a 9 Ee 9 s \*\* \*\* 1428.88595 17.2 0.559E-03 2456.41722 1027.35549 1.0  
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\* P P 13 10 a 13 Ee 6 s 4-1 nu4 1429.03880 14.7 0.132E-02 2481.14373 1052.10640 1.0  
\* P P 13 8 a 12 Ee 11 s 7-1 nu4 1429.24610 0.3 0.116E-02 1559.77752 1284.96524 1.0  
\* Q P 9 4 a 8 Ee 6 s 4-0 2nu2 1429.26610 37.1 0.104E-02 2260.72040 831.45801 0.0  
\* Q P 11 2 a 10 Ee 16 s 2-1 nu4 1429.54272 62.3 0.306E-04 2714.50173 1284.96524 1.0  
\* S Q 13 10 a 13 Ee 10 s 3-1 nu4 1429.61124 0.0 0.352E-03 3469.65459 2040.04335 0.0  
\* S P 9 1 a 8 Ee 10 s 3-1 nu4 1429.74830 1.2 0.502E-03 884.91598 1050.22014 0.0  
\* P P 14 1 a 13 Ee 25 s \*\* \*\* n1430.26624 0.0 0.373E-03 3480.58638 2050.74288 1.0  
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\* S Q 13 10 a 13 Ee 3 s12-1 nu4 1430.64300 0.0 0.866E-04 2860.55147 1429.91057 1.0  
\* P P 13 7 a 12 Ee 12 a 6-1 nu4 1430.80830 58.8 0.251E-02 3043.45519 1612.65277 1.0  
\* O P 11 2 s 10 Ee 16 a 0-1 nu4 c1431.25190 0.0 0.209E-04 2715.85766 1284.60633 0.0  
\* Q P 8 6 a 7 A2e 1 s 6-0 2nu2 c1431.96940 0.0 0.442E-04 2013.44473 581.47075 0.0  
\* S P 6 3 a 5 A2o 1 s 5-1 nu4 1432.00460 13.3 0.302E-03 1816.02272 381.97745 1.0  
\* T P 7 0 a 6 Ee 2 s 3-0 2nu2 c1432.13133 0.0 0.135E-03 1986.52632 554.39306 0.0  
\* R P 9 5 a 8 Ee 5 s 6-1 nu4 1432.15650 10.2 0.421E-02 2230.52999 798.37451 1.0  
\* S P 10 0 a 9 A2e 8 s 2-1 nu4 1432.15680 77.7 0.186E-02 2056.73023 1084.58120 1.0  
\* P P 13 6 a 12 A2e 7 s 5-1 nu4 1432.16612 -117.8 0.415E-02 3010.60455 1658.42705 0.0  
\* P P 13 4 a 12 Ee 18 s \*\* \*\* n1432.63559 0.0 0.513E-03 3160.98117 1728.34758 1.0  
\* P P 10 3 a 9 A2o 6 s \*\* \*\* 1433.03110 0.6 0.529E-03 2485.58087 1052.54983 1.0  
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\* P P 10 9 a 9 Ee 12 s 3-1 nu4 1433.31660 -5.6 0.855E-03 2503.26346 1069.94630 1.0  
\* P P 13 5 a 12 Ee 16 a 4-1 nu4 1433.55330 18.4 0.171E-02 3110.50935 1696.95789 1.0  
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\* P P 11 6 a 11 A2o 3 s 9-0 2nu2 1434.07702 -36.4 0.277E-04 2604.84150 1070.76084 0.0  
\* Q P 9 4 a 8 Ee 13 s \*\* \*\* 1434.32968 18.2 0.296E-02 2439.65843 1070.76084 0.0  
\* P P 10 2 a 9 Ee 13 s \*\* \*\* c1435.68056 0.0 0.705E-04 2506.03598 1070.35781 0.0  
\* O P 13 4 a 12 Ee 19 s 2-0 2nu2 n1435.92573 0.0 0.389E-03 3164.17331 1728.34758 1.0  
\* R P 10 1 a 8 Ee 5 s 4-1 nu4 1436.23890 -9.4 0.710E-03 1976.66152 840.42168 1.0  
\* R F 10 7 a 9 Ee 14 s 2-1 nu4 c1436.26704 0.0 0.254E-03 2516.62476 1080.62686 1.0  
\* S Q 14 10 a 14 Ee 4 s12-1 nu4 c1436.31575 0.0 0.455E-04 3140.46198 1704.14728 0.0  
\* P P 12 12 a 11 A2o 1 s11-1 nu4 1436.51962 34.3 0.101E-03 2448.52257 1012.00638 1.0  
\* N P 9 10 a 10 A2e 1 s 10-0 2nu2 1436.51962 5.2 0.201E-02 2936.91815 1500.40405 0.0  
\* P P 12 12 a 11 A2e 1 s11-1 nu4 1436.69114 -30.6 0.714E-01 2449.74880 1013.05545 0.0  
\* R P 9 5 a 8 Ee 6 a 6-1 nu4 1437.10220 -17.5 0.289E-02 2236.03878 798.94383 1.0  
\* P P 12 12 a 11 A2o 12 a 2-1 nu4 1437.14543 40.9 0.294E-02 3189.79443 1658.44820 1.0  
\* P P 12 1 s 11 Ee 19 s \*\* \*\* n1437.51295 0.0 0.130E-02 2955.94632 1528.43337 0.0  
\* P P 12 11 a 11 Ee 3 s10-1 nu4 1437.67980 -6.2 0.237E-01 2535.11748 1097.43706 1.0  
\* Q P 9 8 a 8 Ee 9 s 2-0 2nu2 1438.15460 27.5 0.148E-02 2312.76929 874.61644 1.0  
\* P P 12 11 a 10 Ee 3 s10-1 nu4 1438.26704 -5.7 0.240E-01 2598.29418 1097.43706 1.0  
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\* Q P 8 5 a 7 Ee 4 s 5-0 2nu2 1438.38766 -50.9 0.158E-03 2060.08568 621.69293 1.0  
\* S P 7 2 a 6 Ee 5 s 4-1 nu4 1438.46820 355.8 0.204E-02 2696.78549 1528.43337 0.0  
\* P P 12 2 a 11 Ee 20 s 2-1 nu4 1438.47600 36.5 0.402E-02 2956.41333 1517.94098 1.0  
\* P P 10 10 a 9 Ee 13 s 1-0 2nu2 c1438.49966 0.0 0.138E-03 3088.44530 1069.94630 1.0  
\* P P 12 10 a 11 Ee 4 a 9-1 nu4 1438.56787 -20.3 0.184E-01 2611.17796 1174.60806 1.0  
\* P P 12 4 a 11 Ee 15 s 3-1 nu4 1438.56810 -10.6 0.412E-02 2914.40214 1475.83298 1.0  
\* S P 13 2 a 10 Ee 22 s \*\* \*\* n1438.59093 0.0 0.107E-02 3208.60392 1770.01299 0.0  
\* S Q 14 10 a 14 Ee 4 a12-1 nu4 1438.72814 -21.9 0.458E-04 3142.36832 1703.63799 1.0  
\* P P 12 12 a 11 A2e 12 a 2-1 nu4 1438.90710 0.0 0.126E-02 2912.46317 1080.39613 0.0  
\* P P 12 9 a 11 A2e 3 s 8-1 nu4 1439.19203 -29.3 0.237E-01 2682.96210 1243.75714 1.0  
\* P P 12 3 s 11 A2e 10 s 4-1 nu4 1439.24350 4.1 0.487E-02 3383.34833 1444.10524 1.0  
\* R P 12 3 s 11 A2e 10 s 2-1 nu4 1439.28407 -40.2 0.643E-02 3929.69214 1500.40405 1.0  
\* R P 9 4 a 8 Ee 7 s 5-1 nu4 1439.30020 -3.9 0.602E-02 2880.77963 1080.39613 0.0  
\* P P 12 8 a 11 Ee 8 s 7-1 nu4 1439.56305 -21.9 0.893E-02 2745.69261 1305.12737 1.0  
\* P P 12 6 a 11 A2o 6 s 5-1 nu4 1439.57131 -28.2 0.198E-03 2735.11953 1295.54540 1.0  
\* P P 12 6 a 11 A2o 6 s 5-1 nu4 1439.58267 1.9 0.115E-01 2404.17618 1051.15377 1.0  
\* P P 12 10 a 11 Ee 4 a 9-1 nu4 1439.64771 17.1 0.169E-01 2614.96760 1175.32160 1.0  
\* P P 12 7 a 11 Ee 10 s 6-1 nu4 1439.69000 -8.5 0.702E-02 3158.87122 1658.42705 1.0  
\* P P 13 4 a 12 Ee 20 s \*\* \*\* n1440.01540 40.9 0.382E-03 3448.52257 1080.51126 1.0  
\* O P 14 5 a 13 Ee 19 a 3-1 nu4 1440.10204 0.0 0.739E-03 3168.44962 1728.34758 1.0  
\* O P 14 5 a 13 Ee 20 s 3-1 nu4 1440.19293 -106.7 0.691E-04 3407.68025 1967.47665 1.0  
\* P P 14 5 a 13 Ee 19 s 3-1 nu4 1440.35494 35.3 0.971E-04 3408.09388 1967.47427 1.0  
\* S P 8 1 a 7 Ee 8 s 3-1 nu4 1440.64360 -2.3 0.848E-01 2149.39043 708.74660 1.0  
\* Q P 9 1 a 8 Ee 11 s 1-0 2nu2 1440.66100 47.8 0.146E-02 2326.02586 885.36964 1.0  
\* P P 12 9 a 11 A2o 4 a 8-1 nu4 1440.86419 23.7 0.248E-01 2685.23360 1244.37178 1.0  
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\* S Q 11 9 a 11 A2e 1 a11-1 nu4 1441.91930 -10.8 0.392E-03 2449.74880 1007.80842 0.0  
\* P P 12 8 a 11 Ee 9 a 7-1 nu4 1441.95538 19.2 0.950E-02 2477.60228 1305.64882 1.0  
\* S P 9 1 a 8 Ee 11 a 3-1 nu4 c1441.97089 0.0 0.118E-03 2326.88564 884.91598 0.0  
\* R P 8 1 a 7 A2e 2 a 7-1 nu4 1442.03601 0.0 0.482E-04 3660.92263 2218.65547 0.0  
\* P P 12 8 a 11 A2e 2 a 7-1 nu4 1442.33228 23.3 0.772E-02 3023.80070 581.47075 1.0  
\* P P 12 7 a 11 Ee 9 a 6-1 nu4 1442.93674 -35.0 0.754E-02 2802.26909 1359.32885 1.0  
\* S P 8 1 a 7 Ee 8 s 3-1 nu4 1443.73763 -2.0 0.243E-02 2275.19451 831.45801 1.0  
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\* P P 12 6 a 11 A2e 6 a 5-1 nu4 1443.90516 -16.5 0.125E-01 2849.47064 1405.56243 1.0  
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\* S Q 11 9 a 11 A2e 1 a11-1 nu4 1444.00314 -23.2 0.605E-03 2152.12347 708.21848 1.0  
\* S Q 15 10 a 15 Ee 6 s12-1 nu4 c1444.55908 0.0 0.185E-04 3480.52761 1995.97688 0.0  
\* P P 12 5 a 11 Ee 14 a 4-1 nu4 1444.81300 -16.1 0.542E-02 2889.29120 1444.47659 1.0  
\* P P 12 4 a 11 Ee 16 s 3-1 nu4 1445.22347 -112.8 0.381E-02 2921.41309 1476.17634 1.0  
\* R P 9 1 a 8 Ee 10 s 3-1 nu4 1445.47282 -1.9 0.124E-04 3103.90066 1658.42705 0.0  
\* Q P 10 2 a 9 Ee 14 s 2-1 nu4 c1446.51997 0.0 0.320E-04 2516.87476 1070.35781 0.0  
\* Q Q 12 9 a 12 A2o 1 s11-1 nu4 c1446.66946 0.0 0.369E-03 2691.04234 1244.37178 1.0  
\* T P 12 8 a 7 Ee 10 s10-0 2nu2 n1447.12763 0.0 0.335E-04 2806.45698 1359.12895 1.0  
\* S Q 15 10 a 15 Ee 6 a12-1 nu4 c1447.42255 0.0 0.185E-04 3442.98424 1995.55410 0.0  
\* P P 12 2 a 11 Ee 19 s \*\* \*\* n1447.69506 0.0 0.282E-02 3965.96432 1518.25026 0.0  
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\* P P 12 8 s 7 Ee 3 s 6-1 nu4 1447.90820 13.8 0.623E-02 2068.97237 621.65555 1.0  
\* P P 10 2 s 9 Ee 14 s \*\* \*\* c1448.05623 0.0 0.118E-04 2517.99678 1069.94630 0.0  
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\* O P 11 3 s 10 A2e 8 s 1-1 nu4 c1448.36190 18.8 0.900E-02 2715.30247 1266.91735 1.0  
\* P P 12 1 a 11 Ee 21 s \*\* \*\* n1448.55759 0.0 0.381E-02 2977.29226 1528.73467 0.0  
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\* R P 12 0 a 11 A2e 12 a 1-1 nu4 1448.74404 120.6 0.750E-02 2980.96435 1532.22547 1.0  
\* S Q 12 9 a 12 A2e 2 a11-1 nu4 1448.75030 0.0 0.375E-03 3243.76714 1658.42705 1.0  
\* R P 9 3 a 8 A2o 5 a 4-1 nu4 1448.78800 14.7 0.328E-02 2305.44496 856.65843 1.0  
\* Q P 8 3 a 7 A2o 3 s 3-0 2nu2 1448.89388 7.7 0.210E-02 2128.72982 679.83671 1.0

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\* Q P 7 6 a 6 A2e 1 s 6-0 2nu2 1449.21660 4.5 0.417E-02 1872.43896 423.22281 1.0  
\* R P 11 0 a 10 Ee 9 s 1-1 nu4 1449.49488 -6.1 0.206E-01 2649.71993 1298.72244 1.0  
\* U P 11 2 a 10 Ee 18 a 0-1 nu4 n1449.71350 0.0 0.201E-04 3219.46317 1769.74957 0.0  
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\* R P 9 2 s 8 Ee 10 s 3-1 nu4 1450.17700 -33.6 0.248E-02 2324.33065 874.15029 1.0  
\* Q P 9 5 a 9 Ee 3 a 9-1 nu4 c1450.27234 0.0 0.181E-04 2248.64641 798.37451 0.0  
\* Q P 11 2 a 10 Ee 18 a 0-1 nu4 1450.51272 -4.7 0.105E-01 2735.11953 1298.72244 1.0  
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\* R P 8 5 a 7 Ee 5 a 6-1 nu4 1451.52039 4.8 0.589E-02 2073.21284 621.69293 1.0  
\* Q P 11 4 a 10 Ee 13 s 3-1 nu4 1451.76229 15.3 0.114E-01 2693.86729 1242.10653 1.0  
\* Q P 8 2 a 7 Ee 16 s 1-1 nu4 1452.20950 -30.1 0.496E-03 2326.02586 874.15029 1.0  
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\* P P 11 5 a 10 Ee 12 s 4-1 nu4 1452.66831 2.5 0.131E-01 2312.46800 860.00074 1.0  
\* S P 6 2 a 5 Ee 3 a 4-1 nu4 1452.70460 -5.9 0.593E-03 1854.98294 402.27775 1.0  
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\* P P 11 6 a 10 Ee 2 s 8-1 nu4 1453.74919 -22.9 0.660E-01 2461.55485 1007.80842 1.0  
\* P P 11 10 a 10 Ee 2 s 9-1 nu4 1453.34070 4.5 0.469E-01 2331.29848 937.95823 1.0  
\* R P 9 1 s 8 Ee 12 s 2-1 nu4 1453.55650 -5.6 0.934E-03 2338.47264 884.91598 1.0  
\* P P 11 7 a 10 Ee 8 s 6-1 nu4 1453.72490 -20.8 0.193E-01 2577.76266 1124.03568 1.0  
\* P P 11 9 a 10 A2e 2 s11-1 nu4 1453.81440 -16.6 0.217E-03 2952.76265 1498.85659 1.0  
\* S Q 13 9 a 13 A2o 2 s11-1 nu4 1453.81440 -16.6 0.217E-03 2952.76265 1498.85659 1.0  
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\* P P 11 10 a 10 Ee 3 s 9-1 nu4 1453.92337 -7.6 0.475E-01 2392.71235 938.78822 1.0  
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\* O P 12 4 a 11 Ee 17 a 2-1 nu4 1454.24280 1.4 0.424E-03 2930.07564 1475.83298 1.0  
\* R P 8 5 a 6 Ee 18 s 2-1 nu4 c1454.26544 0.0 0.134E-03 2339.63141 885.36964 1.0  
\* Q P 7 1 a 6 Ee 2 s 5-0 2nu2 c1454.59310 0.0 0.263E-02 2918.29386 1498.85659 1.0  
\* Q P 8 5 a 6 Ee 9 s 1-0 2nu2 1454.64340 1.1 0.141E-02 2163.38989 708.74660 1.0  
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\* R P 8 4 a 7 Ee 10 s 3-1 nu4 1455.50939 21.6 0.226E-01 2164.74052 708.74660 1.0  
\* P P 11 1 a 7 Ee 10 s 3-1 nu4 1455.50939 21.6 0.226E-01 2164.74052 708.74660 1.0  
\* S Q 13 9 a 13 A2e 3 a11-1 nu4 1456.06952 15.3 0.206E-01 2580.63514 1124.03568 1.0  
\* S P 7 1 a 6 Ee 6 s 3-1 nu4 1456.31320 -1.8 0.112E-02 2007.63372 554.39306 1.0  
\* O P 13 5 a 12 Ee 17 a 3-1 nu4 1456.33020 -0.9 0.156E-03 3152.97220 1696.64811 1.0  
\* O P 13 5 a 12 Ee 17 a 3-1 nu4 1456.33020 -0.9 0.156E-03 3152.97220 1696.64811 1.0  
\* P P 11 5 a 10 Ee 12 a 4-1 nu4 1456.39261 -18.8 0.143E-01 2667.43865 1120.51206 1.0  
\* P P 11 4 a 10 Ee 14 a 3-1 nu4 1457.19061 -45.8 0.120E-01 2699.70024 1242.50505 1.0  
\* R P 7 1 a 6 Ee 6 s 2-0 2nu2 c1457.28767 0.0 0.648E-04 2008.05676 554.39306 1.0  
\* O P 13 3 a 12 A2o 11 s 1-1 nu4 1457.75450 72.2 0.377E-04 3210.39548 1752.64820 1.0  
\* O P 14 6 a 13 A2o 9 a 4-1 nu4 1457.78152 -6.6 0.114E-03 3387.13028 1929.32140 1.0  
\* O P 14 6 a 13 A2o 9 a 2-1 nu4 1458.10272 4.2 0.237E-01 2725.39127 1267.28897 1.0  
\* O P 14 6 a 13 A2o 9 a 4-1 nu4 1458.25864 47.8 0.130E-03 3158.87122 1658.42705 1.0  
\* P P 11 2 a 10 Ee 17 a 1-1 nu4 1458.49180 0.0 0.111E-01 2743.45226 1298.72244 1.0  
\* S Q 10 8 a 10 Ee 2 s10-1 nu4 1458.74590 46.6 0.349E-03 2312.64800 853.90676 1.0  
\* P P 11 7 a 10 Ee 19 s \*\* \*\* n1458.77790 -37.1 0.201E-04 3632.60272 2173.83620 0.0  
\* S P 8 1 a 7 Ee 9 a 3-1 nu4 1458.85505 -11.2 0.151E-03 2167.09465 708.23848 1.0  
\* N P 12 4 a 11 Ee 19 s 1-0 2nu2 c1458.89137 0.0 0.885E-04 2394.69514 1475.83298 1.0  
\* R P 8 7 a 6 Ee 7 s 3-1 nu4 1458.95176 6.9 0.113E-02 2409.71830 580.29849 1.0  
\* S P 7 1 a 6 Ee 7 s 3-1 nu4 1458.96040 6.9 0.113E-02 2409.71830 580.29849 1.0  
\* T Q 10 5 s 10 Ee 5 s 8-0 2nu2 c1458.99176 0.0 0.280E-04 2653.76820 994.77313 1.0  
\* P P 12 2 a 14 Ee 19 s 5-1 nu4 n1459.34958 0.0 0.219E-04 3633.45771 2174.10813 1.0  
\* P P 12 2 a 14 Ee 19 s 5-1 nu4 n1459.34958 0.0 0.219E-04 3633.45771 2174.10813 1.0  
\* Q P 7 1 a 6 Ee 15 a 1-1 nu4 1459.56500 -66.5 0.752E-04 2540.19551 1080.6886 1.0  
\* Q P 7 4 a 6 Ee 3 a 4-0 2nu2 c1459.858

* OP	13	7	#	12	Ex	14	4	5	1	nu4	c1490.07632	0.0	0.154E-03	3102.33607	1612.26340	0.0	
* RP	6	1	a	5	E	2	5	1	1	nu4	c1499.18469	22.3	0.114E-01	1844.46695	358.28449	0.0	
* RP	5	1	a	5	E	3	6	2	0	2nu2	c1490.18481	10.1	0.473E-04	1784.15206	293.96826	2.0	
* OP	14	1	a	5	E	6	4	3	1	nu4	c1490.30170	0.0	0.399E-04	1803.53973	413.23778	0.0	
* OP	14	5	a	13	E	15	6	1	1	nu4	n1501.50574	-2.0	0.678E-04	3321.91900	184.19000	0.0	
* OP	14	6	a	13	E	20	14	6	0	1	nu4	c1499.60599	-2.0	0.231E-03	3696.78549	1476.17634	0.0
* OP	15	9	a	14	A2#	7	7	1	1	nu4	c1490.66600	0.0	0.536E-04	3553.07739	2062.18317	0.0	
* OP	11	5	a	10	E	14	4	3	1	nu4	c1490.71350	46.1	0.841E-03	2701.22095	1210.52106	1.0	
* OP	11	5	a	10	E	14	4	3	1	nu4	c1490.93470	46.1	0.841E-03	2701.22095	1210.52106	1.0	
* SQ	11	5	a	10	E	4	4	9	1	nu4	c1490.93394	0.0	0.503E-03	2614.96760	1124.03568	0.0	
* PP	8	2	a	7	E	10	12	5	1	1	nu4	c1491.30286	-12.6	0.100E+00	1828.69945	697.39533	0.0
* TQ	10	4	a	10	E	5	7	0	2	nu2	c1491.39051	0.0	0.579E-04	2518.47013	1027.07848	0.0	
* TQ	10	4	a	10	E	23	12	1	0	1	nu2	c1491.10718	0.0	0.121E-03	2128.19117	1027.07848	0.0
* OP	12	6	a	11	A2#	8	4	1	1	nu4	c1491.59610	56.3	0.810E-03	2897.15290	1495.56243	1.0	
* SP	5	1	a	4	E	4	4	3	1	nu4	c1491.71730	-13.3	0.973E-03	1785.74149	293.96826	2.0	
* TQ	7	3	a	7	A2#	1	6	0	2	nu2	c1491.81662	-61.8	0.394E-04	2013.44473	521.62193	1.0	
* OP	13	7	a	12	E	15	10	1	0	1	nu4	c1492.06290	-0.4	0.182E-03	3104.71571	1612.65277	1.0
* SP	6	1	a	5	A2#	4	2	2	1	nu4	c1492.19280	1.7	0.716E-02	1909.08037	416.88774	0.0	
* OP	15	9	a	14	A2#	8	7	1	1	nu4	n1492.19866	0.0	0.584E-04	3554.99555	2062.79686	0.0	
* OP	15	9	a	14	A2#	17	16	1	1	nu4	c1492.24010	-37.7	0.716E-02	3554.99555	2062.79686	0.0	
* OP	9	2	a	8	E	15	0	1	0	1	nu4	c1492.79690	-42.0	0.668E-03	2366.95139	874.15029	0.0
* OP	9	2	a	8	E	6	4	3	1	nu4	c1493.07845	-11.3	0.109E-03	1905.70489	412.62430	0.0	
* UQ	12	4	a	12	E	10	8	1	1	nu4	c1493.38155	0.0	0.104E-03	2176.19608	1027.07848	0.0	
* OP	13	7	a	12	E	10	8	1	1	nu4	c1493.38663	0.0	0.118E-04	2324.33065	830.94019	0.0	
* PQ	8	3	a	7	A2#	6	2	2	1	nu4	c1493.52698	38.9	0.212E+00	2172.19059	679.28876	1.0	
* SQ	15	8	a	15	E	10	10	1	0	1	nu4	c1493.69612	0.0	0.168E-04	3165.80435	2122.14027	0.0
* OP	13	7	a	12	E	10	8	1	1	nu4	c1493.69612	0.0	0.168E-04	3165.80435	2122.14027	0.0	
* OP	13	7	a	12	E	1	1	4	0			4.5	0.557E-02	1733.33458	239.40823	1.0	
* PP	8	1	a	7	E	10	13	0	1	1	nu4	c1494.24219	-2.2	0.108E+00	2202.98901	708.74660	1.0
* P	11	5	a	10	E	15	**	**	**	**	c1494.68497	-30.4	0.387E-03	2704.76500	1210.08099	0.0	
* OP	13	7	a	12	E	23	12	1	0	1	nu4	c1494.24219	-30.4	0.387E-03	2704.76500	1210.08099	0.0
* NP	9	4	a	8	E	11	1	0	2	nu2	c1495.09413	84.6	0.233E-03	2326.02586	830.94019	1.0	
* OP	7	1	a	6	E	10	10	1	1	1	nu4	c1495.13220	-8.9	0.251E-02	2046.45343	551.32034	0.0
* RP	6	2	a	7	E	11	1	1	1	nu4	c1495.24290	0.6	0.111E+00	2133.39455	609.91103	0.0	
* RP	6	2	a	7	E	8	3	1	1	nu4	c1495.52002	0.0	0.200E+00	2342.03043	533.87060	0.0	
* TQ	8	3	a	7	A2#	2	2	4	1	nu4	c1495.72144	1.2	0.425E-01	1879.03974	383.31842	1.0	
* TQ	8	3	a	7	A2#	2	6	0	2	nu2	c1495.87407	0.0	0.255E-04	2175.16330	679.28786	0.0	
* OP	8	3	a	7	A2#	7	7	2	0	nu2	c1495.93029	0.0	0.141E-04	2150.37824	554.45027	0.0	
* PP	8	2	a	7	A2#	5	5	2	1	nu4	c1496.13735	31.4	0.219E+00	2176.00752	679.03671	1.0	
* PP	8	2	a	7	A2#	5	5	1	0	2	nu2	c1497.13764	0.0	0.103E-03	1898.84702	401.64783	0.0
* PP	8	2	a	7	A2#	7	4	4	0	1	nu4	c1497.13764	0.0	0.103E-03	1898.84702	401.64783	0.0
* RP	6	5	a	5	A2#	3	4	1	1	nu4	c1497.51514	7.7	0.410E-01	1881.49182	383.97745	1.0	
* RP	6	5	a	5	A2#	1	3	0	2	nu2	c1497.63280	-25.6	0.629E-02	1762.86198	265.22662	1.0	
* RP	6	5	a	5	A2#	8	4	3	1	nu4	c1497.67493	17.3	0.130E+00	2152.12347	554.45027	0.0	
* SQ	12	4	a	12	E	11	8	1	1	nu4	c1497.79208	0.0	0.106E-03	2176.19608	1027.07848	0.0	
* UQ	7	3	a	7	A2#	1	6	9	1	nu4	c1497.78308	4.6	0.271E-03	2856.63584	1358.87122	1.0	
* SQ	12	4	a	12	E	2	1	1	1	nu4	c1498.85140	-1.8	0.361E+00	2079.59121	580.77963	1.0	
* PP	8	5	a	7	E	7	7	4	1	nu4	c1498.84412	15.6	0.153E+00	2120.53549	621.69293	0.0	
* OP	7	1	a	6	E	10	1	1	1	nu4	c1499.11080	25.6	0.279E-02	2049.86693	550.75859	1.0	
* OP	7	1	a	6	E	10	1	0	2	nu2	c1499.11080	25.6	0.279E-02	2049.86693	550.75859	1.0	
* OP	8	2	a	7	E	12	0	1	0	1	nu4	c1499.58040	31.2	0.156E-02	2197.49789	697.51701	1.0
* NP	12	6	a	11	A2#	8	3	0	2	nu2	n1499.73391	0.0	0.164E-03	2904.92768	1405.15377	0.0	
* PP	8	6	a	7	A2#	3	5	1	1	nu4	c1499.80273	4.2	0.374E+00	2081.27306	581.47075	0.0	
* NP	12	6	a	11	A2#	22	22	2	0	1	nu4	c1499.81937	0.0	0.116E-03	3104.71571	1612.65277	1.0
* PP	8	7	a	7	E	2	6	1	1	nu4	c1499.94360	3.9	0.236E+00	2032.83724	532.89403	1.0	
* NP	10	5	a	7	E	11	2	0	2	nu2	c1500.19990	-3.9	0.436E-03	2494.97342	994.77313	1.0	
* NP	10	5	a	7	E	3	6	1	0	1	nu4	c1500.51038	-44.1	0.131E-03	2028.20829	581.47075	0.0
* OP	7	1	a	6	E	3	2	0	2	nu2	c1500.53798	25.8	0.154E-02	2178.15206	283.61666	1.0	
* SQ	9	6	a	9	A2#	1	8	1	1	nu4	c1500.62140	3.4	0.242E-02	2259.62339	759.00233	1.0	
* PP	8	7	a	7	E	2	7	1	1	nu4	c1500.73340	35.4	0.320E+00	1977.99395	477.26409	0.0	
* PP	8	7	a	7	E	13	7	1	0	1	nu4	c1500.94197	-40.3	0.331E+00	2176.19608	1027.07848	0.0
* OP	7	2	a	6	E	9	9	2	1	nu4	n1501.21348	0.0	0.644E-04	3041.05933	539.84490	0.0	
* P	12	4	a	11	E	21	**	**	**	**	n1501.45928	0.0	0.404E-04	2977.29226	1475.83298	0.0	
* RP	6	2	a	7	E	6	3	1	1	nu4	n1501.89136	-5.4	0.287E-01	1903.53973	401.64783	0.0	
* RP	6	2	a	7	E	13	9	1	1	nu4	c1501.37320	0.0	0.114E-03	2176.19608	1027.07848	0.0	
* UQ	7	3	a	7	A2#	2	7	1	1	nu4	c1502.18283	40.6	0.735E-04	2023.80070	521.62193	1.0	
* OP	10	3	a	9	A2#	9	1	1	1	nu4	c1502.23170	-81.5	0.109E-02	2554.34625	1052.10640	1.0	
* SQ	5	1	a	4	E	3	1	0	2	nu2	c1502.35355	-29.5	0.837E-03	1786.98498	293.96826	2.0	
* M	11	5	a	10	E	1	7	2	0	1	nu4	c1502.43505	0.0	0.149E-04	2182.27162	679.83671	0.0
* MP	11	4	a	10	E	18	0	1	1	nu4	c1502.48363	-75.6	0.926E-04	2744.99624	1242.50505	0.0	
* SQ	9	6	a	9	A2#	2	8	1	1	nu4	c1502.62490	-6.9	0.247E-02	2262.10085	758.38526	1.0	
* RP	6	2	a	7	E	13	9	1	1	nu4	c1502.75537	0.0	0.116E-03	3104.71571	1612.65277	1.0	
* RP	6	2	a	7	E	6	4	3	1	nu4	c1503.42603	-11.1	0.228E-01	1905.70489	402.27775	0.0	
* OP	11	6	a	10	A2#	6	4	1	1	nu4	c1503.55030	-39.4	0.933E-03	2674.31508	1170.76084	1.0	
* OP	11	6	a	10	A2#	11	0	1	0	1	nu4	c1504.02185	43.1	0.166E+00	2504.75613	550.75859	0.0
* OP	11	6	a	10	A2#	13	9	1	1	nu4	c1504.02185	43.1	0.166E+00	2504.75613	550.75859	0.0	
* OP	16	11	1	15	E	13	9	1	1	nu4	n1504.95011	0.0	0.123E-04	3736.70087	2231.75076	0.0	
* OP	12	7	#	11	E	12	5	5	1	nu4	c1505.17250	-34.0	0.330E-03	2864.04712	1358.87122	1.0	
* SQ	13	10	a	13	E	8	9	1	1	nu4	c1505.31550	-4.8	0.120E-03	3111.57938	1612.26340	0.0	
* NP	13	7	a	12	E	15	10	1	0	1	nu4	c1505.55421	0.0	0.179E-04	3111.77554	1612.26340	0.0
* OP	8	2	a	7	E	10	13	0	1	nu4	c1505.59330	0.0	0.122E-02	2202.98901	697.39533	0.0	
* OP	13	8	a	12	E	13	6	1	1	nu4	c1505.78760	-44.1	0.131E-03	2028.20829	581.47075	0.0	
* SQ	10	6	a	10	A2#	2	8	1	1	nu4	c1505.90280	-12.8	0.191E-02	2461.55485	955.50777	1.0	
* OP	9	3	a	8	A2#	7	7	1	1	nu4	c1506.56930	24.2	0.235E-02	2363.22501	856.68493	0.0	
* RP	6	1															

\* OP 12 7 a 11 Eo 13 s 5 1 nu4 1508 60720 14.5 0.459E-03 2667 93460 1359 32885 1.0  
\* P 12 7 a 11 Eo 12 s 2 1 nu4 1508 69560 43.8 0.207E-02 2033 33141 830 64019 1.0  
\* PP 7 3 a 6 A2e 4 s 2-1 nu4 1509 13794 13.1 0.363E-03 2030 37586 521 62193 1.0  
\* SP 4 1 a 3 Ee 2 s 3-1 nu4 1509 33860 -43.1 0.413E-03 1704 24922 194 90631 1.0  
\* SQ 14 7 a 14 Eo 10 s 9-1 nu4 c1509 35310 0.0 0.467E-03 1393 66757 184 32138 0.0  
\* P 14 7 a 14 Ee 10 a 1-1 nu4 1509 44805 28.5 0.189E-03 1540 85683 540 18906 0.0  
\* NP 8 4 a 7 Eo 9 s 1 0 2 nu2 c1509 52121 0.0 0.307E-03 2163 38989 653 87060 0.0  
\* SP 5 1 a 4 Ee 5 s 3 1 nu4 1510 39160 0.0 0.496E-04 1804 35963 293 96826 0.0  
\* PP 6 1 a 5 Ee 10 s 1-1 nu4 1511 18620 -10.9 0.235E-02 413 23778 0.0 0.357E-02  
\* P 11 9 a 9 Ee 11 s 1-1 nu4 1511 26550 26.5 0.105E-02 2506 03598 994 77713 1.0  
\* PP 7 4 a 6 A2o 4 a 2-1 nu4 1511 31250 18.8 0.408E-03 2033 53355 522 22293 1.0  
\* SP 5 0 a 4 A2o 3 s 2-1 nu4 1511 43970 -1.7 0.723E-02 1809 08163 297 64176 1.0  
\* P 11 6 a 6 Eo 6 s 3-1 nu4 1511 59851 -1.3 0.217E-03 2047 63372 496 03508 1.0  
\* SQ 11 6 a 11 A2o 3 s 8-1 nu4 1511 72300 -37.8 0.116E-02 2682 96210 1171 23532 1.0  
\* MP 12 5 a 11 Eo 20 s 1-1 nu4 1511 94296 62.2 0.298E-04 2956 41333 1444 47659 1.0  
\* P 13 5 a 12 Ee 22 s 1-1 nu4 1511 96211 0.0 0.106E-04 3208 60392 1696 64181 1.0  
\* UO 10 3 a 10 A2o 4 s 7 1 nu4 c1512 19264 0.0 0.591E-04 2714 74235 1052 54983 1.0  
\* P 11 4 a 10 Eo 19 s 1-1 nu4 c1512 21695 0.0 0.102E-03 2754 32701 1242 10653 1.0  
\* PP 7 4 a 6 Ee 7 s 3-1 nu4 1513 04370 15.4 0.231E-03 2059 71830 496 67614 1.0  
\* RP 5 3 a 4 A2e 1 s 4 1 nu4 1513 08203 -4.6 0.333E-01 1777 59911 264 51662 1.0  
\* P 11 5 a 4 Eo 13 s 1 0 2 nu2 c1513 17840 0.0 0.191E-04 2508 44530 995 26756 0.0  
\* SQ 14 7 a 14 Ee 10 s 9-1 nu4 c1513 53887 0.0 0.454E-04 1377 59403 1883 99402 0.0  
\* PP 7 5 a 6 Ee 5 s 4-1 nu4 1513 64795 -5.3 0.268E-04 1976 66152 463 01304 1.0  
\* TQ 5 2 a 5 Eo 1 s 5 0 2 nu2 c1514 01303 0.0 0.225E-04 1796 96739 282 93714 1.0  
\* P 5 2 a 5 Eo 3 s 1 0 2 nu2 c1514 04270 -42.0 0.903E-04 1796 98404 282 93714 1.0  
\* RP 5 3 a 4 A2o 2 s 4 1 nu4 1514 23200 14.6 0.368E-01 1779 45716 265 22662 1.0  
\* SP 5 7 a 7 Eo 2 s 7-1 nu4 1514 29000 30.6 0.135E-02 1977 99395 463 70701 1.0  
\* OP 7 2 a 6 Ee 11 s 0 1 nu4 1514 36060 61.5 0.297E-02 2054 77613 540 42168 1.0  
\* P 7 2 a 6 Ee 8 s 1-1 nu4 1514 36210 25.0 0.420E-03 1512 62413 1624 82413 1.0  
\* NP 9 5 a 8 Ee 9 s 2 0 2 nu2 c1514 39569 0.0 0.536E-03 2313 76929 798 37451 0.0  
\* SQ 11 6 a 11 A2o 4 a 8-1 nu4 1514 47690 41.4 0.115E-02 2695 23360 1170 76084 1.0  
\* PP 7 5 a 6 Eo 5 s 4-1 nu4 1514 60547 2.3 0.278E-03 1978 31225 463 70701 1.0  
\* UO 10 3 a 10 A2o 4 s 7 1 nu4 c1514 6205 0.0 0.741E-03 1170 76084 1170 76084 1.0  
\* P 9 3 a 9 A2e 3 s 7 1 nu4 c1514 94687 0.0 0.219E-03 2571 12655 856 17882 0.0  
\* MP 10 4 a 9 Ee 16 s 0 1 nu4 c1515 28134 0.0 0.205E-03 2342 81917 1027 55549 0.0  
\* P 10 4 a 9 Ee 11 s 1-1 nu4 1515 32434 2.6 0.688E-03 1937 78219 422 45811 1.0  
\* QP 4 3 a 3 A2o 1 s 3 0 2 nu2 c1515 46875 17.6 0.177E-01 1681 55488 166 08789 1.0  
\* PP 7 6 a 6 A2e 2 s 5-1 nu4 1515 88196 -16.8 0.699E-03 1939 10645 432 22281 1.0  
\* SQ 7 5 a 7 Ee 1 a 7-1 nu4 1516 07970 -42.7 0.140E-02 1979 09701 463 01304 1.0  
\* TQ 6 2 a 6 Eo 2 s 5 0 2 nu2 c1516 65310 69.7 0.370E-04 1918 23936 461 47883 1.0  
\* PP 7 7 a 6 Eo 1 a 6-1 nu4 1516 85205 -43.7 0.257E-04 1891 96319 375 10577 1.0  
\* TQ 13 4 a 13 Eo 12 s 7 0 2 nu2 c1517 08768 0.0 0.159E-04 3245 15807 1728 05529 0.0  
\* NP 12 3 a 12 Ee 7 s 1-1 nu4 1517 20772 0.0 0.176E-04 4022 48926 402 27775 0.0  
\* SQ 15 7 a 15 Eo 12 s 9-1 nu4 c1517 22278 0.0 0.157E-04 3691 32463 2174 10813 1.0  
\* UO 11 3 a 11 A2o 5 s 7 1 nu4 c1517 22467 0.0 0.477E-04 2784 51339 1267 28897 0.0  
\* NP 10 3 a 9 A2o 5 s 3 0 2 nu2 c1517 90300 7.6 0.131E-02 2473 00867 955 10643 1.0  
\* SQ 12 3 a 12 A2e 4 s 8-1 nu4 1518 08148 -24.4 0.573E-03 1923 64635 1405 56243 1.0  
\* OP 4 2 a 3 Ee 1 s 2 0 2 nu2 c1518 15564 -7.7 0.734E-02 1702 70943 184 55302 1.0  
\* SQ 8 5 a 8 Eo 3 s 7-1 nu4 1518 43440 10.4 0.134E-02 2140 12629 621 69293 1.0  
\* NP 12 3 a 12 Ee 11 s 4 0 2 nu2 c1518 64515 -12.9 0.106E-03 3158 87122 1158 87122 1.0  
\* OP 16 12 15 A2o 5 s 10 1 nu4 c1518 79622 0.0 0.314E-04 3669 04894 2150 27904 0.0  
\* OP 7 2 a 6 Eo 11 s 0 1 nu4 1519 29660 41.4 0.198E-02 2059 13736 539 84490 1.0  
\* QP 6 2 a 5 Eo 7 s 2 1 nu4 1519 33530 -11.7 0.276E-03 1920 98430 401 64783 1.0  
\* NP 12 3 a 12 Ee 11 s 4 0 2 nu2 c1519 45470 -7.1 0.164E-03 3182 97314 1158 87122 1.0  
\* PP 6 1 a 5 Ee 9 s 0 1 nu4 1519 66272 41.4 0.243E-03 1932 28288 412 62430 1.0  
\* OP 15 11 14 Ee 11 s 9 1 nu4 c1519 72159 0.0 0.405E-04 3440 88864 1920 96705 0.0  
\* NP 6 3 a 5 A2e 3 s 0 0 2 nu2 c1519 83500 -4.9 0.134E-02 1903 15391 383 31842 1.0  
\* OP 11 7 10 Ee 10 s 5 1 nu4 1519 92000 -26.9 0.591E-03 2643 95837 1124 03568 1.0  
\* NP 9 4 a 7 Eo 13 s 1-1 nu4 c1520 08248 0.0 0.124E-04 2351 02478 830 94019 1.0  
\* TQ 7 2 a 7 Eo 4 s 5 0 2 nu2 c1520 23736 0.0 0.206E-04 2560 08568 539 84490 1.0  
\* OP 14 10 a 13 Eo 10 s 8 1 nu4 1520 42450 -5.6 0.190E-02 2141 09061 821 09061 1.0  
\* QP 4 10 a 13 A2e 1 s 0 0 2 nu2 c1520 43804 0.0 0.957E-04 3224 06858 1703 63799 1.0  
\* P 4 2 a 4 A2e 1 s 0 0 2 nu2 c1520 44946 -18.9 0.103E-01 3171 74525 199 29390 1.0  
\* OP 12 2 a 4 Ee 11 s 6 1 nu4 c1520 74072 0.0 0.381E-03 2825 87540 1305 12737 1.0  
\* OP 13 9 12 A2e 5 s 7 1 nu4 1520 82440 25.1 0.408E-03 3019 16437 1498 34248 1.0  
\* RP 6 0 a 5 A2e 5 s 1 1 nu4 1521 25080 77.1 0.570E-03 1938 11083 146 88774 1.0  
\* OP 16 12 15 A2e 6 s 10 1 nu4 c1521 31880 0.0 0.356E-04 3672 10734 2150 78592 1.0  
\* SQ 12 6 a 12 A2e 5 s 8-1 nu4 1521 44140 26.1 0.565E-03 2926 59256 1405 15377 1.0  
\* TQ 10 3 a 10 A2e 4 s 6 0 2 nu2 c1521 71732 0.0 0.208E-03 2573 82086 1052 10640 0.0  
\* P 12 5 a 11 Ee 19 s 1-1 nu4 c1521 84108 0.0 0.229E-04 2956 94632 1444 10524 1.0  
\* SQ 12 3 a 12 A2e 6 s 7 1 nu4 1522 20059 0.0 0.309E-04 3022 97191 1404 76522 0.0  
\* OP 15 11 14 Eo 11 s 9 1 nu4 c1522 38115 0.0 0.468E-04 3443 86017 1921 47393 1.0  
\* PP 6 1 a 5 Eo 9 s 0 1 nu4 1522 38477 58.4 0.237E-03 1925 61671 413 23778 1.0  
\* SQ 15 7 a 15 Ee 12 s 9-1 nu4 c1522 45040 0.0 0.149E-04 3696 28852 2172 83630 1.0  
\* P 11 2 a 11 Eo 11 s 1 0 2 nu2 c1522 68025 0.0 0.131E-04 2966 78549 1444 10524 1.0  
\* PP 6 2 a 5 Eo 8 s 1-1 nu4 1522 77637 -8.7 0.255E-03 2424 42507 401 64783 1.0  
\* MP 13 6 a 12 A2e 11 s 2-1 nu4 c1522 85662 0.0 0.155E-04 3181 28151 1658 42705 0.0  
\* NP 13 8 a 12 Eo 14 s 5 0 2 nu2 c1522 92582 0.0 0.292E-04 3559 05488 1920 96705 1.0  
\* P 9 5 a 9 Eo 5 s 7 1 nu4 1523 12630 -15.6 0.170E-02 2322 26629 798 94883 1.0  
\* OP 14 10 a 13 Ee 12 s 8 1 nu4 1523 31830 -19.9 0.115E-03 3227 46757 1704 14728 1.0  
\* MP 10 4 a 9 Eo 17 s 0 1 nu4 c1523 71770 -92.9 0.223E-03 2550 80447 1027 07848 1.0  
\* P 13 9 12 A2e 6 s 7 1 nu4 1524 36205 -23.7 0.519E-03 1498 85659 1021 67191 1.0  
\* OP 7 3 a 6 A2e 5 s 1 1 nu4 1524 45691 -64.5 0.151E-01 2046 08529 521 62193 1.0  
\* MF 11 5 a 10 Eo 18 s 1-1 nu4 c1524 60628 0.0 0.698E-04 2735 11953 1210 51206 0.0  
\* TQ 8 2 a 8 Eo 5 s 5 0 2 nu2 c1524 68219 0.0 0.200E-04 3222 07895 697 39333 1.0  
\* OP 12 8 a 11 Ee 11 s 6 1 nu4 1524 75950 4.7 0.543E-03 2830 40785 1305 64882 1.0  
\* OP 8 4 a 7 Eo 10 s 2 1 nu4 1524 91920 -26.9 0.397E-02 2179 37216 654 45027 1.0  
\* RP 5 1 a 4 Ee 6 s 2 1 nu4 1524 95422 -24.9 0.409E-01 1818 92497 293 96826 1.0  
\* P 13 6 a 12 A2e 6 s 7 1 nu4 1524 96205 -23.7 0.244E-03 3181 39879 1658 42705 1.0  
\* NP 7 4 a 6 Eo 7 s 1 0 2 nu2 c1524 97950 -27.6 0.374E-03 2021 01734 496 03508 0.0  
\* OP 11 7 10 Eo 11 s 5 1 nu4 1525 23260 11.2 0.104E-02 2649 79863 1124 56715 1.0  
\* OP 9 5 a 8 Eo 10 s 3 1 nu4 1525 39210 -37.2 0.273E-02 2424 33065 798 94883 1.0  
\* P 12 5 a 9 Ee 5 s 7-1 nu4 c1525 06187 0.0 0.173E-02 2137 79730 798 74513 0.0  
\* OP 10 6 a 9 A2e 6 s 4 1 nu4 1525 49263 -3.3 0.364E-02 2181 14373 955 50777 1.0  
\* PP 6 5 a 5 A2e 4 s 2-1 nu4 1525 76245 0.0 0.588E-04 1909 08037 383 31842 1.0  
\* RP 5 1 a 4 Ee 5 s 2 1 nu4 1525 94412 -13.4 0.290E-01 1820 47545 294 62399 1.0  
\* P 13 6 a 12 A2e 11 s 2 1 nu4 1526 76100 11.6 0.117E-02 1853 87060 1170 76084 1.0  
\* NP 14 9 a 13 A2e 7 s 6 0 2 nu2 c1526 80830 0.0 0.157E-04 3298 09124 1771 31036 1.0  
\* SP 4 0 a 3 A2e 2 s 2-1 nu4 1526 92780 6.4 0.462E-02 1726 22106 199 29390 1.0  
\* OP 8 2 a 8 A2e 5 s 2 1 nu4 1526 92822 0.0 0.247E-02 2137 79730 798 74513 1.0  
\* P 13 6 a 12 A2e 11 s 2 1 nu4 1527 06152 18.1 0.625E-03 2111 03716 983 97745 1.0  
\* MP 9 5 a 8 Eo 11 s 1 0 2 nu2 c1527 09789 0.0 0.139E-03 2926 02586 798 94883 0.0  
\* UO 13 3 a 13 A2e 7 s 7 1 nu4 c1527 22467 0.0 0.166E-04 3279 87606 1752 64820 1.0  
\* SP 4 1 a 3 Ee 3 s 3 1 nu4 c1527 94968 0.0 0.107E-04 1722 85603 194 96331 0.0

\* OP 5 1 a 4 Eo 6 s 1-1 nu4 1528 06740 -2.0 0.409E-02 1822 69759 294 62399 1.0  
\* QP 4 2 a 6 Eo 3 s 6 1 nu4 c1528 26651 0.0 0.418E-04 1929 91175 401 64783 1.0  
\* SQ 10 5 a 10 Eo 6 s 7-1 nu4 1528 37330 -33.1 0.114E-02 2523 64417 995 26756 1.0  
\* PP 6 4 a 5 Eo 4 s 3-1 nu4 1528 37732 -3.9 0.359E-00 1885 96189 357 58418 1.0  
\* P 9 5 a 8 Ee 11 s 1 1 nu4 1528 51140 2.1 0.210E-02 2326 88564 798 37451 1.0  
\* MP 9 4 a 8 Ee 14 s 0 1 nu4 c1528 53166 0.0 0.274E-02 2068 97213 540 42168 0.0  
\* TQ 11 3 a 11 A2e 5 s 6 0 2 nu2 1528 94400 -1.8 0.376E-03 2360 25059 831 45801 1.0  
\* QP 13 6 a 13 A2o 6 s 6 1 nu4 1529 12250 9.9 0.236E-03 2187 20716 1658 42705 1.0  
\* P 6 4 a 5 Ee 5 s 1-1 nu4 1529 28957 0.0 0.374E-00 1887 57400 358 28449 1.0  
\* NP 8 5 a 7 Ee 7 s 2 0 2 nu2 c1529 31501 0.0 0.632E-03 2150 37824 621 06555 0.0  
\* CP 6 2 a 5 Ee 9 s 0 1 nu4 1530 00950 43.7 0.443E-02 1932 28288 402 27775 1.0  
\* P 10 6 a 9 A2o 6 s 1-1 nu4 1530 47480 3.6 0.212E-02 2485 58086 955 10643 1.0  
\* PP 6 5 a 5 Ee 3 s 4-1 nu4 1530 61414 1.1 0.458E-04 1854 38294 324 36891 1.0  
\* QP 5 1 a 4 Ee 7 s 1-1 nu4 1530 65250 19.8 0.470E-02 1824 61878 293 96826 1.0  
\* SQ 10 5 a 10 Ee 7 s 7-1 nu4 1531 11610 47.0 0.114E-02 2525 88453 994 77313 1.0  
\* P 10 6 a 9 A2o 3 s 4-1 nu4 1531 15906 -17.9 0.446E-00 1856 28804 325 36719 1.0  
\* P 12 6 a 12 A2e 9 s 0 0 2 nu2 c1531 35528 0.0 0.117E-04 2936 91815 1405 56243 1.0  
\* PP 4 2 a 3 Eo 2 s 1 0 2 nu2 c1531 64732 0.0 0.525E-04 1715 47848 183 82908 1.0  
\* MP 13 6 a 12 A2o 10 s 2-1 nu4 c1531 71418 0.0 0.233E-04 3189 79343 1658 07925 0.0  
\* P 14 6 a 14 Ee 6 s 8-1 nu4 c1532 33874 0.0 0.901E-04 3461 94911 1929 61381 1.0  
\* PP 6 6 a 5 A2o 1 s 5-1 nu4 1532 45032 19.5 0.121E-01 1816 02272 831 57435 1.0  
\* SQ 6 4 a 6 Ee 1 s 6-1 nu4 1532 59500 24.6 0.179E-02 1890 87703 358 28449 1.0  
\* NP 9 6 a 8 A2o 4 s 0 2 nu2 c1532 60413 6.8 0.157E-02 2290 98871 758 38526 1.0  
\* UO 8 2 a 8 Ee 5 s 6 1 nu4 c1532 61387 0.0 0.472E-04 2210 52999 697 91701 1.0  
\* PP 6 6 a 5 A2e 1 s 5-1 nu4 1532 68298 -42.1 0.121E-01 1817 09732 846 41013 1.0  
\* P 11 7 a 11 Ee 11 s 1-1 nu4 c1533 09353 0.0 0.413E-03 2657 12980 1124 03568 1.0  
\* SQ 6 12 a 12 Ee 4 s 10 1 nu4 c1533 28413 0.0 0.900E-03 3741 74058 1887 57400 1.0  
\* MP 11 5 a 11 Ee 17 s 1-1 nu4 1533 37040 -8.7 0.848E-04 2743 45226 1020 08099 1.0  
\* UO 7 2 a 7 Eo 5 s 6 1 nu4 1533 37040 24.6 0.117E-03 2073 21284 539 84490 1.0  
\* K 5 0 a 4 A2o 4 s 1 1 nu4 1533 79675 63.4 0.682E-00 1831 43217 297 64476 1.0  
\* P 6 2 a 5 Eo 5 s 0 1 nu4 c1533 96939 0.0 0.380E-03 2339 61617 1124 03568 1.0  
\* MP 12 5 a 11 A2o 10 s 2-1 nu4 c1534 12547 0.0 0.368E-04 2939 69214 1405 56243 0.0  
\* SQ 11 5 a 11 Ee 8 s 7-1 nu4 1534 17740 -31.5 0.627E-03 2744 69261 1210 51206 1.0  
\* P 11 5 a 11 Ee 8 s 6-1 nu4 1534 37500 -40.1 0.186E-02 1891 96319 401 64783 1.0  
\* OP 14 11 s 13 Ee 9 s 9 1 nu4 c1534 41901 0.0 0.114E-03 3162 57624 1628 15546 1.0  
\* NP 10 7 s 9 Ee 8 s 4 0 2 nu2 1534 68680 0.8 0.866E-03 2442 65175 907 96503 1.0  
\* P 8 4 a 7 Eo 12 s 1-1 nu4 c1534 82769 0.0 0.208E-04 2188 69945 653 87060 1.0  
\* NP 8 4 a 7 Eo 12 s 1-1 nu4 c1534 82769 0.0 0.208E-04 2188 69945 653 87060 1.0  
\* OP 16 13 a 15 Eo 10 s 11 1 nu4 c1535 03167 0.0 0.234E-04 3596 41349 2061 38411 1.0  
\* OP 13 10 s 12 Ee 8 s 8 1 nu4 1535 27129 -20.4 0.237E-03 2965 18390 1429 91057 1.0  
\* QP 5 2 a 4 Ee 6 s 2 1 nu4 c1535 30576 0.0 0.379E-04 1818 92497 283 61566 1.0  
\* P 11 9 a 10 Ee 6 s 6 1 nu4 1535 37899 0.0 0.687E-03 2605 41109 1887 57400 1.0  
\* OP 12 9 s 11 A2e 4 a 7 1 nu4 1535 73830 -29.5 0.874E-03 2779 50839 1243 76714 1.0  
\* MP 9 4 a 8 Eo 15 s 0 1 nu4 1536 00660 -46.0 0.417E-03 2366 95139 830 94019 1.0  
\* NP 12 3 a 12 Ee 12 s 2 0 2 nu2 c1536 05550 0.0 0.141E-03 2841 19156 1305 12737 0.0  
\* S 7 a 7 Ee 2 s 6 1 nu4 1536 16120 0.0 0.285E-02 2032 83722 496 67614 1.0  
\* PP 5 1 a 4 Ee 8 s 0 1 nu4 1536 20874 27.8 0.308E-00 1830 17422 293 96826 1.0  
\* QP 3 2 a 2 Ee 1 s 2 0 2 nu2 1536 46106 28.9 0.138E-01 1641 64191 105 18374 1.0  
\* UO 13 12 a 14 A2e 9 s 10 1 nu4 c1536 92582 0.0 0.212E-03 3122 31036 1124 03568 1.0  
\* UO 9 2 a 9 Ee 7 s 6 1 nu4 c1536 83321 0.0 0.562E-04 2611 44913 874 61544 1.0  
\* OP 12 3 a 12 A2e 6 s 6 0 2 nu2 1536 92399 37.9 0.884E-04 3037 32425 1500 40405 1.0  
\* R 1 2 a 3 Ee 3 s 1 1 nu4 1537 47034 -10.0 0.276E-01 1721 30042 183 82908 1.0  
\* S 11 7 a 11 Ee 7 s 10 1 nu4 c1537 60121 0.0 0.618E-03 2747 60121 1887 57400 1.0  
\* SQ 14 6 a 14 A2o 7 s 8-1 nu4 c1537 52543 0.0 0.853E-04 3466 84332 1929 32140 1.0  
\* QP 5 2 a 4 Eo 5 s 2 1 nu4 c1537 53732 0.0 0.502E-03 1820 47545 282 93714 1.0  
\* MP 11 11 s 13 Ee 9 s 9 1 nu4 1537 81566 -25.9 0.143E-03 3166 58558 1628 76733 1.0  
\* OP 16 13 a 15 Ee 16 s 1 0 2 nu2 c1537 96939 0.0 0.234E-03 3513 2402 293 96826 1.0  
\* PP 5 1 a 4 Eo 7 s 0 1 nu4 1538 01025 50.6 0.354E-03 2642 63518 294 62399 1.0  
\* OP 3 1 a 2 Eo 1 s 1 0 2 nu2 1538 07446 2.6 0.148E-01 1654 35472 116 27827 1.0  
\* R 4 2 a 3 Ee 3 s 1 1 nu4 1538 30130 -17.1 0.290E-01 1722 85603 184 55302 1.0  
\* TQ 4 1 a 4 Ee 1 s 4 0 2 nu2 c1538 42899



*SQ	12	4	12	Ea	12	s 6-1	nu4	1562.44310	3.6	0.303E-01	3038.61908	1476.17634	1.0
*SQ	12	4	12	Ea	12	s 1-1	nu4	c1562.52919	0.0	0.310E-04	3221.41309	1478.62534	1.0
*SQ	15	5	15	Ea	15	s 7-1	nu4	n1562.58957	0.0	0.142E-04	3819.19740	2256.60783	0.0
*OP	15	14	14	Ea	5	s12-1	nu4	1562.60018	8.8	0.865E-04	3212.16852	1649.56922	0.0
*Q	7	7	7	Ea	5	s 5-1	nu4	c1562.63694	0.0	0.267E-03	3113.39577	590.75859	0.0
*OP	13	12	12	Ea	10	s 1-1	nu4	1562.79199	-14.2	0.547E-03	2811.86702	1269.45364	0.0
*MP	7	4	4	Ea	11	a 0-1	nu4	1563.10623	39.5	0.817E-03	2059.13736	496.03508	1.0
*OP	6	4	4	Ea	7	a 2-1	nu4	1563.39920	-19.2	0.538E-02	1920.98430	397.58416	1.0
*OP	6	4	4	Ea	5	s 3-1	nu4	1563.40000	-27.0	0.511E-02	2026.67007	446.01364	1.0
*PP	4	4	4	Ea	1	s 3-1	nu4	1563.82385	1.8	0.779E-02	1703.16168	139.35801	0.0
*OP	8	6	6	Ea	4	a 4-1	nu4	1563.87090	-2.7	0.765E-02	2144.65080	580.77963	1.0
*OF	4	2	3	Ea	6	s 0-1	nu4	1563.98350	18.5	0.462E-02	1748.53467	184.55352	1.0
*Q	3	1	1	Ea	3	s 1-1	nu4	1563.99570	0.0	0.146E-02	1680.27461	126.63902	1.0
*TO	12	2	12	Ea	14	s 5-0	2nu2	c1564.04783	0.0	0.616E-04	3081.95488	1517.94098	0.0
*NP	7	6	6	A2o	2	s 3-0	2nu2	1564.06710	-11.1	0.166E-02	1986.52632	422.45811	1.0
*PP	4	3	3	Ea	2	a 3-1	nu4	1564.08240	-36.0	0.776E-02	1740.24922	140.16322	1.0
*Q	13	13	13	Ea	11	s 1-1	nu4	1564.15930	-20.3	0.572E-02	2833.21415	1266.93164	0.0
*SQ	8	3	8	A2e	4	a 5-1	nu4	1564.22750	-23.0	0.698E-02	2243.51303	679.28786	1.0
*OP	9	7	8	Ea	7	a 5-1	nu4	1564.33740	-8.1	0.235E-02	2275.19451	710.85630	0.0
*LP	10	8	9	A2o	7	s 1-1	nu4	c1564.34155	0.0	0.104E-03	2519.44370	955.10643	0.0
*Q	12	12	12	Ea	5	s 9-1	nu4	1564.37890	-20.4	0.494E-03	2661.81789	885.35649	0.0
*OP	14	13	13	Ea	6	a11-1	nu4	c1564.74704	0.0	0.195E-03	3018.48140	1453.73603	0.0
*OP	15	12	14	A2o	6	a12-0	2nu2	1565.05314	0.0	0.404E-04	3403.80887	1838.45573	0.0
*OP	10	8	9	Ea	8	s *	nu4	1565.09440	-15.9	0.122E-02	2418.30719	853.21120	1.0
*UQ	9	9	9	Ea	5	s 5-1	nu4	c1565.11977	0.0	0.101E-03	2450.50800	885.35649	0.0
*NP	8	11	10	Ea	4	a 8-1	nu4	1565.60750	-11.4	0.790E-03	2537.56687	937.58523	1.0
*NP	8	7	7	Ea	4	a 4-0	2nu2	1565.69458	-16.1	0.112E-02	2098.59022	532.89403	1.0
*Q	13	11	13	Ea	10	s 1-1	nu4	1565.71789	-0.6	0.120E-01	2426.90659	808.02702	1.0
*OP	3	1	2	Ea	3	s 1-1	nu4	1565.96340	-13.0	0.194E-02	1681.50281	115.53661	0.0
*NP	11	9	10	A2e	4	a 6-0	2nu2	1566.01828	58.4	0.113E-02	2573.82086	1007.80842	1.0
*OP	5	3	4	A2e	4	a 1-1	nu4	1566.21210	65.0	0	0	0	0
*Q	13	13	13	Ea	10	s 1-1	nu4	1566.21210	65.0	0	0	0	0
*RQ	12	11	12	Ea	2	a12-1	nu4	c1566.31513	0.0	0.632E-03	2664.58612	1098.29418	0.0
*RQ	15	13	15	Ea	4	a14-1	nu4	c1566.32589	0.0	0.581E-03	3134.08002	1747.76485	0.0
*NP	10	9	9	A2e	2	a 6-0	2nu2	1566.34850	-10.9	0.217E-02	2357.03012	790.48053	1.0
*NP	9	5	9	Ea	5	s 0-2	nu4	1566.43099	-17.4	0.222E-02	2222.07891	655.02702	1.0
*OP	4	2	3	Ea	6	a 0-1	nu4	1566.51389	-1.1	0.306E-02	1750.34266	183.82908	1.0
*RQ	14	12	14	A2e	2	a13-1	nu4	1566.57291	28.0	0.741E-03	3111.95143	1545.38132	1.0
*Q	13	12	13	A2e	3	a10-1	nu4	1566.80083	-2.5	0.817E-03	2836.78763	1269.99797	1.0
*NP	12	10	11	Ea	8	s 1-1	nu4	c1566.83991	0.0	0.174E-04	3324.42507	1357.58406	0.0
*NP	12	10	11	Ea	7	s 7-0	2nu2	c1566.87470	0.0	0.242E-03	2741.48040	1174.60806	0.0
*TO	5	0	5	A2o	2	s 3-0	2nu2	1566.88894	-54.4	0.413E-03	1864.53554	297.64176	1.0
*Q	13	13	13	Ea	7	s 5-1	nu4	1566.95755	-7.7	0.345E-03	2757.19451	710.85630	0.0
*MP	8	5	7	Ea	12	s 1-1	nu4	1567.00488	-16.4	0.252E-03	2188.69945	621.62923	1.0
*Q	14	13	14	Ea	2	a13-0	2nu2	1567.17707	-6.0	0.200E-02	3020.97100	1453.73603	1.0
*NP	13	11	12	Ea	8	s 8-0	2nu2	c1567.49993	0.0	0.975E-04	3921.03371	1353.58634	0.0
*NP	13	11	12	Ea	8	s 8-0	2nu2	c1567.49993	0.0	0.975E-04	3921.03371	1353.58634	0.0
*NP	14	12	13	A2o	4	a 9-0	2nu2	c1567.66083	0.0	0.703E-04	3121.53171	1544.63569	0.0
*RP	3	0	2	A2o	2	s 1-1	nu4	1567.99304	21.4	0.677E-04	3687.22874	1719.23784	1.0
*PP	16	15	15	Ea	3	a14-1	nu4	c1568.60154	0.0	0.222E-02	1309.43039	1740.83513	0.0
*Q	13	12	13	Ea	5	s 1-1	nu4	1568.70133	0.0	0.192E-03	2826.98133	1478.62534	1.0
*UQ	1	1	1	Ea	11	s 5-1	nu4	1568.77301	21.0	0.814E-04	2649.79863	1081.02772	1.0
*OP	12	11	11	Ea	5	s 9-1	nu4	1568.77420	19.7	0.795E-03	2667.06641	1098.29418	1.0
*Q	12	11	11	Ea	2	a 4-1	nu4	1568.77420	19.7	0.795E-03	2667.06641	1098.29418	1.0
*MP	10	6	9	A2o	8	a 2-1	nu4	c1569.06442	0.0	0.145E-03	2524.17689	955.10643	0.0
*MP	11	7	10	Ea	13	s 3-1	nu4	1569.30353	33.9	0.342E-04	2693.86729	1124.56715	1.0
*SQ	13	4	13	Ea	14	s 6-1	nu4	1569.35050	-10.2	0.122E-03	3297.69190	1728.34758	1.0
*Q	13	13	13	Ea	5	s 1-1	nu4	1569.54540	-44.3	0.470E-02	2425.72158	856.02702	1.0
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*RQ	12	11	12	Ea	2	a12-1	nu4	1570.15895	-44.3	0.609E-02	2667.60044	1097.43706	1.0
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*SQ	5	5	15	Ea	17	a 7-1	nu4	n1570.52831	0.0	0.127E-04	3826.91528	2256.38697	0.0
*SQ	4	2	4	Ea	1	a 4-1	nu4	1570.68810	-32.2	0.243E-02	1754.52040	183.82908	1.0
*Q	10	10	10	Ea	1	a10-0	2nu2	1571.25868	17.5	0.202E-01	2292.39035	721.13324	1.0
*SQ	15	13	15	Ea	2	a13-1	nu4	c1571.31398	0.0	0.104E-03	3111.95143	1545.38132	1.0
*SQ	5	2	5	Ea	3	a 4-1	nu4	1571.36620	-0.8	0.456E-02	1854.98294	283.61666	1.0
*Q	9	1	9	Ea	9	s *	nu4	c1571.50509	0.0	0.408E-03	2456.41972	884.91558	0.0
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*RQ	11	10	11	Ea	1	a11-1	nu4	1571.97390	149.0	0.108E-02	2510.74722	938.78822	1.0
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*MP	8	5	7	Ea	11	a 1-1	nu4	1572.09587	19.7	0.365E-03	2193.15945	621.06555	1.0
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*Q	10	9	9	Ea	9	s 7-1	nu4	1572.42422	9.2	0.475E-02	2363.99992	721.13324	1.0
*TO	13	13	13	A2o	16	s 5-0	2nu2	n1572.45455	0.0	0.282E-04	3342.20422	1769.74967	0.0
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*Q	13	12	13	A2e	3	a 4-1	nu4	1573.34669	-13.4	0.185E-02	2816.40004	283.61666	1.0
*RQ	15	12	15	A2e	3	a13-1	nu4	n1573.89770	0.0	0.398E-03	3412.97167	1839.07397	0.0
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*MP	6	4	5	Ea	9	s 0-1	nu4	1574.00095	25.6	0.537E-03	1932.28888	558.28449	1.0
*MP	6	4	5	Ea	6	a 1-1	nu4	1574.00095	25.6	0.537E-03	1932.28888	558.28449	1.0
*Q	3	2	2	Ea	2	a 2-1	nu4	c1574.21621	0.0	0.326E-04	1768.63849	140.42207	0.0
*TO	7	0	7	A2o	3	s 3-0	2nu2	1574.33650	-2.6	0.441E-03	2128.72982	554.39306	1.0
*SQ	6	2	6	Ea	5	s 4-1	nu4	1574.38300	-7.7	0.558E-02	1976.66152	402.27775	1.0
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*MP	11	7	10	Ea	14	a 3-1	nu4	1575.67570	-68.6	0.503E-04	2699.70024	1124.03568	0.0
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*SQ	13	4	13	Ea	14	a 6-1	nu4	c1575.78783	0.0	0.113E-03	3303.82567	1728.05529	0.0
*PP	3	2	2	Ea	3	s 1-1	nu4						

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Q 9 3 9 A2e 8 s1 0 2nu2 1660.55600 45.9 0.847E-02 2516.73023 856.17882 1.0  
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Q 8 7 8 Ee 4 s1 0 2nu2 1661.83704 -14.4 0.179E-01 2194.73251 532.89403 1.0  
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Q 8 7 8 Ee 4 s1 0 2nu2 1662.77300 5.3 0.124E-01 2196.44145 533

[illegible]



[illegible]

Q P 7 4 6 Eo 12 a 4 0 2nu2 1736.44090 -0.1 0.180E-02 2232.47599 496.03508 1.0  
\* Q 6 6 7 A2o 4 a 2-1 nu4 1735.50510 283.57435 1.0  
\* T R 7 6 6 A2o 4 a 3 0 2nu2 -1736.59733 0.0 0.121E-03 2290.98871 554.39306 1.0  
\* O Q 9 7 8 Eo 7 a 5 1 nu4 1736.61250 45.0 0.133E-02 2270.27698 573.66998 1.0  
\* U R 8 2 10 Ee 9 a 6 1 nu4 -1736.87216 0.0 0.510E-04 2611.48776 874.61644 0.0  
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\* Q O 7 7 8 Ee 5 a 5 1 nu4 1739.14480 -18.7 0.739E-03 2113.39577 374.24900 0.0  
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\* R R 6 1 6 A2e 2 a 7 1 nu4 1739.39307 25.0 0.788E-00 2023.80070 284.41013 1.0  
\* S R 6 1 7 Ee 8 a 3-1 nu4 1739.50030 11.3 0.406E-02 2152.12347 412.62430 1.0  
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\* Q R 6 4 7 Ee 12 a 5 1 nu4 1740.01290 14.6 0.287E-03 2864.04712 1124.03568 1.0  
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\* Q R 7 7 8 Ee 1 a 7 0 2nu2 1745.08557 -4.0 0.202E-00 2120.15281 375.10577 1.0  
\* Q 12 7 9 Ee 8 a 1 1 nu4 1745.38530 -15.6 0.165E-03 3104.71571 1359.32855 0.0  
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\* S R 9 4 10 Ee 8 a 6-1 nu4 1746.30130 -33.5 0.188E-02 2577.76266 831.45801 1.0  
\* M Q 6 5 11 Ee 9 a 6 1 nu4 1746.34897 0.0 0.413E-02 284.41013 0.0 1.0  
\* H Q 6 5 11 Ee 9 a 2 1 nu4 1746.42800 -13.4 0.209E-01 2041.05933 294.62999 1.0  
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\* P R 4 4 5 Ee 9 a 3-1 nu4 1747.28929 0.0 0.169E-04 3159.95088 1612.65270 1.0  
\* P R 4 4 5 Ee 9 a 3-1 nu4 1747.41101 1.4 0.114E-01 1887.57409 140.16322 1.0  
\* O R 4 2 5 Ee 9 a 8 0 2nu2 1747.73420 43.4 0.206E-02 1932.28288 184.95302 1.0  
\* R R 6 5 7 Ee 5 a 6 1 nu4 1748.08679 11.4 0.211E-00 2073.21267 325.12716 1.0  
\* Q R 6 2 6 Ee 7 a 2 0 2nu2 1748.10320 27.1 0.527E-01 2150.37824 402.27775 0.0  
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\* N Q 9 8 9 Ee 7 a 5 0 2nu2 1748.33450 -7.5 0.366E-03 2403.98157 655.64632 1.0  
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\* M Q 10 5 10 Ee 17 a 1-1 nu4 1748.68268 0.0 0.137E-03 2743.45226 994.77313 0.0  
\* O Q 14 7 14 Ee 19 a 5 1 nu4 1749.13633 0.0 0.217E-04 3633.45771 1884.32138 0.0  
\* Q 10 3 11 Ee 11 a \* \* \* -1749.16397 -8.0 0.288E-03 2657.12980 907.96503 1.0  
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\* M Q 7 6 7 A2e 6 a 2-1 nu4 1749.59314 50.0 0.122E-03 2172.81095 423.22281 1.0  
\* S R 9 4 10 Ee 7 a 6-1 nu4 1749.70140 64.5 0.184E-02 2580.63514 830.94019 1.0  
\* R R 6 2 7 Ee 8 a 3-1 nu4 1749.84726 0.0 0.141E-04 2152.12347 402.27775 0.0  
\* M Q 6 6 6 A2o 4 a 2-1 nu4 1749.96164 24.4 0.663E-04 2033.53355 283.57435 1.0  
\* Q R 6 1 7 Ee 9 a 1 0 2nu2 1750.15430 21.9 0.399E-01 2163.38989 413.23778 1.0  
\* Q R 6 0 8 A2e 5 a 0 0 2nu2 1750.89661 42.8 0.744E-01 2167.78007 416.88774 1.0  
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\* S R 10 7 11 Ee 17 a 1-1 nu4 1751.08412 -11.4 0.441E-00 2125.34426 994.77313 1.0  
\* S R 6 1 4 Ee 10 a 3 1 nu4 1751.50102 2.8 0.220E-02 2164.74052 413.23778 1.0  
\* O R 4 2 5 Ee 6 a 5 1 nu4 1751.53136 5.9 0.210E-00 2190.32675 357.58418 1.0  
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\* Q R 7 6 8 A2e 2 a 6 0 2nu2 1751.82310 -3.4 0.406E-02 2046.45343 294.62999 1.0  
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\* O Q 10 8 10 Ee 9 a 6 1 nu4 1752.19780 -20.9 0.359E-03 2605.41109 853.21120 1.0  
\* Q 13 4 13 Ee 10 a 1-1 nu4 1752.79120 0.0 0.619E-03 2210.51299 478.14860 1.0  
\* M Q 12 5 12 Ee 22 a 1-1 nu4 1752.39967 0.0 0.331E-04 3196.85891 1444.47659 0.0  
\* S R 11 6 12 A2e 4 a 8-1 nu4 1752.40880 -22.3 0.123E-02 2923.64635 171.23532 1.0  
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\* R R 6 4 13 Ee 5 a 5 1 nu4 1755.10494 -4.4 0.177E-00 2133.95077 358.28449 1.0  
\* S R 12 7 12 Ee 9 a 5 1 nu4 1755.35860 -16.0 0.309E-03 3114.59005 1359.32855 0.0  
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\* S R 11 6 12 A2o 5 a 8 1 nu4 1755.83240 6.8 0.121E-02 2926.59256 1710.76084 1.0  
\* Q 11 5 10 Ee 19 a \* \* \* -1755.86533 0.0 0.445E-04 2965.94652 1210.08092 0.0  
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\* S R 6 0 8 A2e 6 a 7 1 nu4 1755.92639 31.8 0.139E-01 2172.81095 416.88774 1.0  
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\* Q P 6 2 5 Ee 11 a 2 0 2nu2 1756.93989 -10.2 0.261E-02 2158.58755 401.64783 1.0  
\* O Q 10 8 10 Ee 9 a 6 1 nu4 1757.58250 15.0 0.606E-03 2611.48776 853.90676 1.0  
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\* S R 13 8 14 Ee 8 a 10-1 nu4 1757.97411 0.0 0.142E-03 3317.48556 1559.51145 0.0  
\* Q R 7 7 8 Ee 8 a 0 2nu2 1758.37708 -11.4 0.902E-03 2222.07896 463.01304 1.0  
\* M Q 8 8 A2o 6 a 2-1 nu4 1758.56846 0.0 0.265E-03 2139.34844 800.77963 0.0  
\* S R 12 7 13 Ee 8 a 9-1 nu4 1758.59600 8.4 0.303E-03 3117.59398 1358.87122 1.0  
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\* L Q 10 6 10 A2e 8 a 1 1 nu4 1759.65362 0.0 0.913E-04 2715.30247 955.65077 0.0  
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\* Q 11 8 11 Ee 11 a 6 1 nu4 1760.03340 28.5 0.352E-03 2830.40785 1070.37030 0.0  
\* O R 10 2 11 Ee 11 a 6 1 nu4 1760.05094 0.0 0.352E-04 2830.40785 1070.37030 0.0  
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\* O Q 13 8 13 Ee 15 a 6 1 nu4 1764.47350 -40.5 0.683E-04 3323.98900 1559.51145 1.0  
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\* R R 8 8 9 Ee 2 a 9 1 nu4 1765.50439 -18.9 0.300E-00 2242.77037 477.26409 1.0  
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\* R R 10 10 Ee 10 a \* \* \* -1766.74297 -29.9 0.464E-03 2179.37216 412.62430 1.0  
\* R R 6 1 7 Ee 11 a 2 1 nu4 1767.39570 8.8 0.624E-02 2180.63260 413.23778 1.0  
\* R R 6 1 7 Ee 11 a 2 1 nu4 1767.39570 8.8 0.624E-02 2180.63260 413.23778 1.0  
\* S R 7 5 6 Ee 5 a 6 1 nu4 1767.58107 11.2 0.151E-00 2230.52999 463.01304 1.0  
\* S R 8 2 9 Ee 10 a 4 1 nu4 1767.83630 0.9 0.209E-02 2465.23154 697.91701 1.0  
\* Q 10 9 10 A2e 3 a 7



\*QR 6 2 7 Ee 10 2 1 nu4 1777.09112 -32.9 0.109E-03 2179.37216 402.27775 1.0  
\*MQ 8 7 8 Ee 9 3-1 nu4 1777.45501 16.4 0.312E-04 2311.12235 533.66898 1.0  
\*SR 12 6 13 A2e 5 8-1 nu4 1777.82590 -4.6 0.470E-03 2183.38879 1405.56243 1.0  
\*H 11 6 13 Ee 5 1-1 nu4 1777.86057 164.5 0.101E-03 2170.76084 1.0  
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\*QP 5 1 4 A2e 4 5 0 2nu2 1778.23880 -21.4 0.638E-02 2075.88270 297.64176 0.0  
\*QP 5 1 4 Ee 9 1 0 2nu2 1778.39720 -0.6 0.311E-02 2072.36552 293.96826 1.0  
\*Q 5 1 4 Ee 5 3-1 nu4 1778.51841 0.6 0.7 2275.16751 496.67614 1.0  
\*OO 9 9 9 A2e 3 7 1 nu4 c1778.53919 0.0 0.418E-03 2371.12655 592.58650 1.0  
\*OO 12 9 12 A2e 6 7 1 nu4 1778.59970 -4.3 0.323E-03 3022.97191 1244.31718 1.0  
\*SR 11 5 12 Ee 11 7-1 nu4 1778.69890 23.7 0.459E-03 2988.77752 1210.08099 1.0  
\*R 9 13 13 A2e 6 7 1 nu4 1778.80629 139.0 0.130E-03 3277.13487 1498.34248 1.0  
\*Q 13 6 13 A2e 11 1 1 nu4 1778.87142 0.0 0.150E-04 3437.29847 1658.42705 1.0  
\*QP 5 2 4 Ee 9 2 0 2nu2 1778.87640 -3.3 0.285E-02 2061.81387 282.93714 1.0  
\*QR 6 2 7 Ee 11 2 1 nu4 1778.98596 21.9 0.474E-04 2180.63260 401.64783 1.0  
\*UR 12 3 8 A2e 5 4 1 nu4 1779.96570 -10.7 0.956E-01 2301.58870 521.62193 1.0  
\*OR 4 4 5 Ee 7 2 1 nu4 1779.32700 9.6 0.281E-03 1919.48926 140.16322 0.0  
\*QP 5 3 4 A2e 4 4 0 2nu2 1779.71176 0.0 0.469E-02 2044.22762 264.51662 0.0  
\*RR 9 3 10 A2e 1 8 0 1 nu4 1779.72907 -29.4 0.378E-00 2372.31851 592.58650 1.0  
\*R 7 3 8 A2e 7 7 1 nu4 c1779.10765 0.0 0.180E-04 3279.87606 1500.76522 1.0  
\*QR 6 1 7 Ee 11 1-1 nu4 1780.53440 -7.5 0.234E-02 2193.15945 412.62430 1.0  
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\*SR 13 7 14 Ee 10 9-1 nu4 c1781.02171 0.0 0.106E-03 3391.66787 1612.65277 0.0  
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\*R 6 6 A2e 5 1 1 nu4 1781.36170 -69.7 0.413E-02 2466.08529 264.51662 1.0  
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\*MQ 8 7 8 Ee 10 3-1 nu4 c1781.80730 0.0 0.465E-04 2314.70076 532.89403 0.0  
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\*NQ 10 9 10 A2e 4 6 0 2nu2 c1783.14119 0.0 0.202E-04 2667.98073 1284.36524 1.0  
\*RR 7 3 8 A2e 5 4 1 nu4 1783.22290 8.7 0.199E-00 2363.79962 592.58650 1.0  
\*Q 14 9 14 A2e 8 7 1 nu4 n1783.25318 0.0 0.379E-03 2573.82086 790.69053 1.0  
\*R 9 10 10 Ee 4 9 1 nu4 1783.78321 9.3 0.366E-01 2355.44496 522.22293 1.0  
\*SR 8 1 9 Ee 11 3-1 nu4 1783.93580 19.3 0.154E-02 2492.68147 708.74660 1.0  
\*SR 14 8 15 Ee 10 10-1 nu4 c1784.07140 0.0 0.444E-04 3615.80435 1831.74499 1.0  
\*R 8 5 15 A2e 1 5 1 nu4 1784.39089 -25.0 0.176E-04 3846.76817 0.0  
\*NR 6 3 7 A2e 5 5 0 2nu2 1784.47977 181.2 0.105E-02 2167.80007 383.31842 0.0  
\*Q 12 6 12 Ee 10 3 1 nu4 1784.48206 -36.9 0.202E-01 2324.33065 539.84490 1.0  
\*QR 12 6 12 A2e 10 2-1 nu4 n1784.48730 0.0 0.517E-04 3189.78343 1405.15377 1.0  
\*SR 7 0 8 A2e 6 2-1 nu4 1784.95060 -47.8 0.605E-02 2339.34844 554.39306 0.0  
\*SR 13 7 14 Ee 10 9-1 nu4 1785.27047 -4.6 0.103E-03 3397.53433 1612.65240 1.0  
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\*Q 15 9 15 A2e 9 7 1 nu4 c1785.30538 0.0 0.171E-04 3848.11122 2062.75969 1.0  
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\*SR 14 9 13 A2e 11 10-1 nu4 n1788.37089 0.0 0.161E-04 3819.72105 1.0  
\*SR 8 1 9 Ee 12 3-1 nu4 1789.06420 -15.0 0.105E-02 2497.30418 708.74660 1.0  
\*RR 6 0 7 A2e 7 1 1 nu4 1789.32874 -4.6 0.805E-01 2206.21694 511.32034 1.0  
\*PR 6 1 7 Ee 6 2-1 nu4 1789.49646 19.3 0.518E-01 2172.10595 383.31842 1.0  
\*R 10 10 11 Ee 1 8 1 nu4 1789.52910 151.2 0.744E-01 2510.74722 721.13324 1.0  
\*RR 8 6 9 A2e 3 7 1 nu4 1789.65540 -0.6 0.702E-01 2371.12655 581.47075 1.0  
\*RR 8 6 10 Ee 3 9 1 nu4 1789.72911 4.6 0.105E-00 2445.37497 655.64632 1.0  
\*PR 6 1 7 Ee 13 0 1 nu4 1789.75050 -7.9 0.369E-01 2202.98901 413.23778 1.0  
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\*OQ 11 10 11 Ee 7 6 1 nu4 1791.33900 11.0 0.223E-03 2790.12612 938.78822 0.0  
\*MQ 10 7 10 Ee 14 4 1 nu4 c1791.73062 0.0 0.542E-04 2699.70024 907.96503 1.0  
\*PR 6 4 7 Ee 8 3-1 nu4 1791.80664 3.9 0.157E-01 2149.39043 357.58419 1.0  
\*R 6 6 A2e 5 4 1 nu4 1791.82250 67.9 0.232E-02 2057.14233 265.22662 1.0  
\*PR 6 3 7 A2e 5 4 1 nu4 1792.01752 -13.9 0.448E-01 2503.56687 711.54796 1.0  
\*MR 4 4 5 Ee 9 0 1 nu4 1792.03300 29.3 0.167E-01 2176.00752 383.37745 1.0  
\*QR 8 3 11 A2e 5 9 0 2nu2 1792.12368 0.0 0.275E-04 2312.28288 140.16322 0.0  
\*MQ 13 6 13 A2e 12 2-1 nu4 1793.17310 11.4 0.368E-01 2473.00667 679.83671 1.0  
\*SR 9 2 12 A2e 12 2-1 nu4 c1793.26706 0.0 0.206E-04 3451.35746 1658.07925 0.0  
\*Q 12 10 11 Ee 12 4-1 nu4 1793.28630 -20.6 0.105E-02 2667.43865 874.15029 1.0  
\*R 10 10 11 Ee 12 4-1 nu4 1793.56118 4.0 0.630E-04 3037.32425 1243.76714 1.0  
\*RR 10 10 11 Ee 2 11 1 nu4 1793.76174 -37.2 0.111E-00 2513.94456 720.17910 1.0  
\*PR 6 4 7 Ee 8 3-1 nu4 1793.84009 11.1 0.128E-01 2152.12347 358.28449 1.0  
\*OQ 13 10 13 Ee 6 8 1 nu4 1794.03002 -4.7 0.835E-02 2218.33911 324.36891 1.0  
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\*MQ 12 7 12 Ee 10 8 1 nu4 c1794.53530 0.0 0.160E-04 3153.86733 1359.32885 1.0  
\*R 6 2 7 Ee 12 3 1 nu4 1795.22280 26.7 0.146E-02 2197.49789 402.27775 1.0  
\*PR 6 5 7 Ee 12 5 1 nu4 1795.40955 12.5 0.701E-02 2120.5349 322.12719 1.0  
\*PR 6 6 7 A2e 2 5-1 nu4 1796.01860 17.4 0.622E-02 2079.59121 283.57435 1.0  
\*SR 11 4 12 Ee 12 6 1 nu4 1796.11530 12.7 0.365E-03 3038.61908 1242.50505 1.0  
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\*R 8 5 9 Ee 8 1 1 nu4 1796.61228 -9.8 0.179E-01 2418.30719 621.69293 1.0  
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\*OQ 13 10 13 Ee 12 8 1 nu4 1796.94920 -14.6 0.689E-04 3227.46757 1430.51691 1.0  
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\*SR 13 3 11 A2e 6 5 1 nu4 1797.28565 -3.0 0.1 2187.28565 1.0  
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\*M 11 7 11 Ee 16 4 3-1 nu4 c1797.36393 0.0 0.336E-04 2921.41309 1124.03568 0.0  
\*TR 11 2 12 Ee 14 5 0 2nu2 c1797.38248 0.0 0.499E-04 3081.95488 1284.60633 0.0  
\*OQ 14 10 14 Ee 12 8 1 nu4 n1797.43435 0.0 0.263E-04 3501.07234 1703.63799 0.0  
\*TR 12 3 13 A2e 7 6 0 2nu2 c1797.71461 0.0 0.425E-04 3298.09124 1500.40405 0.0  
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\*QR 7 2 8 Ee 12 2 1 nu4 1798.05064 -3.2 0.166E-03 2338.47264 540.42168 1.0  
\*NQ 10 10 10 Ee 5 7 0 2nu2 1798.29085 -1.8 0.980E-04 2518.47013 720.17910 1.0  
\*RR 9 7 8 Ee 6 8 1 nu4 1798.57982 16.5 0.597E-01 2509.43447 719.84630 1.0  
\*R 9 11 A2e 2 10 1 nu4 1798.90494 40.8 0.873E-01 2590.38874 790.69053 1.0  
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\*OQ 14 10 14 Ee 14 8 1 nu4 c1799.44831 0.0 0.276E-04 3503.60181 1704.14728 0.0  
\*A 3 7 1 nu4 1799.62440 -36.0 0.563E-01 2558.63033 759.00233 1.0  
\*QR 7 1 8 Ee 13 1-1 nu4 1799.69950 -49.4 0.177E-02 2351.02478 551.32034 1.0  
\*QR 8 1 9 Ee 13 1 0 2nu2 1799.69982 11.2 0.934E-02 2508.44530 708.74660 1.0  
\*NQ 13 9 13 A2e 7 6 0 2nu2 c1799.77618 0.0 0.145E-04 3298.09124 1498.34248 0.0  
\*Q 7 2 8 Ee 12 2 1 nu4 c1799.79619 0.0 0.105E-03 2339.63141 539.84490 0.0  
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\*QP 4 3 3 A2e 4 3 0 2nu2 1801.43130 4.7 0.318E-02 1966.76191 165.33108 1.0  
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\*R 9 6 Ee 10 4 1 nu4 1802.49512 13.5 0.731E-03 2453.38889 649.84634 1.0  
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\*NQ 11 10 11 Ee 7 7 0 2nu2 c1803.52453 0.0 0.796E-04 2741.48040 937.95823 0.0  
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\*SR 13 6 14 A2e 7 8 1 nu4 c1808.76758 0.0 0.150E-03 3466.84332 1658.07925 0.0  
\*R 7 0 A2e 6 1 1 nu4 1808.83131 11.8 0.599E-01 2363.22501 554.39306 1.0  
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\*OQ 13 11 13 Ee 9 9 1 nu4 c1809.00913 0.0 0.514E-04 3162.57624 1353.56634 0.0  
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\*PR 7 1 8 Ee 14 0 1 nu4 1809.49231 3.1 0.271E-01 2360.25059 550.78589 1.0  
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\*OQ 14 11 14 Ee 11 9 1 nu4 1812.53

*M	Q	11	9	#	11	A2e	6	a	5-1	nu4	c1841.66101	0.0	0.267E-04	2849.47064	1007.80842	0.0
*M	Q	11	9	#	10	E	16	a	0-1	nu4	1841.70780	4.3	0.135E-03	2715.85766	744.15029	1.0
*O	R	7	4	a	8	E	1	a	1-1	nu4	1841.78593	0.0	0.667E-03	2338.47124	87.35138	1.0
*O	R	7	4	a	8	E	9	a	1-1	nu4	1841.98522	-78.5	0.104E-01	2554.34656	712.35318	1.0
*R	R	13	12	a	14	E	2	a	13-1	nu4	1841.98522	-62.4	0.112E-01	3111.95143	1269.95997	0.0
*R	R	13	12	a	14	E	2	a	1-1	nu4	1842.05040	-74.7	0.510E-02	2550.80478	708.74660	1.0
*P	R	8	6	a	9	E	10	a	4-5	nu4	1842.10397	-24.2	0.481E-02	2422.88665	580.25850	1.0
*Q	P	2	1	s	1	E	3	a	1-0	2nu2	1842.10397	37.2	0.129E-02	1898.03957	55.93872	1.0
*Q	P	2	1	s	2	E	15	a	1-1	nu4	1842.27630	-52.0	0.504E-02	2540.13851	697.91701	1.0
*S	R	12	3	a	13	E	3	a	1-1	nu4	1842.72455	0.0	0.290E-03	2167.09465	424.36891	1.0
*S	R	12	3	a	13	E	8	a	5-1	nu4	1842.74180	-17.6	0.205E-03	3143.50878	1500.85789	1.0
*S	R	12	3	a	13	E	12	a	3-1	nu4	1842.85250	-14.1	0.327E-02	2497.30418	654.45027	1.0
*N	Q	13	12	s	13	A2o	4	a	9-0	2nu2	c1843.22578	0.0	0.326E-04	3112.31371	1269.07084	0.0
*N	Q	13	12	s	13	E	11	a	1-1	nu4	c1843.22578	0.0	0.129E-03	2923.91117	1090.62586	1.0
*R	R	14	14	a	15	E	2	a	15-1	nu4	1843.53519	62.1	0.471E-02	3197.07242	1353.54246	1.0
*R	R	14	14	a	15	E	10	a	4-1	nu4	1843.53760	10.1	0.262E-02	2465.23154	621.69293	0.0
*P	R	8	5	a	9	E	6	a	6-1	nu4	1843.53760	-52.3	0.142E-02	2376.42260	552.89403	0.0
*P	R	8	5	a	9	E	12	a	1-1	nu4	1843.60013	37.7	0.551E-03	2035.33145	313.54346	1.0
*Q	R	13	13	a	14	E	2	a	13-0	2nu2	1843.65988	-6.6	0.430E-02	3020.91370	1177.25316	1.0
*Q	R	12	11	a	13	E	6	a	11-1	nu4	1843.87490	15.6	0.820E-02	3018.48140	1174.60806	1.0
*Q	R	12	11	a	13	E	5	a	11-0	2nu2	1844.23470	-44.2	0.385E-02	2942.53300	1098.29418	1.0
*P	R	8	3	a	9	E	2	a	1-1	nu4	1844.23470	15.6	0.375E-02	2525.72114	580.25850	1.0
*P	R	8	3	a	9	E	2	a	1-1	nu4	1844.33360	-57.8	0.865E-02	2524.17689	679.83671	1.0
*M	R	5	11	a	13	E	10	a	1-1	nu4	c1844.60032	0.0	0.129E-04	4249.86693	205.26910	0.0
*M	R	5	11	a	13	E	9	a	11-1	nu4	c1844.68040	0.0	0.196E-04	3298.42397	1453.73603	0.0
*P	R	8	3	a	9	E	5	a	7-1	nu4	1844.78710	-15.0	0.582E-03	2322.06269	477.26409	1.0
*P	R	8	2	a	9	E	16	a	0-1	nu4	1844.89980	-23.6	0.107E-03	2542.81197	697.91701	1.0
*P	R	8	2	a	9	E	6	a	6-1	nu4	1844.96900	19.3	0.114E-02	2		

[illegible]

OR 10 4 11 Eo 17 a 2.1 nu4 1902.97750 3.4 0.168E-03 2930.07564 1027.07848 1.0  
OR 12 3 13 A2o 10 a 3.0 2nu2 1903.50752 41.3 0.226E-04 3404.26861 1500.76529 1.0  
RR 10 4 11 Ee 18 \*\*\* \*\* n1903.89545 0.0 0.186E-03 2931.43094 1027.53544 1.0  
RR 13 4 14 Ee 18 a 5.1 nu4 1904.24980 -53.4 0.399E-04 3262.60272 1728.34758 1.0  
OR 12 3 13 Ee 12 a 2.0 2nu2 n1906.16902 0.0 0.282E-04 3424.41828 1518.25026 1.0  
NO 6 3 6 A2o 7 a 0.0 2nu2 n1904.71441 0.0 0.142E-04 2688.90927 383.97745 1.0  
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RR 14 8 15 Ee 13 a 9.1 nu4 n1904.95588 0.0 0.105E-03 3736.70087 1831.74499 0.0  
OR 12 3 13 Ee 11 \*\*\* \*\* n1905.21847 0.0 0.119E-04 3437.22647 1518.25026 1.0  
RR 13 4 14 Eo 19 a 5.1 nu4 n1905.40242 0.0 0.343E-04 3633.45771 1728.05529 1.0  
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SR 14 3 15 A2e 11 a 5.1 nu4 n1905.82404 0.0 0.159E-04 3928.43429 2022.61025 1.0  
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RR 10 2 11 Eo 21 \*\*\* \*\* n1907.34596 0.0 0.104E-03 2977.29226 1069.94630 0.0  
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MR 7 6 8 A2e 6 a 2.1 nu4 c1911.08316 0.0 0.212E-04 2334.30300 423.22281 0.0  
RR 14 7 15 Ee 16 a 1.1 nu4 1911.54480 -25.0 0.500E-04 2833.24203 621.89293 1.0  
RR 14 7 15 Eo 14 a 8.1 nu4 n1911.54831 0.0 0.555E-04 3795.86969 1884.32138 1.0  
RR 11 1 12 Ee 21 \*\*\* \*\* n1911.56192 0.0 0.998E-04 3206.75769 1295.19577 0.0  
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PR 11 4 12 Eo 19 a 1.1 nu4 1911.57771 67.6 0.383E-03 3210.39548 1298.72244 1.0  
PR 11 4 12 Eo 22 a 1.1 nu4 1911.57771 67.6 0.383E-03 3210.39548 1298.72244 1.0  
PR 11 4 12 Eo 22 a 1.1 nu4 1912.27000 174.2 0.170E-03 3165.85891 1284.60633 1.0  
PR 11 5 12 Ee 16 a 4.1 nu4 1913.05640 -9.8 0.110E-03 3123.13837 1210.08091 1.0  
RR 11 1 12 Ee 22 \*\*\* \*\* n1913.05640 -9.8 0.110E-03 3123.13837 1210.08091 1.0  
MR 9 4 10 Ee 18 a 0.1 nu4 1913.52980 -84.3 0.863E-04 2744.99624 1001.45890 1.0  
RR 14 7 15 Ee 16 a 8.1 nu4 n1913.72620 0.0 0.528E-04 3797.72022 1883.99402 0.0  
PR 11 6 12 A2o 7 a 5.1 nu4 1913.87110 6.1 0.208E-03 3084.63133 1170.76084 1.0  
PR 11 1 12 Eo 11 a 1.0 2nu2 n1913.74626 27.0 0.418E-03 3266.93735 1418.25026 1.0  
QR 14 10 15 Ee 11 a 10.0 2nu2 n1914.54817 0.0 0.221E-04 3618.69545 1704.14728 1.0  
PR 11 7 12 Ee 12 a 6.1 nu4 1914.58290 -5.0 0.944E-04 3038.61908 1124.03568 1.0  
PR 11 8 12 Eo 10 a 7.1 nu4 1915.23580 -10.9 0.821E-04 2985.00837 1069.77148 1.0  
PR 11 8 12 A2e 6 a 2.1 nu4 1915.82950 -14.3 0.103E-03 2923.68435 1007.80842 1.0  
OR 9 6 10 A2o 6 a 4.1 nu4 1915.92628 -35.4 0.165E-03 2674.31508 758.38526 1.0  
PR 11 10 12 Eo 6 a 9.1 nu4 1916.38900 -7.2 0.466E-04 2854.34795 937.95823 1.0  
MR 8 7 9 Eo 9 a 5.1 nu4 1916.83970 0.6 0.492E-04 2450.50862 533.66898 1.0  
MR 8 7 9 A2o 6 a 2.1 nu4 c1916.88798 0.0 0.291E-04 2322.31811 423.22281 0.0  
PR 11 11 12 Ee 5 a 10.1 nu4 1916.88870 -75.0 0.226E-04 2776.96964 860.00074 0.0  
RR 14 6 15 A2e 8 a 7.1 nu4 c1917.20063 0.0 0.572E-04 3486.76937 1929.61381 0.0  
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PR 12 2 13 Eo 23 a 1.0 2nu2 n1917.73456 0.0 0.116E-04 3435.67554 1518.25026 1.0  
PR 11 10 12 Ee 6 a 9.1 nu4 1917.86740 17.8 0.341E-04 2856.65384 938.78822 1.0  
PR 11 9 12 A2o 5 a 8.1 nu4 1918.08300 17.0 0.932E-04 3226.59256 1008.51126 1.0  
PR 11 8 12 Ee 11 a 7.1 nu4 1918.08300 17.0 0.932E-04 3226.59256 1008.51126 1.0  
RR 14 6 15 A2o 6 a 7.1 nu4 c1918.78487 0.0 0.536E-04 3848.11122 1929.32140 0.0  
PR 11 7 12 Eo 12 a 6.1 nu4 1918.89790 98.6 0.543E-04 3043.45519 1124.56715 1.0  
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OR 1 1 2 Ee 5 a 1.0 2nu2 1920.62040 -3.3 0.173E-03 1936.79372 19.88989 1.0  
QR 1 6 10 Ee 7 a 1.0 2nu2 1920.73740 -0.5 0.261E-03 2679.73508 759.02333 1.0  
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RR 14 5 15 Ee 19 a 6.1 nu4 1923.01653 0.0 0.130E-04 3890.49318 1967.47665 0.0  
RR 9 4 10 Ee 19 \*\*\* \*\* 1923.38300 -38.2 0.768E-04 2754.32701 830.94019 1.0  
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RR 8 7 9 Ee 9 a 5.1 nu4 1923.50710 14.1 0.481E-04 2456.41972 532.89403 1.0  
RR 11 2 12 Ee 22 \*\*\* \*\* n1923.63868 0.0 0.135E-04 3208.60392 1284.96524 0.0  
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OR 11 4 12 Ee 20 a 2.1 nu4 1923.91777 0.0 0.383E-03 3219.46317 1295.54540 1.0  
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OR 10 3 11 A2o 11 a 1.1 nu4 1928.87007 121.2 0.261E-03 2980.96435 1052.10640 1.0  
RR 10 5 11 Ee 17 \*\*\* \*\* n1929.13806 0.0 0.112E-04 2923.91119 994.77313 0.0  
OR 9 7 10 Eo 10 a 5.1 nu4 1931.10030 -17.7 0.502E-04 2643.95837 710.85630 1.0  
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PR 12 5 13 Ee 18 a 4.1 nu4 1937.69120 -121.8 0.141E-04 3381.80862 1444.10524 1.0  
PR 12 1 13 Ee 24 a 0.1 nu4 1937.72720 0.0 0.129E-04 3466.16057 1528.43337 0.0  
PR 12 7 10 Ee 11 a 5.1 nu4 1938.25150 26.9 0.784E-04 3189.79343 1267.28897 1.0  
PR 12 2 13 A2o 8 a 1.1 nu4 1938.28078 358.7 0.221E-04 3456.18589 1517.94098 1.0  
PR 12 6 13 A2o 8 a 5.1 nu4 1938.35290 -21.1 0.321E-04 3438.50878 1405.15377 1.0  
RR 12 4 13 Ee 15 a 3.1 nu4 1938.66870 46.3 0.165E-04 2519.44370 580.77963 1.0  
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RR 12 5 13 A2o 8 a 1.1 nu4 1939.62030 13.5 0.316E-04 3456.18589 1517.94098 1.0  
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RR 10 4 11 Ee 20 \*\*\* \*\* n1939.25000 0.0 0.307E-04 2966.78549 1027.53544 0.0  
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PR 12 11 13 Ee 6 a 10.1 nu4 c1940.32673 0.0 0.106E-04 3037.76527 1097.43706 0.0  
PR 12 12 13 A2o 2 a 1.1 nu4 c1940.66392 0.0 0.111E-04 2952.67265 1012.06388 0.0  
OR 12 9 13 A2e 12 a 1.1 nu4 c1940.74638 0.0 0.137E-04 3692.14934 1752.43300 0.0  
RR 8 8 9 Ee 8 \*\*\* \*\* 1941.04380 7.0 0.443E-04 2418.30719 477.26409 1.0  
RR 12 1 13 Ee 25 \*\*\* \*\* n1941.22122 0.0 0.288E-04 3469.65459 1528.43337 0.0  
OR 10 6 11 A2e 8 a 4.1 nu4 1941.50620 60.7 0.146E-03 2897.15290 955.65077 1.0  
PR 12 9 13 A2o 6 a 9.1 nu4 c1942.82958 0.0 0.185E-04 3187.20076 1244.37178 1.0

OR 11 5 12 Ee 17 a 3.1 nu4 1942.89140 1.9 0.483E-04 3152.97220 1210.08099 1.0  
OR 11 3 12 A2o 11 a 1.1 nu4 1943.11350 69.9 0.478E-03 3210.39548 1269.88997 0.0  
OR 11 5 12 Ee 17 a 3.1 nu4 c1943.20719 0.0 0.437E-04 3153.72715 1210.51206 0.0  
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PR 12 4 13 Ee 6 a 5.1 nu4 n1944.97235 0.0 0.115E-04 3350.53478 1405.56243 0.0  
MR 9 5 10 Ee 17 a 1.1 nu4 c1945.08130 0.0 0.297E-04 2743.45225 798.91483 0.0  
RR 12 4 13 Ee 22 \*\*\* \*\* n1945.62837 0.0 0.297E-04 3421.46135 1475.83298 0.0  
RR 9 7 10 Ee 11 \*\*\* \*\* c1946.27291 0.0 0.289E-04 2657.12980 710.85630 0.0  
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OR 10 7 11 Ee 12 a 5.1 nu4 1956.08180 -2.9 0.413E-04 2864.04712 907.96503 1.0  
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QR 3 1 4 Ee 9 a 1.0 2nu2 1956.82022 -5.9 0.316E-04 2072.36552 115.53661 1.0  
QR 3 2 4 Ee 9 a 2.0 2nu2 1957.39140 -4.0 0.261E-04 2061.81387 104.42207 1.0  
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OR 11 6 12 A2e 8 a 4.1 nu4 1960.92700 -2.2 0.695E-04 3131.68806 1170.76084 1.0  
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RR 9 6 10 A2e 9 a \*\*\* \*\* c1962.67676 0.0 0.147E-04 2721.71254 759.02333 0.0  
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RR 9 8 10 A2e 3 a 7.1 nu4 1966.04220 -16.3 0.147E-04 2558.63033 592.58650 1.0  
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OR 10 8 11 Ee 11 a 6.1 nu4 1976.50110 6.1 0.297E-04 2810.40785 853.90676 1.0  
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OR 11 7 12 Ee 15 a 5.1 nu4 1980.14710 -12.6 0.244E-04 3104.71571 1124.56715 1.0  
OR 11 7 12 Ee 15 a 5.1 nu4 1980.14710 -12.6 0.244E-04 3104.71571 1124.56715 1.0  
OR 12 6 13 A2o 10 a 1.1 nu4 c1981.36420 0.0 0.145E-04 3116.85891 1269.88997 0.0  
OR 12 6 13 A2o 10 a 1.1 nu4 n1982.31102 0.0 0.248E-04 3387.87345 1405.56243 0.0  
OR 12 3 13 A2o 13 a 1.1 nu4 n1983.89338 0.0 0.408E-04 3484.29743 1500.40405 0.0  
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QR 5 1 6 Ee 13 a 1.0 2nu2 1991.20962 4.7 0.235E-04 2285.17741 297.64176 1.0  
QR 5 1 6 Ee 13 a 1.0 2nu2 1991.20962 4.7 0.235E-04 2285.17741 297.64176 1.0  
QR 5 3 6 A2e 6 a 3.0 2nu2 1992.55550 3.6 0.559E-04 2257.07176 264.51662 1.0  
OR 10 9 11 A2e 5 a 7.1 nu4 1993.02544 -0.1 0.287E-04 2784.51339 791.48794 1.0  
OR 10 9 11 A2e 5 a 7.1 nu4 1993.02544 -0.1 0.287E-04 2784.51339 791.48794 1.0  
QR 5 4 6 Ee 12 a 0.0 2nu2 1993.82340 7.7 0.266E-04 2248.60757 295.10643 0.0  
OR 11 8 12 Ee 13 a 6.1 nu4 1995.08020 54.0 0.156E-04 3064.84628 1069.77148 1.0  
OR 13 3 14 A2o 13 a 1.1 nu4 n1995.21654 0.0 0.225E-04 3747.86474 1752.43300 0.0  
OR

Q R	10	7	*	11	Ee	21	a	7	0	2nu2	2076.93310	26.2	0.448E-04	2984.89551	907.96503	1.0
Q R	10	8	*	11	Ex	18	a	8	0	2nu2	2079.22450	33.5	0.508E-04	2932.43235	853.21120	1.0
Q R	10	9	*	11	A2e	7	a	9	0	2nu2	2082.26930	56.2	0.106E-03	2872.94421	790.68053	1.0
Q R	10	10	*	11	Ex	10	a	10	0	2nu2	n2086.27778	0.0	0.426E-04	2806.45688	720.17910	0.0
Q R	11	0	*	12	A2o	13	a	0	0	2nu2	n2087.40679	0.0	0.190E-04	3386.12923	1298.72244	0.0
Q R	11	2	*	12	Ex	25	a	2	0	2nu2	n2087.63905	0.0	0.103E-04	3372.24538	1284.60633	0.0
Q R	11	3	*	12	A2e	12	a	3	0	2nu2	n2087.94670	0.0	0.228E-04	3354.88405	1266.93735	0.0
Q R	11	4	*	12	Ex	24	a	4	0	2nu2	n2088.44509	0.0	0.130E-04	3330.55162	1242.10653	0.0
Q R	11	5	*	12	Ex	24	a	5	0	2nu2	n2089.16191	0.0	0.154E-04	3299.24290	1210.08099	0.0
Q R	11	6	*	12	A2o	12	a	6	0	2nu2	2090.17610	1.6	0.371E-04	3260.93678	1170.76084	1.0
Q R	11	7	*	12	Ex	23	a	7	0	2nu2	n2091.58092	0.0	0.226E-04	3215.61660	1124.03568	0.0
Q R	11	8	*	12	Ex	19	a	8	0	2nu2	n2093.49862	0.0	0.275E-04	3163.27010	1069.77149	0.0
Q R	11	9	*	12	A2e	8	a	9	0	2nu2	2096.09151	-1.3	0.648E-04	3103.90006	1007.80842	1.0
Q R	11	10	*	12	Ex	11	a	10	0	2nu2	2099.42695	-54.1	0.334E-04	3037.39059	937.95823	1.0
Q R	11	11	*	12	Ex	9	a	11	0	2nu2	c2104.01490	0.0	0.285E-04	2964.01347	860.00074	0.0
Q R	12	6	*	13	A2o	13	a	6	0	2nu2	n2105.13285	0.0	0.151E-04	3510.28662	1405.15377	0.0
Q R	12	8	*	13	Ex	21	a	8	0	2nu2	n2107.85007	0.0	0.122E-04	3412.97744	1305.12737	0.0
Q R	12	9	*	13	A2e	9	a	9	0	2nu2	n2110.36542	0.0	0.303E-04	3354.13256	1243.76714	0.0
Q R	12	10	*	13	Ex	13	a	10	0	2nu2	c2112.78997	0.0	0.177E-04	3287.31994	1174.60806	0.0
Q R	12	11	*	13	Ex	11	a	11	0	2nu2	n2116.61632	0.0	0.201E-04	3214.05338	1097.43706	0.0
Q R	12	12	*	13	A2o	5	a	12	0	2nu2	n2121.72970	0.0	0.344E-04	3133.73608	1012.00638	0.0
Q R	13	12	*	14	A2o	6	a	12	0	2nu2	n2134.43803	0.0	0.194E-04	3403.50887	1269.07084	0.0

Note : (I) : Assignment; (II) Identification of the upper level; (III): Vibrational band;  
 (IV) : Observed wavenumber in  $\text{cm}^{-1}$ . If the line was not observed,  
 "c" is the predicted value corrected with the average of the observed-calculated  
 values corresponding to all the transitions included in the fit that reach the same  
 upper state level, 'n' is the predicted value if no transition to the same upper  
 state level has never been observed or has never been included in the fit  
 (V) (Obs-calc) wavenumber in  $10^{-4} \text{ cm}^{-1}$ ;  
 (VI)  $S_0$  in  $\text{cm}^{-2} \text{ atm}^{-1}$  at 296 K; (VII) Upper state energy levels (in  $\text{cm}^{-1}$ );  
 (VIII): Lower state energy levels (in  $\text{cm}^{-1}$ ); (IX) : weight used for the energy fit.